



Using Taguchi method for the optimization of processing variables to prepare porous scaffolds by combined melt mixing/particulate leaching



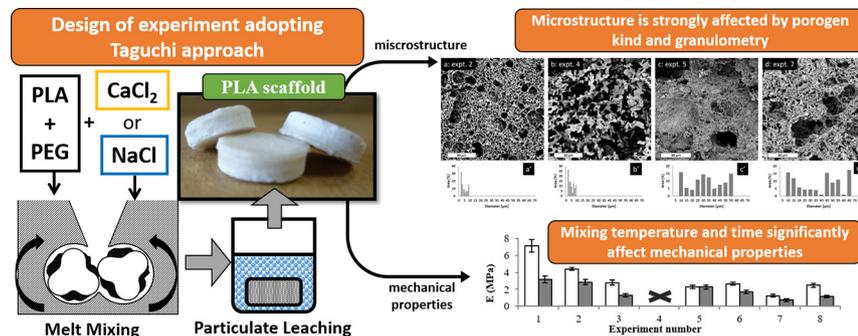
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HIGHLIGHTS

- Polylactic acid porous scaffolds were successfully fabricated by combining melt mixing and particulate leaching.
- Mixing temperature and time are the most significant variable affecting mechanical properties of the scaffolds.
- Pores morphology was found to be affected by the kind of porogen salt (i.e. NaCl or CaCl₂) and their dimension.

GRAPHICAL ABSTRACT



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ABSTRACT

Synthetic biopolymers have made significant inroads into the development of devices for tissue regeneration. In this context, a challenge is the achievement of appropriate properties mimicking the natural extracellular matrix by fabricating scaffolds presenting mechanical properties, specific surface, porosity and pore interconnection adequate for the final application. This study involved a systematic procedure based on Taguchi method for parameters optimization of melt mixing/particulate leaching combined processes aiming to enhance the performance of the scaffolds. In particular, it was evaluated the effect of time and temperature of melt mixing of the poly(lactic acid) matrix with two water-soluble inorganic porogen agents (i.e. NaCl or CaCl₂) with two different pore size and poly(ethylene glycol). Thereafter, the blends were compression molded and water-leached for different time and at different pH. By adopting L₈ Taguchi orthogonal array, seven control factors, each at two levels, were tested, and ANOVA was applied to find the statistically significant factors and the combination of their optimal levels. The results revealed that the mixing temperature had the highest effect on mechanical properties. Moreover, the internal architecture of the scaffolds was studied by morphological analysis, finding that it is affected by the kind of porogen salt and by mixing time.

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1. Introduction

Over the past decades, one of the primary aims of tissue engineering was to develop scaffolds using biodegradable and biocompatible materials for repairing bone or tissue defects by a regenerative process [1]. Due to the complexity of the human body, mimicking the structural

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and biological function of native extracellular matrix (ECM) requires materials with manifold characteristics [2–5]. Biomaterials used for this aim are ceramics, bioglass, polymers, composites either of natural or synthetic origin and, rarely, metals [6,7]. The current challenge is to find an ideal device with the following characteristics: (i) mechanical behaviour matching that of replacement tissue; (ii) suitable surface that actively supports cell attachment, proliferation and differentiation to build up the new tissue; (iii) appropriate pore dimensions, porosity and interconnection between pores in order to allow the transport of cellular nutrients and metabolites [8–10]; (iv) biodegradation rate comparable with tissue regeneration rate and innocuous degradation products; (v) sterilizability to avoid toxic contamination [6]. Actually, the most promising materials are biopolymers, widely studied because they are nontoxic, biocompatible and possess desirable mechanical and physical properties [4,9–11]. Among biodegradable polymers of synthetic origin, poly(lactic acid) (PLA) has been extensively studied for several decades, thanks to its chemical-physical properties and easy processability [5,12–14]. One of the most efficient plasticizers for PLA is poly(ethylene glycol) (PEG) hydrophilic and biocompatible polymer [13,15–18].

Since the above mentioned characteristics required for the scaffolds depend both on the polymer used and on the fabrication method [19], a wide variety of techniques have been developed to prepare scaffolds. Generally, those techniques can be divided into two groups: conventional and advanced [20]. Conventional techniques include combined melt mixing/particulate leaching [5,13,17], thermally induced phase separation [21], combined solvent casting/particulate leaching (SC/PL) [22], combined high-pressure moulding/salt leaching [23], gas anti-solvent [8]. Advanced techniques include, among the others, electrospinning [9,24] and 3D printing [25]. Each of these techniques has strengths and weaknesses regarding resolution control and manufacturability; e.g., the widely used SC/PL method, on the one hand can effectively control the porosity by varying the amount and size of the pore former on the other hand it often uses toxic solvent [13].

Since each method present peculiar processing variables, considerable effort has been directed in searching the relationships between these parameters and the final performance of the scaffolds [19]. Therefore, determining the influence of the process conditions by appropriate optimization methods, such as statistical methods, represents a useful strategy to improve specific target properties. Among the statistical methods, Taguchi's method is a useful tool applied to investigate the effect of multiple variables on the observed properties. Recently, Taguchi's approach has been successfully applied in combination with the analysis of variance (ANOVA) for the optimization of process parameters of several processes, e.g. investigation of the optimal design of ternary activators activated slag [26], production of metal-composite overlap joints [27], fabrication of hybrid plastic-metal joints for medical device applications [28], synthesis of minimal-size ZnO nanoparticles [29], tribological analysis of composite fibers [30], electrochemical machining [31], plastic materials processing [32,33], steel manufacture [34,35], engineering ceramics [36,37]. Eddie et al. [38] used Taguchi method and ANOVA in the parametric study of the biopotential equation for breast tumour identification and, finally, Lin et al. [39] and Dar et al. [40] applied such method in conjunction with others statistical approach. Up to date, Vigneswari et al. have been the only ones who applied Taguchi method and ANOVA in the design of scaffolds for tissue engineering to investigate the effect the significant process parameters on the hydrophilicity of the scaffolds and to determine their optimal values [41].

For the first time, our study applied Taguchi's experimental design and ANOVA to maximize the mechanical properties of porous scaffolds fabricated by combining melt mixing and particulate leaching; this combined manufacturing method offers several advantages in terms of low cost production, industrial scalability and absence of dangerous/toxic solvents. The process was optimized by using Taguchi's orthogonal arrays (OAs), a simple and easy tool to investigate a large number of variables by performing a workable number of experiments.

More in detail, the effect of seven process variables, i.e. porogen salt, salt granulometry, mixing temperature and mixing time, leaching temperature, leaching time and leaching pH, was investigated. This study analyses the effect of these parameters at two levels on the compressive Young's modulus in air and in phosphate buffered saline (PBS). The final goal is the determination of optimal values of the statistically significant processing variables, in order to maximize the compressive elastic modulus and to give immediate information and a precious tool to researchers for future studies. The results obtained have been validated by confirmation experiment.

2. Theoretical background: statistical methods, Taguchi approach and ANOVA

In 1920, for the first time the English statistician R. A. Fisher studied the effect of multiple variables simultaneously and developed a powerful statistical technique, the Design of Experiments (DOE) [42]. A design in which every setting of every factor (variable) appears with every setting of every other factor, identifying all possible combinations for the given set of factors, is a full factorial design [43,44]. The discrete values of the factors are named levels. If there are k factors, each at 2 levels, a full factorial design has $N = 2^k$ experiments [45]. However, since most industrial experiments usually involve a relevant number of factors, a full factorial design would often result in a too large number of experiments. The fractional factorial design reduces the number of experiments by selecting only a small set from all the possible experimental combinations. In this issue, to reduce the number of experiments to a practical level, Taguchi's approach inserts in the science of DOE by selecting only a small set of orthogonal arrays (OAs), from all possible experimental combinations, which includes all the independent combinations of the factors chosen [46].

Before beginning the experimental runs, Taguchi's approach decides the entire process, i.e. the factors, the levels, how run the tests, how analyse the results. These steps are in contrasts with the traditional techniques in which some initial ideas are tested, followed by other ideas and tests and so on. Taguchi's approach has consistency and reproducibility rarely found in any other statistical methods and it can be employed to obtain the best values of process variables, called optimal values in Taguchi's terminology, with the minimum number of investigations.

Analysis of variance (ANOVA) is the most common statistical method applied to results, in a factorial design of experiments, to determine which factors examined have most influence on the property of interest. The effect of one factor represents the variation of the response of interest of the process varying the levels of the same factor. ANOVA computes quantity called sum of squares, degree of freedom, variance and variance ratio and organizes in standard tabular format [47]. ANOVA uses a F-test to determine the statistically significant factors within the confidence interval examined. A more detailed explanation about ANOVA application is provided in the Supporting information (SI).

3. Experimental

3.1. Design of experiments using the Taguchi approach

The experiments were carried out with seven variables (factors) and two discrete values (levels) for each variable: type of porogen salt, salt granulometry, temperature and time of melt mixing, temperature, time and pH of leaching. Table 1 shows the factors selected and their levels.

It may be expected that the porogen salt factor may change the pore shape and therefore the microstructure of the scaffold, in addition to the leachability, while salt granulometry may dominates the pore size. It is reasonable to suppose that mixing temperature and time will vary the viscosity and the molecular weight of thermo-mechanically biodegradable PLA, which influence the mechanical properties. Finally, the factor

Table 1
Parameters selected and their values at two different levels.

Code	Parameter	Level 1	Level 2
A	Salt granulometry (μm)	0–45	90–110
B	Mixing temperature ($^{\circ}\text{C}$)	190	220
C	Mixing time (seconds)	300	600
D	Porogen salt	NaCl	CaCl ₂
E	Leaching time (hours)	5	8
F	Leaching temperature ($^{\circ}\text{C}$)	50	70
G	Leaching pH	4.74 buffer	7 no buffer

related to the leaching, i.e. time, temperature and pH, will affect the efficiency of removing the porogen salt.

Table 2 presents the L₈ Taguchi OA selected in this study with the assigned parameters. The table consists of seven columns, which were assigned the seven factors, and eight rows that define the eight trials conditions that have to be performed. Across the row, it is possible to read the discrete values, at the level 1 (low level) or 2 (high level) that must be assumed during the experiment.

4. Materials and methods

4.1. Materials

Poly(lactic acid) (PLA 2002D, $M_w = 112,600$ g/mol, density $\rho = 1.24$ g/cm³ [48]) was purchased from NatureWorks®. Poly(ethylene glycol) (PEG, $M_w = 2000$ g/mol, $\rho = 1.12$ g/cm³), sodium chloride (NaCl, purity > 99%, $\rho = 2.16$ g/cm³) and calcium chloride (CaCl₂, purity > 93%, $\rho = 2.15$ g/cm³) were purchased by Sigma-Aldrich.

In this work, NaCl and CaCl₂ were first ground and sieved to obtain two size ranges in order to fabricate scaffolds with two different pore dimensions, i.e. 0–45 μm and 90–110 μm . Before processing, both PLA and the salts were dried in a vacuum oven at 90 $^{\circ}\text{C}$ for 16 h to prevent macromolecules hydrolytic scission and particles re-aggregation during processing.

4.2. Scaffolds fabrication

Porous scaffolds have been manufactured by melt mixing as described in our previous works [10,49]. In brief, PLA/PEG/salt, with formulation 12/3/85 wt%, were fed to a batch mixer (Brabender PLE-330) and processed at the temperature and for the period of time of the specific running experiment, as reported in Table 2. The blends were compression molded in a Carver laboratory press at 210 $^{\circ}\text{C}$ and 180 bar in an appropriate cylindrical mold with a diameter of 10 mm and a height of 3 mm.

The final step is the selective leaching of the porogen agents of the scaffolds (salt and PEG) in demineralized water under the specific conditions of temperature, time and pH depending of the running experiment. The resulting porous structures were let to dry for 24 h at room temperature. Figs. 1a–b show the samples before leaching and after leaching and drying.

Table 2
Taguchi orthogonal array L₈ of the experimental runs.

Expt. no.	A Salt granulometry (μm)	B Mixing temperature ($^{\circ}\text{C}$)	C Mixing time (s)	D Porogen salt	E Leaching time (h)	F Leaching temperature ($^{\circ}\text{C}$)	G Leaching pH
1	0–45	190	300	NaCl	5	50	4.74
2	0–45	190	300	CaCl ₂	8	70	Neutral
3	0–45	220	600	NaCl	5	70	Neutral
4	0–45	220	600	CaCl ₂	8	50	4.74
5	90–110	190	600	CaCl ₂	5	50	Neutral
6	90–110	190	600	NaCl	8	70	4.74
7	90–110	220	300	CaCl ₂	5	70	4.74
8	90–110	220	300	NaCl	8	50	Neutral

4.3. Characterizations

4.3.1. Scanning Electron Microscopy (SEM)

The morphology of the scaffolds were evaluated by scanning electron microscopy (Quanta 200 ESEM, FEI) equipped with EDX probe. The samples were fractured in liquid nitrogen and then sputter-coated with a thin layer of gold (Sputtering Scancoat Six, Edwards) in order to avoid electrostatic discharge during the test.

4.3.2. Pore Size Distribution (PSD)

Pore size analyses were carried out using a MATLAB (MathWorks Inc., MA, USA) based software previously described [49]. The custom-made software is able to accomplish the segmentation of images containing pores of any geometry in a semi-automatic way. It converts the digital images into binary form and then calculates the pores area distribution (PAD). The software reports the percentage of the total area occupied by the pores having diameters in a given interval. PAD were calculated in different seven region of the scaffolds. A minimum of 7 spots for each experiment were analyzed and representative data were shown.

4.3.3. Torque measurements

During the melt processing step, the mixing torque was monitored versus the time to obtain qualitative indications of melt viscosity.

4.3.4. Mechanical properties

Compression tests on the scaffolds were performed in two different mediums, air and phosphate buffered saline (PBS), using an universal testing machine (Instron model 3365). The tests in air were carried out at room temperature while those in PBS were carried out at $T = 37$ $^{\circ}\text{C}$ by using BioPuls Temperature Controlled Bath (Norwood, MA), pH = 7.4. In order to prepare samples to measurements in BioPuls Bath, the pores of the scaffolds were filled with PBS in a vacuum flask for 5 min to let PBS to fill the inner pores. Thereafter, the scaffolds were left in PBS at 37 $^{\circ}\text{C}$ for 15 min to let the achievement of the temperature test throughout the structure. The samples (3:10 height-diameter ratio) were tested under deformation control with a constant crosshead speed of 1 mm/min. A minimum of 7 specimens were averaged for each experiment.

4.4. Statistical analyses

Analysis of variance (ANOVA) was applied for investigating the percentage contribution of the individual parameters on compressive Young's modulus in air and in PBS. ANOVA computes quantity called sum of squares (SS), degree of freedom (DOF), variance (V) and variance ratio, organizes in standard tabular format [47] and uses a F-test to determine the statistically significant factors within the confidence interval examined (see S2 section in SI).

According to Taguchi method, after identifying the optimal level of each process parameter, a confirmation test was carried out and statistical analyses of the data were performed by using the GraphPad Prism version 6 software (GraphPad Software Inc., La Jolla, CA, USA). Significant differences among mean values were determined by the means

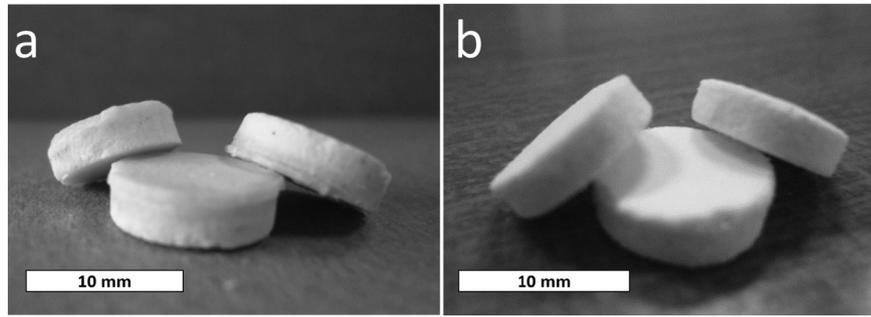


Fig. 1. (a) Example of scaffolds before the leaching and (b) after the leaching and the drying for 24 h at room temperature.

of ANOVA and by Tukey's Honestly Significant Difference (HSD) post hoc test for multiple comparisons.

In this work, the statistical analyses were carried out for a level of confidence of 95%.

5. Results and discussion

5.1. Morphological analysis of scaffolds

The morphology of the scaffolds was observed to investigate the effect of salt type and particles size on the internal porous architecture. Since the pores morphology strongly depends on the type of salt involved in the experiment, the SEM images related to NaCl salt, i.e. experiments no. 1, 3, 6, 8, and the SEM images related to CaCl_2 salt, i.e. experiments no. 2, 4, 5, 7, will be shown and discussed separately.

5.2. Experiments with NaCl as porogen salt (expts. no. 1, 3, 6, 8)

Figs. 2a–d show the SEM images of the porous architecture of the scaffolds obtained by leaching NaCl, while Figs. 2a'–d' show their corresponding PAD. In particular, Fig. 2a displays the morphological structure of the scaffolds manufactured under the experimental conditions no. 1 which keep all the factors at the lowest level. The macro-pores, resulting by NaCl solubilization, are highly interconnected due to the micro-pores in the walls, formed during PEG solvation [4,13,49]. The presence of these micro-pores in the structure is crucial because they drive the water deeply in the core of the structure ensuring complete leaching of the scaffold and allowing the passage of cell nutrients after implantation.

SEM analysis showed no evidence of the presence of residual NaCl particles as confirmed by EDX analysis carried out on all the related materials. In fact, the EDX carried out on the experiments with NaCl as porogen salt revealed the presence of only three elements i.e. O (in the range 64–66 atomic %), C (in the range 32–34 atomic %) and Au (in the range 2.8–3.2 atomic %) due to the sputter-coating with gold.

The presence of PEG, partially miscible with PLA, induced roughness to the pore walls (Fig. 2a) also according to previous findings [13,50]. Indeed, it is known that the plasticizing effect of PEG increases chain mobility and also acts as nucleating agent accelerating the creation of crystalline domains; the formation of spherulites with different size, morphologies and distribution in PLA/PEG blends leads to surface roughness [15]. The PAD of this system, shown in Fig. 2a', presents a bimodal behaviour with two peaks at 20 μm and 40 μm .

Fig. 2b shows the morphology of the scaffolds prepared under the following experimental condition (expt. no. 3): salt granulometry 0–45 μm , mixing temperature 220 $^{\circ}\text{C}$, mixing time 600 s, porogen salt NaCl, leaching time 5 h, leaching temperature 70 $^{\circ}\text{C}$ and neutral pH. The presence of a higher number of pores smaller than 10 μm (Fig. 2b') can be likely associated to the longer mixing time that increased the NaCl breaking. The leaching condition seems not to affect the shape of the pores.

In Fig. 2c the size range of the salt leached is 90–110 μm . The pore dimensions has a bimodal behaviour (Fig. 2c') with a peak at about 50 μm and another corresponding to the salt granulometry. The walls of the internal structure appear rough, likely due to leached PEG incorporated in the blend, as it was also found in the other experimental runs. However, compared to the previous cases, pore shape is more similar to NaCl crystals shape. This result can be justified by the larger dimensional range of

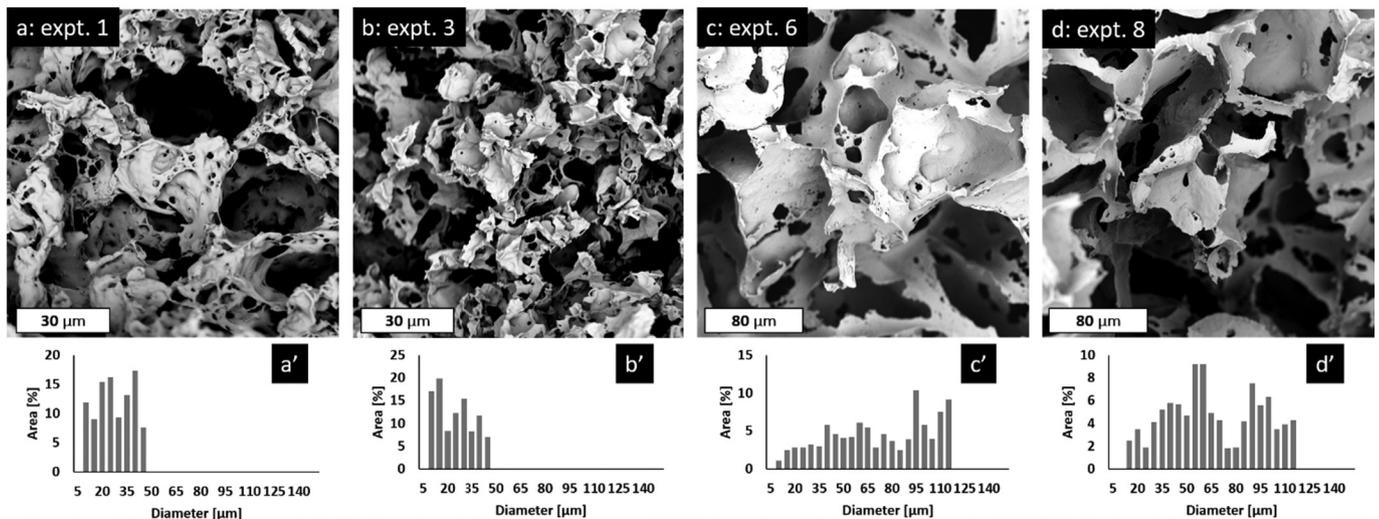


Fig. 2. SEM images of the scaffolds derived by leaching of NaCl salt and their corresponding PAD: (a, a') experiment no. 1 and (b, b') expt. no. 3; (c, c') expt. no. 6 and (d, d') expt. no. 8.

the salt particles that produces a lower interfacial area and, as a consequence, promotes a more efficient PLA wrapping of the NaCl particles. It is evident the effectiveness of the leaching process, in agreement with the strong leaching conditions, $T = 70\text{ }^{\circ}\text{C}$ and $t = 8\text{ h}$.

The morphological structure of the scaffolds prepared in run no. 8 - i.e. NaCl as porogen salt with granulometry 90–110 μm , mixed at 220 $^{\circ}\text{C}$ for 300 s, and leached 8 h at 50 $^{\circ}\text{C}$ and neutral pH - is showed in Fig. 2d. The PAD, in Fig. 2d', is similar to the PAD in Fig. 2c' (expt. no. 6) but the peak at 50 μm is higher than that at 100 μm . Again, this result highlights the effect of the mixing time on the PAD, i.e. higher mixing time increases NaCl fracture. The leaching variables seem to not to affect the morphology of the pores.

5.3. Experiments with CaCl_2 as porogen salt (expts. no. 2, 4, 5, 7)

Figs. 3a–d and Figs. 3a'–d' report the morphologies and their corresponding PAD of the scaffolds manufactured with calcium chloride as porogen salt. They are deeply different compared to those deriving from sodium chloride. Fig. 3a shows the uniform and rounded pore shape of the scaffold obtained in run no. 2, CaCl_2 particles diameter 0–45 μm , temperature and melt mixing time respectively 190 $^{\circ}\text{C}$ and 300 s, temperature and time of leaching equal to 70 $^{\circ}\text{C}$ and 8 h, and neutral pH. The walls are not indented, as found in the case of NaCl, and the small thickness allow forming a continuous structure surrounding the pores, despite the higher superficial area of the salt particles due to smaller granulometry. These results may derive from the different shape of CaCl_2 crystals and their interaction with the matrix, if compared to NaCl crystals. The PAD in Fig. 3a' shows a bimodal pore distribution with high number of micropores and a little peak around 10 μm . Fig. 3b displays the SEM image of the scaffolds fabricated during expt. no. 4, that is by using CaCl_2 salt with size range 0–45 μm , by mixing the material for 600 s at 220 $^{\circ}\text{C}$ and by leaching the scaffolds 8 h at 50 $^{\circ}\text{C}$ and pH 4.74. The structure is highly porous and interconnected with rough walls and a bimodal PAD very similar to that of the exp. no. 2, as highlighted in Fig. 2b'. In Fig. 3c, it is reported the morphology of scaffolds prepared using particles diameter 90–110 μm , mixed at 190 $^{\circ}\text{C}$ for 600 s and leached at 50 $^{\circ}\text{C}$, 5 h at neutral pH (variable set no. 5). The morphology is similar to that of the scaffolds prepared in expt. no. 2 except for pore dimensions, that present three PAD peaks at about 10 μm , 35 μm and 45 μm (Fig. 3c'). Finally, Fig. 3d exhibits the internal structure of the scaffolds prepared during the experiment no. 7, with the granulometry 90–110 μm , the mixing temperature of 220 $^{\circ}\text{C}$ for 300 s and leached at 70 $^{\circ}\text{C}$, 5 h, pH value 4.74. The three-modal PAD behaviour (Fig. 3d') is very similar to that found in expt. no. 5, being equal the size range of the salt particles. All the structures are highly porous and

interconnected. The morphological analysis clearly revealed that the use of CaCl_2 as porogen agent makes difficult the control of internal architecture of the scaffold. Indeed, although expts. no. 5 and no. 7 were carried out with salt granulometry in the range 90–110 μm , the resulting pores dimension is smaller. This phenomenon should be due to the breakage of CaCl_2 particles during the melt mixing, easier if compared to NaCl. The breakage of the CaCl_2 particles can be also considered the reason to the uneven distribution of pores size showed by the PAD. Even in this case, SEM analysis showed no evidence of the presence of residual CaCl_2 particles: the EDX carried out on the experiments with CaCl_2 as porogen salt revealed the presence of oxygen, carbon and gold in the same atomic % range of the NaCl experiments. The leaching time and temperature seem to not to affect the morphology of the pores.

5.4. Viscosity measurements of the blends

Qualitative indications of melt viscosity and viscosity-temperature dependence can be obtained by using Brabender torque-rheometer [51]. Therefore, during the melt mixing operation the torque values were collected and reported as a function of time to indirectly monitor the variation of viscosity of the blends. The torque offered by the blends depends both on kind and on granulometry of the salt and on mixing temperature. Fig. 4 shows the torque values of the blends incorporating sodium chloride as porogen salt. It is worth noting that the torque of the blends processed at 220 $^{\circ}\text{C}$ (expts. no. 3 and no.8) is lower than that observed for the blends processed at 190 $^{\circ}\text{C}$ (expts. no. 1 and no. 6). This behaviour is due to the improvement of the mobility of the polymer chains and to the decrease of the resistance between the melt layers at higher temperature [52], related to the decreasing of the melt viscosity with increasing temperature.

After an initial steep reduction, the torque slowly decreased due to the melting of the polymer matrix. Thereafter, a steady state is reached and this stabilization is remarkable for longer time, i.e. 600 s, and less evident for shorter time, i.e. 300 s.

The blends containing CaCl_2 show torque values higher than those of the blends with NaCl, particularly in the early moments of the mixing (Fig. 5). This behaviour might be due to the easier breakage of the crystals that produces a larger surface area. Indeed, from PAD analysis of the expts. no. 2 and no. 4 (Figs. 3a'–b'), salt granulometry 0–45 μm , it can be observed high amount of the pores in the dimensional range 1–10 μm and few pores in the dimensional range 10–45 μm . Likewise, for the 90–110 μm size range, most of pores belongs to a smaller dimensional range, probably due to the breakage of salt particles during mixing.

In Fig. 5, the curves of the systems mixed at 190 $^{\circ}\text{C}$, namely expts. no. 2 and no. 5, show values of torque higher than the systems no. 4 and no.

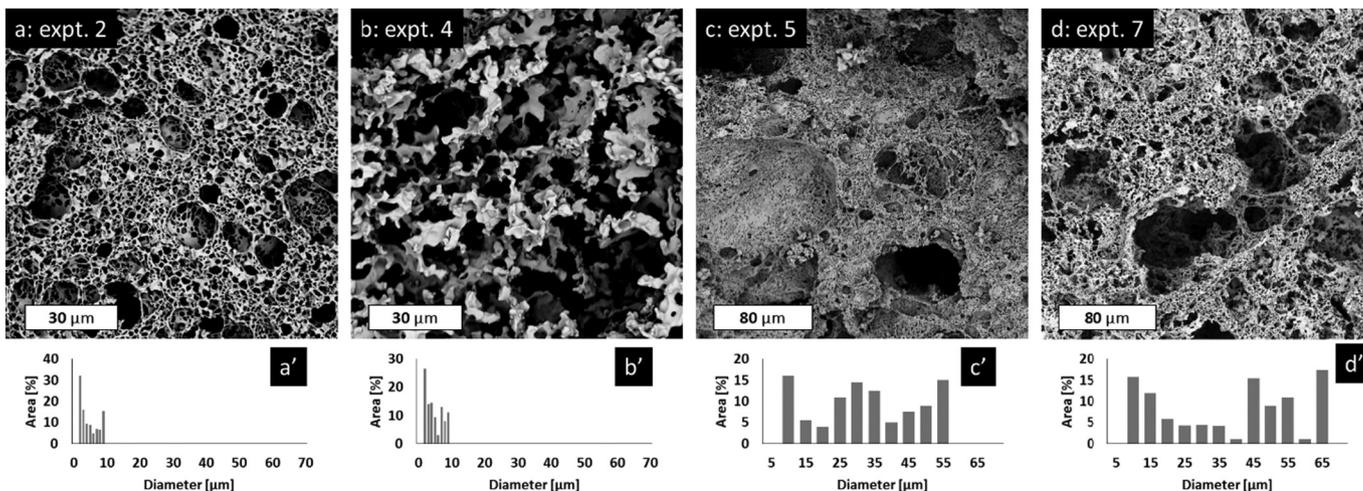


Fig. 3. SEM images of the scaffolds derived by leaching of CaCl_2 salt and their corresponding PAD: (a, a') experiment no. 2 and (b, b') expt. no. 4; (c, c') expt. no. 5 and (d, d') expt. no. 7.

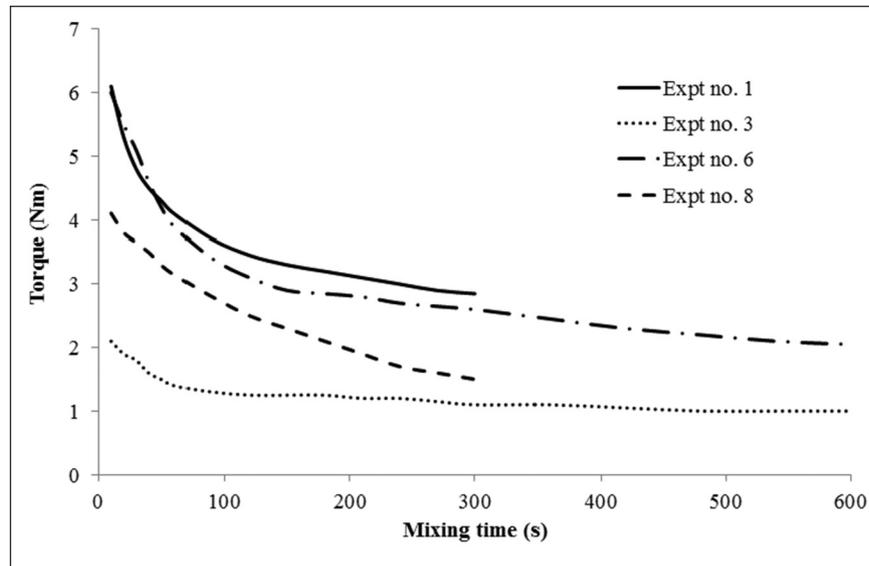


Fig. 4. Torque curves of the blends containing NaCl salt, experiments no. 1 (salt granulometry 0–45 μm , mixing temperature 190 $^{\circ}\text{C}$, mixing time 300 s), no. 3 (salt granulometry 0–45 μm , mixing temperature 220 $^{\circ}\text{C}$, mixing time 600 s), no. 6 (salt granulometry 90–110 μm , mixing temperature 190 $^{\circ}\text{C}$, mixing time 600 s), and no. 8 (salt granulometry 90–110 μm , mixing temperature 220 $^{\circ}\text{C}$, mixing time 300 s).

7 mixed at 220 $^{\circ}\text{C}$, in accordance with the decrease of viscosity with temperature. Being temperature the same, the torque of the blend no. 2 (size range 0–45 μm) is higher than that of the blend no. 5 (size range 90–110 μm) and the torque of the blend no. 4 (size range 0–45 μm) and is higher than that of the blend no. 7 (size range 90–110 μm). At the same temperature conditions, the torque depends by the dimensional range of the particles: by decreasing the diameter of the particles, the torque increases because of the higher interfacial area and subsequent larger interaction between CaCl_2 salt and polymer matrix.

As in the case of blends with NaCl, at the beginning of the mixing time, the values of torque quickly decrease because of polymer matrix melting that causes the reduction of viscosity, afterwards the trend is almost constant (Fig. 5).

5.5. Effect of the process variables on mechanical properties

As already marked in this study, the aim of the optimization of process parameters is the maximization of the compressive Young's modulus.

The compressive mechanical tests were carried out both in air at ambient temperature and in PBS at 37 $^{\circ}\text{C}$ to simulate wet conditions.

Fig. 6 displays nominal stress-strain curves (σ - ϵ) of the scaffolds. After the initial elastic deformation (Fig. 6-inset), likely related to the bending of the walls of the pores [13], there is a transition zone that indicates the beginning of the permanent plastic deformation (Fig. 6-inset) [13,53]. The final region of the stress-strain curve monolithically increases, indicating the typical plastic deformation of the thermoplastic polymers, which may be associated with the densification of the

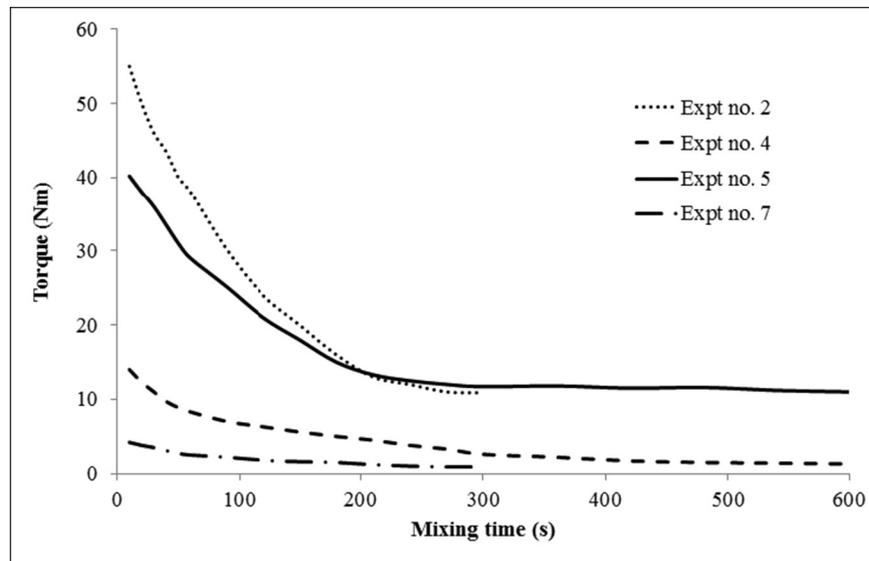


Fig. 5. Torque curves of the blends containing CaCl_2 salt, experiments no. 2 (salt granulometry 0–45 μm , mixing temperature 190 $^{\circ}\text{C}$, mixing time 300 s), no. 4 (salt granulometry 0–45 μm , mixing temperature 220 $^{\circ}\text{C}$, mixing time 600 s), no. 5 (salt granulometry 90–110 μm , mixing temperature 190 $^{\circ}\text{C}$, mixing time 600 s), no. 7 (salt granulometry 90–110 μm , mixing temperature 220 $^{\circ}\text{C}$, mixing time 300 s).

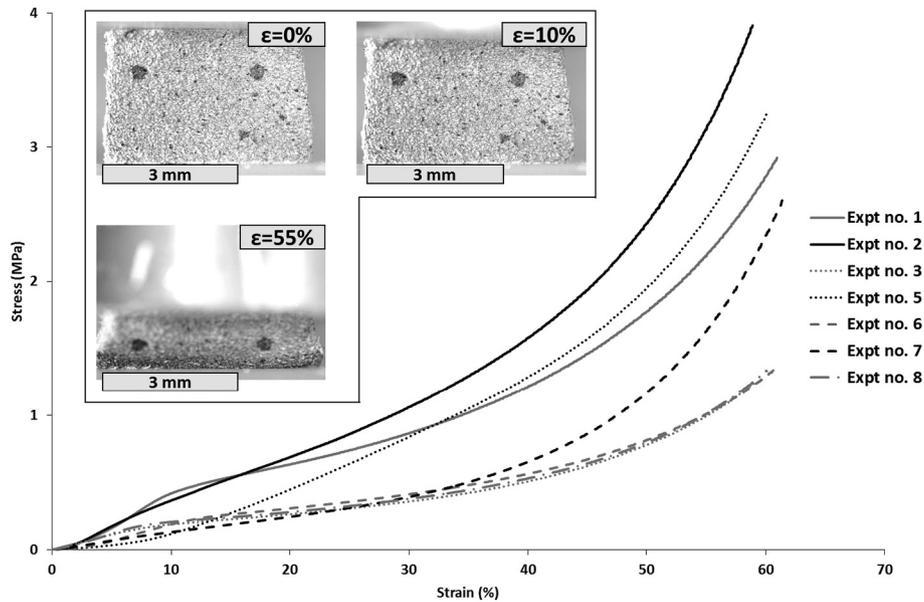


Fig. 6. Compressive stress-strain curves of the scaffolds. Inset: pictures of the scaffold (expt. no. 8) during compression at different strain percentage (ϵ).

internal architecture of the sample (Fig. 6-inset) [13]. The shape of the stress-strain curves of the scaffolds tested in PBS is the same, even if, of course, with values of lower magnitude.

Fig. 7 reports the mean values of the compressive Young's modulus in air and in PBS, calculated as the slope of the linear stretch in the stress-strain curves, for the scaffolds of all the experimental runs. The diagram does not show the values of the expt. no. 4 because the scaffolds crumbled during leaching. This phenomenon might be imputed to the previous degradation of the material during melt mixing operation under the hardest conditions, i.e. $T = 220\text{ }^{\circ}\text{C}$ and $t = 600\text{ s}$.

The data in Fig. 7 were used for F-test calculation and Table 3 shows the results of pooled ANOVA for the dry elastic modulus. At first, column G was associated with the estimate of the error due to its lower SS value. In these calculations, no factor was found to be statistically significant. Therefore, by *pooling up* and by merging G and F column effects, the factors A–E were found to be statistically significant at a level of confidence of 95%. The last column of Table 3 shows the percentage contribution of each factor on the total variation of the elastic modulus, that is the degree of influence on the result.

In Fig. 7, the highest elastic modulus is observed for the of the experiment no. 1, followed by expt. no. 2. These blends were melt mixed at $190\text{ }^{\circ}\text{C}$ for 10 min which are the optimal levels of the first two factors statistically significant revealed by the analysis of variance. The following statistically significant factors, in order of significance, are: type of salt, size range and leaching time. These results can be likely associated to the degradation of the polymer chains induced by melt mixing. In fact, it is well established that PLA is susceptible to thermo-degradation during melt processing operations [54]. The use of NaCl salt gives more uniform internal structure while smaller pore size leads to more homogeneous mass distribution of PLA in the scaffold [55] and a greater number of points of contacts, so that the elastic modulus of the devices is higher. The lower leaching time, level 1 of the factor E, allows the scaffolds to be exposed at the thermal stress of leaching for a shorter time, however, it is the least influential factor.

The tests carried out in wet condition present values of the elastic modulus lower than the corresponding in dry (Fig. 7), therefore the elastic characteristic of the materials immersed in PBS decreases, except for the expt. no. 5 that presents a values almost constant.

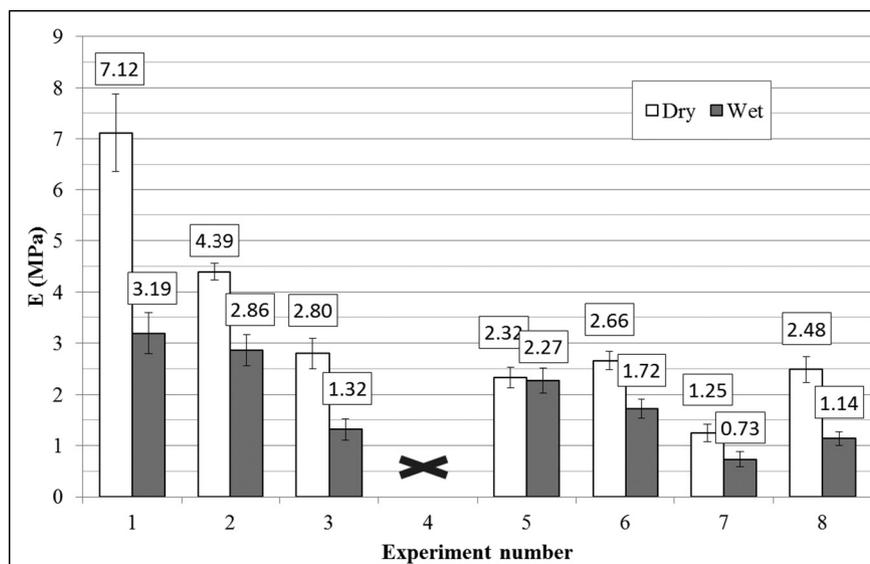


Fig. 7. Compressive Young's modulus of the scaffolds in dry and wet environment, for all the experimental runs.

Table 3
ANOVA for Young's modulus in air.

Source	SS	DOF	V	F _{calc} (e pooled)	P (%)
A	3.920	1	3.920	39.35 ^b	12.35
B	12.400	1	12.400	124.47 ^b	39.07
C	6.956	1	6.956	69.83 ^b	21.92
D	6.301	1	6.301	63.25 ^b	19.85
E	1.960	1	1.960	19.68 ^b	6.18
F ^a	0.084	1	0.084		0.26
G ^a	0.115	1	0.115		0.36
Tot	31.737	7			
<i>e pooled</i>	0.199	2	0.100		

SS Sum of squares, DOF Degree of freedom, V Variance, F_{calc} F value calculated in F test, P (%) = SS_{Tot}/SS_i; Percent contribution.

^a Factors merged in *e pooled*.

^b Significant at 95% confidence level.

Table 4 shows the analysis of variance performed for the wet elastic modulus. At 95% confidence level, by considering the factor F for the evaluation of the error, all the factors were found to be statistically significant. In this case, it was not necessary to apply pooling up method.

Table 5 displays the significant factors affecting Young's modulus in air and in PBS, in order of contribution, and their optimal values among those investigated. It is interesting to note that in the case of wet elastic modulus, unlike the dry elastic modulus, the pH of leaching takes statistically significance overcoming the effects of time leaching and salt granulometry.

6. Confirmation test

Confirmation test with the optimal levels of the significant parameters was carried out in order to verify the effectiveness of the results in Taguchi's design approach [47]. The optimal values were set for the significant factors while the no significant factors were set at economic levels. Seven confirmation experiments were conducted and the average of the results is equal to 7.34 and 3.26 for E_{dry} and E_{wet} respectively. According Tukey's HSD post hoc test, the values did not show statistically significant difference if compared with the optimum performance estimated by the expt. no. 2.

7. Conclusions

Processing parameters generally have a great impact on the mechanical properties of polymer based systems. The Taguchi method was applied to investigate the effects of seven process parameters on the properties of PLA-based porous scaffolds for tissue engineering prepared by combined melt mixing and particulate leaching.

The results obtained in this study indicate that the most statistically significant factors affecting the mechanical properties are temperature and time of mixing, kind of porogen salt, followed by salt granulometry

Table 4
ANOVA for Young's modulus in PBS.

Source	SS	DOF	V	F _{calc} (e = F)	P (%)
A	0.285	1	0.285	2533 ^a	3.49
B	5.865	1	5.865	52,136 ^a	71.85
C	0.852	1	0.852	7569 ^a	10.43
D	0.285	1	0.285	2533 ^a	3.49
E	0.401	1	0.401	3560 ^a	4.91
F	0.112 × 10 ⁻³	1	0.112 × 10 ⁻³		0.00
G	0.475	1	0.475	4225 ^a	5.82
Tot	8.163	7			
<i>e pooled</i>	2.297	6	0.383		

SS Sum of squares, DOF Degree of freedom, V Variance, F_{calc} F value calculated in F test, P (%) = SS_{Tot}/SS_i; Percent contribution.

^a Significant at 95% confidence level.

Table 5
Significant factors affecting Young's modulus in air and in PBS and their optimal values, among the two investigated values, in order of contribution.

Significant factors	Optimal level
Young's modulus in air	
B: Mixing temperature	190 °C
C: Mixing time	300 s
D: Porogen salt	NaCl
A: Salt granulometry	0–45 μm
E: Leaching time	5 h
Young's modulus in PBS	
B: Mixing temperature	190 °C
C: Mixing time	300 s
G: Leaching pH	7 no buffer
E: Leaching time	5 h
A: Salt granulometry	0–45 μm
D: Porogen salt	NaCl

and time of leaching. More in detail, the temperature and the time of mixing are the most statistically significant variable and their optimal level were the lowest (at 95% confidence level). In particular, the highest elastic modulus value was obtained for the samples prepared by melt mixing temperature of 190 °C and for a mixing time of 300 s. Increasing one of these parameters induce a significant reduction of the modulus value in almost all the experiments. These results can be likely associated to the thermo-degradation of the polymer chains induced by the melt mixing.

In this work, the combination of Taguchi's experimental design and ANOVA provided a simple and effective systematic approach for the determination of the optimal levels of the significant parameters carrying out a reduced number of experiments.

The optimal values obtained in this research may be adopted in future process of fabrication of porous scaffolds within the melt mixing and particulate leaching with same materials. Moreover, this work may be considered as a preliminary study for further experimental investigation of the significant factors in more complicated factorial design or to evaluate further properties such as cell activities, adhesion, infiltration and differentiation, as well as control of cell delivery with drug impregnation in PLA scaffold and kinetic of bioabsorption.

Appendix A. Supplementary data

Supplementary data to this article can be found online at <http://dx.doi.org/10.1016/j.matdes.2017.06.025>.

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