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A PTFE membrane for the in situ extraction of dissolved gases in natural waters: Theory and applications

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[1] A new method for extracting dissolved gases in natural waters has been developed and tested, both in the laboratory and in the field. The sampling device consists of a polytetrafluroethylene (PTFE) tube (waterproof and gas permeable) sealed at one end and connected to a glass sample holder at the other end. The device is pre-evacuated and subsequently dipped in water, where the dissolved gases permeate through the PTFE tube until the pressure inside the system reaches equilibrium. A theoretical model describing the time variation in partial gas pressure inside a sampling device has been elaborated, combining the mass balance and "Solution-Diffusion Model" (which describes the gas permeation process through a PTFE membrane). This theoretical model was used to predict the temporal evolution of the partial pressure of each gas species in the sampling device. The model was validated by numerous laboratory tests. The method was applied to the groundwater of Vulcano Island (southern Italy). The results suggest that the new sampling device could easily extract the dissolved gases from water in order to determine their chemical and isotopic composition.

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1. Introduction

[2] The study of the chemical and isotopic composition of the dissolved gases in natural waters is a very useful tool in several branches of the earth sciences, e.g., hydrology, volcano monitoring and earthquake prediction [Gurrieri et al., 1984; D'Alessandro et al., 1997; Allard et al., 1997; Sano et al., 1998; Capasso et al., 2000; Italiano et al., 2004]. Dissolved gases can also be used as environmental tracers in groundwater dating techniques and in the determination of recharge

temperature [Mazor, 1977; Andrews et al., 1989; Stute et al., 1995; Sanford et al., 1996; Solomon et al., 1998; Aeschbach-Hertig et al., 1999; Peeters et al., 2002; Manning and Solomon, 2003]. Furthermore, the study of dissolved gases occupies an important role both in freshwater biochemistry and oceanography [Kana et al., 1994; McNeil et al., 1995; Chapelle et al., 1997; Emerson et al., 2002].

[3] Different methods have been developed in order to separate the dissolved gaseous phase from



liquid water. They can be divided into two main groups: the laboratory extraction technique (LET) and the field extraction technique (FET). LET methodologies are based on three different techniques: the vacuum extraction technique (VET), the equilibration extraction technique (EET) and the bubble extraction technique (BET). In the VET, a water sample is usually collected with a special copper tube or glass vessel with stopcocks, after which the dissolved gases are extracted, following a specific procedure in the laboratory which involves a vacuum line. This method is widely used for noble gas analysis [Weiss, 1968; Mazor, 1977; Andrews et al., 1985; Bayer et al., 1989; Ludin et al., 1997; Beyerle et al., 2000]. Another VET method separates the dissolved gases from a water sample, which has been collected in a Schlenk bottle. The bottle is connected to a vacuum line and dipped in an ultrasonic bath [Holt et al., 1995]. This line is equipped with cold traps and a complex valve system with which to separate each gas species.

- [4] The EET technique is based on the gas partitioning equilibrium between the liquid and gas phases, and it involves the collection of a water sample in a glass flask of known volume and its equilibrium with a host gas. According to Henry's law, the host gas dissolves in water and, simultaneously, the dissolved gases pass from the liquid phase to the gas phase until equilibrium is reached. The total amount of dissolved gases is computed by the partitioning equilibrium between the gas and the liquid, where the equilibrium can be mainly obtained in two ways: either a known volume of the host gases is injected into a glass flask, which draws out the equivalent water volume [Capasso and Inguaggiato, 1998; Inguaggiato and Rizzo, 2004] or the host gas and water sample are inserted into a special injector [Sugisaki and Taki, 1987]. Finally, the bubble extraction method (BET) was mainly developed to detect dissolved hydrocarbons in environmental research. It consists of the equilibration of a water sample in a bulb, with a headspace filled with an inert gas. The water is pumped through the bulb until equilibrium is reached [Walsh and McLaughlan, 1999].
- [5] The FET methodologies can be divided into two main groups: the field bubble extraction technique (FBET) and passive diffusion technique (PDT). The FBET and the BET are based on the same principle but, in the former, the gas extraction is performed in situ [*Tonani*, 1971; *Chapelle et al.*, 1997; *Kampbell et al.*, 1998]. The PDT is based on

the use of semipermeable membranes, which are generally in the form of a polydimetylsilicone (PDMS) tubes. Passive diffusion samplers, consisting of a copper tube sealed at one end and connected to a sealed silicone tube at the other, have been developed by Sanford et al. [1996]. The samplers are dipped in water for a sufficient period of time in order to re-equilibrate the sampler headspace via permeation through the silicone tube. When complete re-equilibration has been reached, the samplers are removed and closed by crimping. Jacinthe and Groffman [2001] have developed another PDT device, consisting of a PVC pipe with internal PDMS tube. The water flows into the space between the pipe and the PDMS tube and the dissolved gases permeate through the PDMS tube. Takahata et al. [1997] assembled an apparatus for the continuous monitoring of dissolved noble gases in water which were then analyzed using a Quadrupole Mass Spectrometer with a remote controller. The gas separation is performed in situ, by a semipermeable polypropylene film membrane, located at the head of a sampling probe and dipped into water. As suggested by these authors, the separation is performed by evacuating the inside of the tubing slowly.

- [6] A field VET, consisting of a glass bottle (preevacuated) which is partially filled with a water sample, has been performed by *Chiodini* [1996]. According to Henry's law, the gases partitioned between the gas and the liquid phase and the total amount of single dissolved gas is recalculated with known volumes of the liquid and gas phases and the chemical composition of the gas phase.
- [7] A comparison of the aforementioned methods suggests some general considerations. The most important shortcoming of LETs regards the collecting and handling of the water sample; this can involve several random accidents, such as the partial out gassing of dissolved gases and/or sample contamination with air micro-bubbles. The FETs necessitate more time spent in the field but they supply gas samples that do not require further laboratory equilibration. Otherwise, the FETs cannot generally furnish the total pressure of dissolved gases (TDGP) but only gas concentrations. In order to solve these disadvantages, Manning et al. [2000] have recently coupled Sanford's method with a TDGP probe. Despite the numerous methods developed, it is necessary to collect more samples by different techniques in order to perform the chemical and isotopic analyses of dissolved gases.

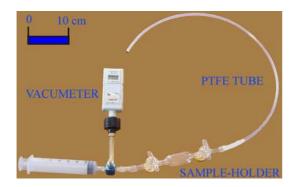


Figure 1. Sampling device and vacuum system control. The PTFE tube is sealed at one end and connected to the sample holder at the other end. The syringe is used to evacuate the system. The function of the vacumeter is to control the evacuation process of the sampling device before dipping it in natural waters.

[8] This paper describes a new in situ method (FET-PDT), using a polymeric semipermeable membrane, for extracting the dissolved gaseous phase from natural waters. The method consists of a very simple sampling device and a mathematical model to recalculate the gas partial pressures at equilibrium by less than fully equilibrated samples. Furthermore, this method provides a unique gas sample for chemical and isotopic analyses. Another significant advance of the proposed method is the capability to collect an in situ sample of dissolved gases from deep wells without a pump. Such wells are the best places to effect a periodical and continuous monitoring of dissolved gases, with the aim of volcano surveillance. Furthermore, this method enables a concentration profile of lakes, seas and rivers to be easily performed. This paper also shows the results of a field application of the new method in an active volcanic area (Vulcano Island, southern Italy).

2. Method and Materials

2.1. Analytical Procedure

[9] The dissolved gases (O₂, N₂, CH₄ and CO₂) were analyzed by gas chromatography (G.C.) Perkin-Elmer mod. 8500, equipped with 4-m carbosieve II columns, hot wire and flame ionization detectors; Ar was the carrier gas and the instrumental precision of the G.C. was ±3%. In order to measure the quantity of noble gases, gas samples were purified in a high-vacuum line equipped with a charcoal trap, a cold trap and getter pumps. The first purified fraction, consisting of He and Ne, was analyzed using a quadrupole mass spectrometer

(QMS, VG Quartz). Finally, the He was totally isolated and analyzed with a static vacuum mass spectrometer MS (VG-5400TFT, VG Isotopes), which had been specifically modified to simultaneously detect 3 He and 4 He ion beams. The 3 He/ 4 He ratio was determined by measuring 3 He with a Daly electron multiplier detector, and 4 He with a Faraday cup detector. The results have been reported as R/Ra values (R is the ratio of 3 He/ 4 He in the sample and Ra is the ratio of 3 He/ 4 He in air = $1.39 \cdot 10^{-6}$ [Ozima and Podosek, 2002]).

2.2. Extraction Procedure

[10] In order to effectively extract dissolved gases from the liquid phases, the separation membranes would have to be characterized by the following fundamental properties: being waterproof, stiff, and chemically and biologically inactive. These properties are common in the solid synthetic polymeric membrane group. In such polymers, the gas permeation is essentially confined to the amorphous regions while the crystalline regions represent tortuous impediments to gas permeation but they confer good mechanical proprieties to the polymer. In general, the gas permeation rate is inversely proportional to its mechanical properties.

[11] The method described in this paper is based on the use of a membrane made of polytetrafluro-ethylene (PTFE). This material was selected because it represents the best compromise between gas permeation rates and mechanical and chemical properties. The high crystallinity confers stiffness and high tolerance to PTFE, which is sufficient to bear mechanical stress. Furthermore, PTFE resists bacterial growth and every known chemical agent or solvent at low and high temperatures (PTFE melting point = 327°C, useful temperature up to 260°C).

[12] The sampling device used for extracting dissolved gases in natural water consists of a PTFE tube connected to a glass sample holder with two stopcocks (Figure 1). The PTFE tube is a semipermeable membrane, which allows the permeation of gas inside the system, while the glass sample holder stores the extracted gases. Before use, the device is evacuated, using a syringe, and dipped into water (wells, springs, lakes or rivers). Throughout the immersion period, the stopcock between the semipermeable membrane and the glass sample holder is left open. After an established exchange time, when equilibrium has been totally or partially reached, the stopcock is closed in order to isolate the extracted gases inside the sample holder and

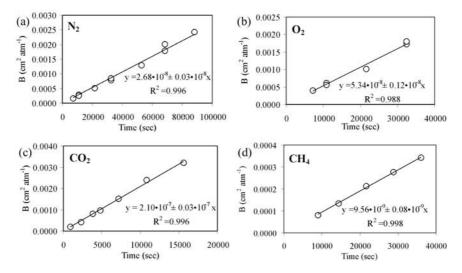


Figure 2. Determination of the Kp PTFE (a) nitrogen, (b) oxygen, (c) carbon dioxide, and (d) methane. Each linear best fit represented the Kp of the *i*th gas species (see text). The variation in time range on the graphs depends on the different equilibration time. The N_2 data range over 100,000 seconds and the O_2 data range over 40,000 seconds because, after this period, the O_2 has reached equilibrium and no further variation in O_2 partial pressure was recorded.

prevent diffusion phenomena through the membrane after the device has been removed from the water.

2.3. Theoretical Model

[13] Gas transport through a dense nonporous membrane, such as PTFE, can be described by the Solution-Diffusion Model [Barrer, 1934; Van Amerongen, 1946; Wijmans and Baker, 1995], according to which the gas on the high-pressure side of the membrane dissolves in the membrane body and, due to a concentration gradient, diffuses toward the low-pressure side of the same membrane, where the gas is finally desorbed. The law governing the flux through the membrane is

$$J_{i} = K_{p} \frac{\Delta p}{h}, \tag{1}$$

where J_i is the flux (cm³ STP cm⁻² sec⁻¹), Kp is the permeability coefficient (cm³ STP cm⁻¹sec⁻¹atm⁻¹), ΔP is the pressure difference (atm) and h is the membrane thickness (cm).

[14] The mass balance, given by the continuity equation, is

$$dM(t) = VdP_i(t) = J_i \cdot A \cdot dt, \tag{2}$$

where V is the internal volume of the device, P_i is the partial pressure of gas inside the device, J_i is the gas flux, referring to a unity surface, of the species

permeating through the membrane and A is the membrane surface. Combining equations (1) and (2), the following equation is obtained:

$$VdP_{i}(t) = K_{p} \times A \frac{P_{a} - P_{i}(t)}{h} dt, \tag{3}$$

which has the solution

$$P_i(t) = P_a + a \cdot e^{-\frac{K_p \cdot A}{Vh}t}, \tag{4} \label{eq:4}$$

where $P_i(t)$ is the partial pressure of the *i*th gas at time t inside the sampling device, P_a is the partial pressure of *i*th gas dissolved in the water and a is a constant which depends on initial system conditions. If, at time t=0, the initial partial pressure (P_{in}) of the *i*th gas inside the device is zero $(P_i(0) = P_{in} = 0)$, a is equal to $-P_a$ and equation (4) becomes

$$P_{i}(t) = P_{a} \left(1 - e^{-\frac{K_{p} \cdot A}{Vh} t} \right), \tag{5}$$

and according to Dalton's law,

$$P_i(t) {=} (\chi_a \cdot P_t) \cdot \left(1 - e^{-\frac{K_P \cdot A}{Vh}t}\right). \tag{6} \label{eq:pi}$$

If $P_i(0) = P_{in} \neq 0$, $a = P_{in} - P_a$, equation (4) becomes

$$P_i(t) = P_a + (P_{in} - P_a) \cdot e^{-\frac{K_p \cdot A}{Vh}t}. \eqno(7)$$



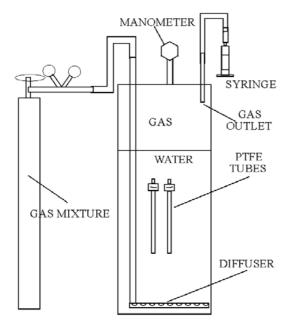


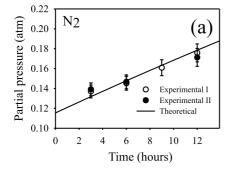
Figure 3. Sketch of apparatus used to compute the Kp of PTFE. The gas mixture was dissolved in water by the diffuser. In order to rigorously check the equilibrium partial pressure, a syringe was used to collect a sample of the equilibrated gas phase over water.

The above equations describe the time variation in the partial pressure of the *i*th gas species inside the device under different initial conditions.

2.4. Experimental Parameters

[15] In order to use the above equations, the geometric characteristics of the device and the PTFE permeability coefficients (Kp) for each gas species must be known. The cylinder radius and wall-thickness were directly measured while the Kp values were experimentally determined from the theoretical model. Rearranging the general equation (5), we have

$$\left[\ln P_a - \ln(P_a - P_i)\right] \cdot \frac{Vh}{A} = K_p t \tag{8}$$



and setting

$$B = \left[\ln P_a - \ln(P_a - P_i)\right] \cdot \frac{Vh}{A}$$

$$B = K_n t$$
(9)

The Kp values were determined from equation (9) by calculating the angular coefficient of the best fitting line for all the data (Figure 2).

[16] The Kp values for nitrogen and oxygen were calculated by assembling a simple device, consisting of a PTFE tube closed at one end and connected to a three-way stopcock at the other end. The device was dipped into a thermostat bath filled with air-saturated water (ASW) and left there for different time periods. Initially, the gas partial pressure of the atmospheric gases (N2 and O2) inside the PTFE tubes was equal to zero because each tube was filled with argon at atmospheric pressure. Pi(t) was measured for seven different extraction time periods and, in some cases, two tubes were used at the same time under the same boundary conditions to verify experimental reproducibility. All the tests were carried out at 1 atm at a temperature of 24°C and no significant variations in the main atmospheric parameters (temperature and pressure) occurred during all the experiments. The gaseous phases inside the PTFE tubes were analyzed with the G.C. and the measured values are shown in Figures 2a and 2b.

[17] The determination of the Kp values for CH₄ and CO₂ were performed by using the same device in a special system, which consisted of an exchanging bath and gas diffuser (Figure 3). The diffuser was connected to a tank containing a gas mixture of known composition. In order to effect a rigorous control on equilibrium partial pressure (P_a) during the tests, the gas phase inside the system was monitored by periodic sampling and analyses. The results of the experiments have been illustrated

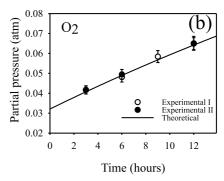


Figure 4. Comparison between theoretical (line) and experimental partial pressures (open and solid circles): (a) nitrogen and (b) oxygen. The error bar in each point indicates the instrumental precision $(\pm 3\%)$.



Table 1.	Partial Pressure of	`Atmospheric	Gases	Inside 1	Devices of	of Different	PTFE To	abe Lengths

Sample	PiO ₂ , a atm	PiN ₂ , atm	PaO ₂ , ^b atm	PaN ₂ , atm	Pin, atm	L, cm
1	0.08	0.29	0.14	0.78	0.121	40
2	0.08	0.27	0.14	0.79	0.090	40
3	0.09	0.39	0.13	0.78	0.090	90
4	0.10	0.40	0.13	0.77	0.121	90
5	0.11	0.47	0.13	0.78	0.121	140

^a P_i is the partial pressure of atmospheric gases inside devices after 71 hours.

in Figures 2c and 2d. The Kp value for He was computed by two experiments, with a partial equilibrium pressure equal to $5 \cdot 10^{-4}$ atm, directly using equation (9): Kp $_{\text{Helium}} = 2.6 \cdot 10^{-7} \text{ cm}^3 \text{ STP cm}^{-1} \text{ atm}^{-1} \text{ sec}^{-1}$.

2.5. Recalculation Method

[18] A theoretical method, recalculation method (R.M.), for calculating the gas partial pressures in equilibrium with the water from the disequilibrium experimental data was elaborated, starting from the theoretical model. From equation (7), which describes the concentration variation inside the system, it follows that

$$P_{i}(t) = P_{a} + P_{in}e^{-\frac{K_{p} \cdot A}{Vh}t} - P_{a}e^{-\frac{K_{p} \cdot A}{Vh}t}$$

$$P_{i}(t) = P_{a}\left(1 - e^{-\frac{K_{p} \cdot A}{Vh}t}\right) + P_{in}e^{-\frac{K_{p} \cdot A}{Vh}t}$$

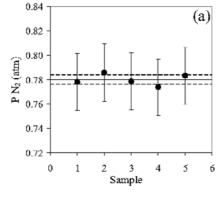
$$P_{a} = \frac{P_{i}(t) - P_{in}e^{-\frac{K_{p} \cdot A}{Vh}t}}{1 - e^{-\frac{K_{p} \cdot A}{Vh}t}}$$
(10)

This final equation allows us calculate the real equilibrium pressure of the dissolved gases in water, knowing the partial pressure of the *i*th gas

species inside the sample holder after the exchange time (P_i) , the initial partial pressure of the *i*th gas species (P_{in}) and the exchange time (t).

3. Laboratory Tests

[19] In order to verify the theoretical model and reliability of the recalculation method, several tests were performed in the laboratory. The main objective of the first test was to obtain experimental data regarding the time variation in the partial pressure of the atmospheric gases inside the sampling device. Eight sampling devices, assembled with glass sample-holders and a PTFE tube with the same geometric characteristics, were placed in ASW. The initial partial pressure inside each device was equal to 0.148 atm. At four different time intervals (3, 6, 9 and 12 hours), two sampling devices were removed and the gas composition was analyzed using the G.C. Figures 4a and 4b show the comparison between the theoretical model and experimental data. The close agreement between the two sets of data sets confirms the reliability of the theoretical model.



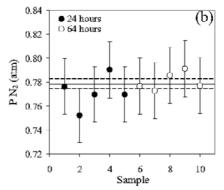


Figure 5. Values of N_2 partial pressure, computed by the recalculation model from the values of N_2 partial pressure inside (a) five sampling devices dipped in ASW for 71 hours and (b) ten sampling devices in ASW after 24 hours (solid circles) and 64 hours (open circles), respectively. In both figures the solid line represents the equilibrium N_2 partial pressure, the dashed lines define the analytical uncertainty of the barometric pressure (0.005 atm), and the error bar in each point indicates instrumental precision ($\pm 3\%$).

^bP_a is the computed partial pressure according to recalculation model.



Table 2. He Isotope Reproducibility Tests

Sample	Time, hours	R/Ra
ASW1	12	0.97 ± 0.05
ASW2	24	1.00 ± 0.04
ASW3	24	1.06 ± 0.06
ASW4	24	0.99 ± 0.06

[20] The devices used in the second test comprised five equal sample-holders joined to PTFE tubes of three different lengths (40, 90 and 140 cm). The initial gas pressure inside the devices ranged from 0.09 to 0.121 atm of air. The devices were dipped in ASW for 71 hours, then the N₂ and O₂ contents were determined by the G.C. As predicted by the theoretical model, the pressures inside the sample-holder were proportional to the length of the PTFE tubes (Table 1). This indicated that 71 hours of exchange time were not sufficient to reach total equilibrium between the dissolved and separated gas phase. Therefore the values were processed in accordance with equation (10). Regarding the nitrogen content, the recalculated values were equal to the partial atmospheric pressure (Figure 5a) with a maximum discrepancy equal to ± 0.006 atm, smaller than the instrumental uncertainty (±0.023 atm). The recalculated partial pressures for oxygen were lower than its common value for air-saturated water because the tests were carried out in water where

oxygen had been consumed in bacterial processes. However, the data are characterized by a low uncertainty, which is equal to 0.005 atm.

[21] A third test was carried out using sampling devices with tubes of the same length. Five devices were left in ASW for 24 hours and a second set of five devices were left for 64 hours. The variation in atmospheric pressure was measured throughout the experiment with a mean value equal to $0.998 \pm$ 0.005 atm. The analytical uncertainty, expressed by standard deviation (σ_x) , was computed by the square root of the variance of the set (σ_x^2) [Taylor, 1982], and this equaled ± 0.011 atm for the nitrogen and ± 0.007 atm for the oxygen. Precision, expressed as relative uncertainty, was computed by a standard deviation of the set and divided by the average of the set; it was found to be 1.5% for N_2 and 3.7% for O_2 . The "true value" for N_2 partial pressure was calculated by the product of measured barometric pressure (0.998 atm), for the N_2 molar fraction in the atmosphere (0.78), and resulted equal to 0.778 atm. Therefore the method accuracy for N2 was determined compared this "true value" with the average over the set (the so-called "best value"). The results for nitrogen, summarized in Figure 5b, suggest that the methodology is characterized by good precision and reproducibility, since the computed nitrogen partial pressures are very close to the "true value."

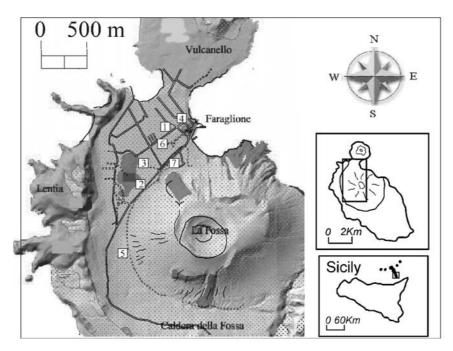


Figure 6. Location of sampling wells on Vulcano Island: 1, Bambara; 2, C. Sicilia; 3, Le Calette; 4, Castello; 5, Discarica; 6, Casmento; 7, Rifici. The numbers are the same as those in Table 3.



Table 3. Physicochemical Parameters of Waters and Chemical Composition of Dissolved Gases From Vulcano Wells

Number ^a	Sample	Date	T, °C	рН	Cond., mS cm ⁻¹	Eh, mV	N ₂ , atm	O ₂ , atm	CO ₂ , atm	$CH_4 \cdot 10^4$, atm	PT, atm
1	Bambara	May 2003	25.7	5.68	1.6	153	0.22	0.02	0.77	0.92	1.01
2	C. Sicilia	May 2003	53.6	6.04	2.5	140	0.69	0.03	0.01	1.89	0.72
2	C. Sicilia	May 2003	53.6	6.04	2.5	140	0.71	0.03	0.01	2.24	0.75
3	Le Calette	May 2003	31.9	n.d	n.d	n.d	0.96	0.13	0.02	≤02	1.12
4	Castello	May 2003	49.7	5.7	39.7	-206	0.07	0.00	0.90	<u>≤</u> 02	0.97
5	Discarica	May 2003	49.4	6.60	4.29	-136	0.21	0.03	0.70	2.20	0.94
6	Casamento	May 2003	24.7	6.77	1.89	50	0.78	0.14	0.15	≤02	1.08
6	Casamento	May 2003	24.7	6.77	1.89	50	0.81	0.17	0.18	≤02	1.16
7	Rifici	May 2003	28.2	n.d	n.d	n.d	0.77	0.17	0.01	≤02	0.95
1	Bambara	July 2003	28.2	5.67	1.64	239	0.36	0.03	0.81	1.36	1.20
2	C. Sicilia	July 2003	53.6	7.70	8.4	162	0.64	0.02	0.01	1.31	0.67
3	Le Calette	July 2003	32.3	n.d	n.d	n.d	0.88	0.04	0.12	0.27	1.04
4	Castello	July 2003	50.2	5.82	37.1	-198	0.29	0.03	0.89	1.28	1.21
5	Discarica	July 2003	48.8	6.60	4.42	-39	0.14	0.00	0.75	2.76	0.89
5	Discarica	July 2003	48.8	6.60	4.42	-39	0.15	0.00	0.75	3.30	0.91
6	Casamento	July 2003	27.0	5.97	1.98	227	0.55	0.09	0.30	2.93	0.94
6	Casamento	July 2003	27.0	5.97	1.98	227	0.57	0.09	0.30	2.70	0.96

^a The numbers correspond to the well locations shown in Figure 6. The consecutive equal numbers refer to two samples collected in the same well at the same time.

[22] Owing to the high PTFE permeability of He, its equilibration time is fast. Regarding the geometric characteristics of the sampling devices used in this test, the He equilibration time was approximately 24 hours; after this time, all kinetic fractioning process should cease. The accuracy of the method for He isotopic composition was also tested, following the aforementioned procedure. Table 2 shows the results expressed as R/Ra value. All the samples provide a value of R/Ra which is very close to 1 (the value belonging to the atmospheric helium source). This result confirms the absence of any kinetic fractionation process at least for 12 hours, and confirms reliable reproducibility of the method for the helium isotope.

4. Field Application

[23] This method was applied to a volcanic context (Vulcano Island) where the circulating groundwater interacts with fluids of different natures [Tedesco and Nagao, 1996; Capasso et al., 1997, 2001; Cortecci et al., 2001]. Vulcano Island is the southernmost volcanic island in the Aeolian archipelago, located in the southern Tyrrhenian Sea (southern Italy) off the north coast of Sicily (Italy). The evolution of these volcanic islands is linked to the presence of an active crustal discontinuity [Ventura, 1994], corresponding to the NNW-SSE-trending dextral strike-slip fault system which is named Tindari-Letojanni [Ghisetti, 1979], a continuation of the Malta Escarpment. According to Favara et al. [1997], the Vulcano Porto phreatic

aquifer is fed by groundwater which mainly comes from the Vulcano Piano area in the southern part of the island at about 400 m elevation a.s.l., and subordinately from the volcanic cone. The aquifer rock permeability is high, as supported by rapid drainage in the underground of heavy rains and the quick restoration of the static level in the wells after exploitation. There are four main groups of groundwater on Vulcano island [Bolognesi and D'Amore, 1993; Aiuppa et al., 2000]. Seven wells on the island (Figure 6) were selected on the basis of their chemical composition, which represents all water groups: (1) Le Calette, Discarica and Bambara (bicarbonate waters, warmer and saline rich);

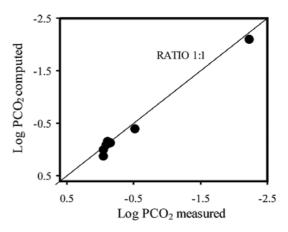


Figure 7. Comparison between the log of CO₂ partial pressure values, measured by the new method and calculated by PHREEQC computer code for the samples collected in May and July 2003 from Vulcano wells.

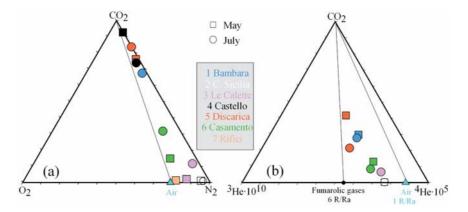


Figure 8. (a) O_2 - CO_2 - N_2 triangular plot. The point relating to air composition (the triangle) and the line with N_2/O_2 atmospheric ratio are also shown. (b) CO_2 and He isotope triangular plot. The point relating to R/Ra of air (R/Ra = 1) and fumarolic gas from crater (R/Ra = 6) are also shown. Both plots highlight the mixing phenomena between the atmospheric gases and gases of deep and/or radiogenic origin.

Casamento (bicarbonate water, hypothermal and diluted); (2) C. Sicilia (chloride-sulfate groundwater); (3) Castello (chloride-rich water); (4) Rifici (SO₄-rich waters or steam-heated groundwater).

[24] In order to investigate both the spatial and time variations in the dissolved gas phase, the wells were sampled in May and July 2003, by using devices with PTFE tubes which were 90 cm in length. The devices were pre-evacuated and dipped into the wells for approximately 24 hours. Table 3 shows the physicochemical parameters of the waters and the chemical composition of dissolved gases. In some wells two samples were collected simultaneously and this shows that the method has good reproducibility in the field. In order to further investigate the applicability of the method, the CO₂ partial pressure values, which had been measured by the proposed method, were compared with the values calculated by the PHREEQC computer code [Parkhurst, 1995], using the chemical composition of the waters. As suggested by Figure 7, an acceptable concordance was found to exist between two data sets.

[25] The dissolved gases in the groundwater of Volcano Island can be interpreted as a mixture of two components, one atmospheric and the other CO₂-rich of deep origin. This mixing is clearly highlighted by the O₂-CO₂-N₂ triangular plot (Figure 8a) where the samples are aligned along a mixing line between atmospheric gases and a CO₂-rich member. Furthermore, all the samples have a N₂/O₂ ratio which is higher than the atmospheric one. This distribution could be due to two main processes: the organic and inorganic consumptions of O₂ and/or the presence of a deep N₂ component. The presence of deep nitrogen flux in a volcanic context is well documented, e.g., in island arc fluids, Sano et al. [2001] has recognized three nitrogen components: mantle-derived, sedimentary and atmospheric. Figure 8b shows the CO₂, ³He and ⁴He triangular plot, where the helium concentrations also include the air component. Two

Table 4. Helium Data^a

Sample	Date	R/Ra	4 He/ 20 Ne	R/Ra c	PHe10 ⁵ , atm
Bambara	May 03	3.41	2.347	3.83	1.06
C. Sicilia	May 03	2.21	0.654	3.61	1.37
Discarica	May 03	4.82	1.992	5.60	0.48
Casamento	May 03	2.59	1.134	3.32	0.85
Bambara	July 03	3.69	3.531	3.98	1.23
C. Sicilia	July 03	2.20	0.564	4.11	1.26
Discarica	July 03	5.26	4.937	5.58	1.33
Casamento	July 03	2.97	1.498	3.58	1.99
Le Calette	July 03	2.23	0.621	3.81	1.09

^a The R/Ra, corrected with respect to atmospheric gases denoted as R/Ra c, was computed using the atmospheric ²⁰Ne concentration, according to *Polyak* [2003].

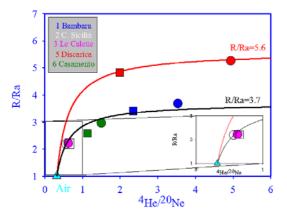


Figure 9. Correlation diagram R/Ra versus ${}^4\text{He}/{}^{20}\text{Ne}$. The curves show a mixing between air and two endmembers with R/Ra = 3.7 (black line) and R/Ra = 5.6 (red line). The sample distributions testify to the presence of both magmatic and radiogenic helium in the dissolved gases. The samples from the Discarica well seem to be less contaminated by the radiogenic component, given that it follows the red line.

lines, linking the vertex of CO₂ with two isotopic ratios, R/Ra = 1 and R/Ra = 6, are also traced. The first R/Ra value represents the atmospheric source while the second is the R/Ra value, which was measured in the fumarolic gases from La Fossa Crater [Italiano and Nuccio, 1996]. All the samples fall between two straight lines, thereby reflecting a mixing process between a deep member, which is rich in CO₂ and ³He, and the atmosphere. The differences in the He isotopic ratio (Table 4) can be ascribed to different mixing percentages between "deep" end-members and atmospheric ones. The ⁴He/²⁰Ne ratio in the atmosphere is well known and constant. Assuming an end-member with R/Ra= 1 and ⁴He/²⁰Ne_{atm.} it is therefore possible to derive mixing curves between end-members with various R/Ra and the atmospheric one. From Figure 9, the presence of mixing processes between atmospheric gases and two end-members with an R/Ra equal to 3.7 and 5.6 respectively is evident. The last R/Ra value is very close to the value of gases emitted from La Fossa Crater fumaroles [Italiano and Nuccio, 1996; Tedesco and Nagao, 1996]. The other R/Ra value is likely to be indicative of the contamination of the deep component with a radiogenic helium source (⁴He). The presence of a radiogenic helium component in fluids emitted in volcanic areas is rather common. Generally, ⁴He is linked to rock with high concentrations of radiogenic elements like U and Th. These elements are enriched in the last phases of crystallization so acid rocks bear higher concentrations of these elements. These types of rocks are widely outcropping on Vulcano island. Moreover, the elevated presence of radiogenic components has also been highlighted by various studies on γ_{ray} emission in the Aeolian archipelago [Brai et al., 1995; Chiozzi et al., 2001] and on the trace element contents in the groundwaters of Vulcano [Aiuppa et al., 2000]. The latter study highlights the presence of intense leaching processes in rocks which are rich in radiogenic elements in this area.

4.1. Temporal Variations

[26] The helium data demonstrate the most meaningful time variations. In order to clarify the behavior of dissolved helium, the percentage of different components of dissolved helium was computed (Table 5). The triangular plot in Figure 10 shows the differences between the two temporal sets. Excluding the C. Sicilia well, the amount of deep helium increased from May to July in all the other samples. These data also highlighted an increase in radiogenic helium. On the contrary, the dissolved gases from C. Sicilia showed an increase in the atmospheric component between May and July, even if the R/Ra value remained constant. This unusual condition can be explained by a con-

Table 5. Percentages of Different Helium Components^a

		F		
Sample	Date	% atm	% rad	% Deep
Bambara	May 03	14.8	30.9	54.3
Bambara	July 03	9.7	30.4	59.8
C. Sicilia	May 03	53.6	18.5	27.9
C. Sicilia	July 03	61.4	12.2	26.4
Casamento	May 03	31.5	30.7	37.9
Casamento	July 03	23.6	30.8	45.5
Discarica	May 03	17.0	5.5	77.5
Discarica	July 03	7.0	6.5	86.5
Le Calette	July 03	56.2	16.0	27.8

^a In order to compute the He components, the value R/Ra = 0.01 was used as a radiogenic end-member [Mamyrin and Tolstikhin, 1984], and R/Ra = 6 as a magmatic value [Italiano and Nuccio, 1996].

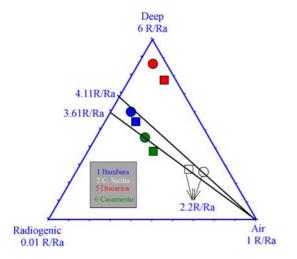


Figure 10. Variations between May (squares) and July (circles) of the helium components in Vulcano groundwater. The July samples have been shifted toward the side of nonatmospheric components, excluding C. Sicilia samples. Notwithstanding the increase in the air component in this well, the value of R/Ra remained constant (2.2 R/Ra) between May and July because the value of corrected R/Ra increased from 3.61 to 4.11, as shown on the left-hand side of the triangle. The graphic feature indicated an input of helium of deep origin.

comitant input of deep ³He, as confirmed by an increase in Ra/Ra_c (R/Ra corrected by the atmospheric component) from 3.6 to 4.1; in short, the increase in the atmospheric component diluted the input of deep ³He in this well. The deep input is also indicated by an increase in CO₂ partial pressure.

[27] As has been well documented by several authors [Carapezza et al., 1980; Capasso et al., 1991; Bolognesi, 2000], both seismic and volcanic activities can determine time variations in the chemical and isotopic composition of the fluids emitted in this area. The time variations in the Helium isotopic composition and CO₂ contents may also be linked to a seismic event of magnitude 3.0 which occurred 24h prior to the second sampling survey, a few miles north of the island.

5. Conclusion

[28] In this paper a polymeric membrane made of PTFE, gas-permeable and waterproof, was used to separate the dissolved gaseous phase from water. The processes involved in the permeation of gas through the PTFE were modeled according to the "Solution-Diffusion Model." Commencing with

this model and applying a mass balance, a theoretical model were developed. The equations of the model related the partial pressure inside the device at any time with the equilibrium partial pressure of dissolved gases.

[29] A new sampling device was developed, which is constituted by two interconnected parts, a glass sample-holder (where the gas sample is preserved) and a semipermeable membrane, where the gas can permeate into the device. The theoretical model was used to elaborate a mathematical method to recalculate (R.M.) the equilibrium partial pressure of each gaseous species inside the sampling device, using the composition of gas that still had not reached equilibrium. Experimental data of partial pressure variations with time inside the device were obtained, and a comparison between theoretical and experimental data gave very good results. Furthermore, several laboratory tests have highlighted the accuracy and precision of the methodology proposed in this paper.

[30] This method was applied to a volcanic area (Vulcano Island) from which several samples of dissolved gases were collected and each of them analyzed for both chemical and isotopic composition. The composition of dissolved gases in the analyzed wells highlighted their origin and this could be explained as the mixing of almost three different components: the first comprises atmospheric gases, the second derives from a deep magmatic reservoir and the final component is of crustal origin. Finally, temporal variations in chemical and isotopic composition were recorded and they seem to be related to an earthquake (M = 3) which occurred very close to the island 24h hour prior to the July sampling survey.

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