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EFFECT OF DIFFERENT AQUEOUS SOLUTIONS OF PURE SALTS AND SALT MIXTURES IN REVERSE ELECTRODIALYSIS SYSTEMS FOR CLOSED-LOOP APPLICATIONS

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Abstract

Reverse Electrodialysis (RED) in a closed-loop arrangement is a viable way to convert low-grade heat into electric power. The present work experimentally investigates the use of pure salt- and equimolar two salts-water solutions as feeds in a lab-scale RED unit. RED performances were analyzed in terms of Open Circuit Voltage (OCV), stack resistance and corrected power density. The pure salts and the mixtures employed were chosen via a computational analysis. Effect of feed solution velocity and concentration was investigated. Results concerning the pure salt-water experiments show that NH4Cl is the most performing salt in the concentration range probed, while higher power density values are expected with the use of LiCl at larger concentrations. As regards the salt binary mixtures, in some cases, the measured stack electrical resistance was found lower than both the two values measured for the corresponding pure salts, thus resulting into higher power density values for the mixtures. This surprising experimental evidence suggests that it is possible to increase the power produced by a conventional RED unit by adding an equivalent molar quantity of another suitable salt. Finally, among the mixtures tested, the NH₄Cl-LiCl mixture appears as the most promising, thanks to the combination of the favorable properties of these two salts.

Keywords:

Reverse Electrodialysis Heat Engine; Closed loop RED; Salt mixture; Salinity Gradient Power

1. INTRODUCTION

The continuous growth of the energy demand is giving impulse to the search and the development of new renewable energy sources. Among these, the energy deriving from salinity gradients (i.e. Salinity Gradient Power, SGP) represents a promising option [1]. This form of energy is available whenever two solutions at different concentration are put in contact and is progressively dissipated while the two solutions are naturally mixing together. Performing a "*controlled mixing*" between the two solutions to convert the chemical potential difference into available power is the goal of all the SGP technologies [2]. Among these, Pressure Retarded Osmosis (PRO) and Reverse Electrodialysis (RED) have reached the highest technology readiness level and are currently the most investigated [3].

Pressure Retarded Osmosis is based on the use of osmotic membranes to convert the salinity gradient energy into mechanical power [4–6], while Reverse Electrodialysis makes use of ionic exchange membranes (IEMs) to allow a direct conversion into electric power. More in detail, a RED stack is composed of a number of repeating units named cell pairs constituted by a cationic exchange membrane, a channel fed by the dilute stream, an anionic exchange membranes and a channel fed by the concentrate solution. The chemical potential difference between the adjacent channels along with the presence of the two types of IEMs results into the spontaneous generation of separate ion fluxes: one positive and the other negative directed towards opposite directions. These are directly converted into electric current via red-ox reactions occurring at the end compartments of the unit where two electrodes are hosted.

The properties of IEMs represent one of the most crucial aspects affecting the performance of a RED unit [7]: the perm-selectivity (i.e. transport selective property) of an IEM towards its counter-ion dramatically affects the process driving force [8], while the IEM electrical resistance may significantly reduce the producible power [9] as it often represents the highest contribution to the stack resistance [10]. These two properties are affected by the swelling degree and the ion exchange capacity of the membrane, the first is a measure of the increase of the membrane volume in presence of a solution and the second represents the number of fixed charges per unit volume of dry membrane.

RED has been traditionally studied as a viable way to exploit either naturally existing salinity gradients as river estuaries [11] or artificial gradients based on the use of industrial brines as those deriving from desalination plants [12] or saltworks [13]. In both cases, almost all studies have focused on the use of aqueous solutions with sodium-chloride as the main (or only) solute. IEMs have been progressively studied and developed in order to enhance their performance and capability to efficiently deal with this kind of solutions.

As an alternative to its traditional application, very recently, RED has been studied as a viable way to convert low-grade waste heat into electrical power by taking advantage of a closed-loop configuration [1,14]. The RED Heat Engine (REDHE) [15,16] is mainly composed of a RED stack and of a regeneration unit (Figure 1): the RED stack is devoted to converting the salinity gradient into electric power by mixing the two solutions at different concentration, while the regeneration unit makes use of unworthy thermal power (temperature lower than 100°C) to separate them and restore the initial salinity gradient.

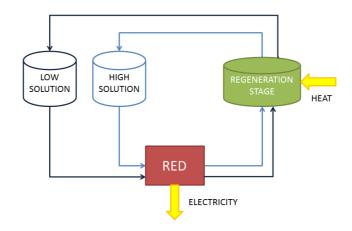


Figure 1. Reverse Electrodialysis Heat Engine concept [15].

Within the above closed-loop arrangement, it is not anymore necessary to locate the plant close to estuaries or industries producing brines, thus guaranteeing a higher versatility and flexibility of RED technology. More important, this application also allows the use of artificial solutions composed of any solvent-solute couple with the scope of maximizing the cycle efficiency. For instance, salts besides NaCl or mixtures of two or more salts may be used to generate and exploit a higher theoretical potential difference. Moreover, operating conditions in terms of solution concentration and velocity are no more dependent on the available stream but can be easily tuned to maximize the REDHE performance. The investigation of RED units fed by non-conventional (i.e. NaCl-water) solutions is nowadays a topic of crucial importance.

Surprisingly, only a very few studies have been presented so far on the use of a RED unit fed with salts other than NaCl. Some of them regard the investigation of the performance of multivalent ions in a RED unit, mainly referring to the most common ions present in seawater (Mg^{2+} , Ca^{2+} and SO_4^{2-}) in order to predict the behaviour of a RED stack fed by natural seawater [17–19]. Other studies concern the use of thermolytic salts, such as ammonium hydrogen carbonate (NH_4HCO_3). These salts are able to decompose into ammonia, carbon dioxide and water at temperatures of about 40-45°C. Thus, they can be used within a salt extraction regeneration strategy [20–22] in a REDHE. Unfortunately, power densities lower than those obtainable with NaCl solutions have been reported [20,23] so far. Other studies focus on the interaction between specific ions and IEMs without investigating the RED process performance: in particular these studies investigate how membrane properties, such as electrical resistance and permselectivity, can be affected by a specific ion [8,24]. For instance,

Cassady et al. [24] demonstrated how the permselectivity is not only influenced by the membrane water content, but also by the strength of the ionic interaction between counter-ion and fixed charge groups. Choi et al. [25] studied the effect of various electrolytes on the transport phenomena across the ionic exchange membranes. Martí-Calatayud et al. [26] investigated the possibility of treating industrial waste-water effluents containing metals via electrodialysis: they showed how the membrane structure and the ions size may influence the competitive ion transport. Other studies deal with the determination of the diffusion coefficient of some counter- and co-ions, in order to understand the transport mechanism through IEMs and to model their internal structure [27].

Summarizing, an insufficient amount of data has been collected so far on the performances of a RED unit fed by non-conventional salt-water solutions including pure and mixture salts. Therefore, the present work aims at filling this gap in the literature by selecting the most promising salts to be fed in a RED unit either as pure salt or together as couple (i.e. binary mixture) and at experimentally measuring the main parameters of a RED unit (fed by these non-conventional solutions) including Open Circuit Voltage (OCV), stack resistance and power density.

2. SELECTION OF THE PURE AND MIXTURE SALTS FOR THE EXPERIMENTAL CAMPAIGN

2.1 Pure salts selection

Firstly, investigations were limited to salts based on monovalent ions as the presence of bivalent ions (e.g. Ca^{2+} , Mg^{2+} and SO_4^{2-}) was found to strongly affect the IEMs performance, thus resulting into a lower power production [17,18,28,29]. As shown in Table 1, a large number of salts based on monovalent ions were included into the selection procedure to identify a few salt-water solutions to be tested in the experimental campaign.

Table 1: Salts formed by monovalent ions included in the selection procedure. Selected salts are reported in bold-red. Chaotrope ions are indicated in bold-blue. Kosmotrope ions are indicated in bold-black [30].

Cations>	Li ⁺	Na ⁺	K +	\mathbf{NH}_{4^+}	Cs ⁺
F Anions					

Cl-	LiCl	NaCl	KCl	NH ₄ Cl	CsCl
NO 3 ^{- (*)}	LiNO ₃	NaNO ₃	KNO ₃	NH ₄ NO ₃	
Br ⁻		NaBr			

(*) These anions are considered as Chaotrope ions since quite similar ions are considered so in the literature.

Table 1 divides the ions into two different groups: kosmotrope ions and chaotrope ions. In principle, chaotrope ions are featured by large ion radius, single charge and consequently low charge density. Conversely, kosmotrope ions are featured by small ion radius or multiple charge and high charge density. Contrary to what is expected on the basis of the ion radius, the chaotrope ions have a higher mobility in water with respect to the kosmotrope ions. This is due to the fact that the actual ion size in water is much different from the one measured in a crystal: small kosmotrope ions are strongly hydrated and they move bearing several water molecules, while large chaotrope ions are less hydrated thus moving much faster than the kosmotrope ones [31,32]. The classification of the ions in the chaotrope or kosmotrope categories is based on the value of the Jone and Dole's viscosity coefficient *s* [30], which is present in the equation for the solution relative viscosity:

$$\frac{\eta}{\eta_0} = r\sqrt{C} + sC \tag{1}$$

where η_0 is pure water viscosity at the same temperature and *r* is a constant independent of the concentration *C*.

The kosmotrope ions tend to increase the solution viscosity, 'making the order' in the water structure, thus, they are featured by a positive value of the coefficient *s*. Conversely, the chaotrope ions 'break the order' in the water structure and cause a decrease of the solution viscosity, thus, their coefficient *s* is a negative value [30]. Just to give some simplified examples, Cl^- , Br^- , NO_3^- , K^+ , NH_4^+ and Cs^+ are generally considered as chaotrope ions, while Li^+ and Na^+ typically belong to the kosmotrope group. Nevertheless, such differences are not always so clear and it is often easier to define which ion is more chaotrope or more kosmotrope than another one, rather than providing an absolute classification: e.g. potassium, lithium and sodium ions can be

ordered as $K^+ < Li^+ < Na^+$ with respect to the kosmotrope properties and in the opposite way with respect to the chaotrope properties.

The salt selection was performed by referring to some properties of the pure salts in water, i.e. (a) *activity coefficients*, (b) *conductivity* and (c) *solubility*.

(a) Activity coefficients have a strong influence on the available potential difference across each membrane and therefore on the voltage generated by the stack. (b) Salt solution conductivity strongly affects the stack resistance (R_{stack}), which is composed of the electrical resistance of the anionic exchange membranes (R_{AEM}) and the cationic exchange membranes (R_{CEM}), the electrical resistance of the dilute and the concentrate compartments (R_{low} and R_{high}) and the blank resistance R_{blank} (i.e. the resistance of the electrodic compartments). The term R_{low} is often so significant in determining R_{stack} that the conductivity of the salt solution flowing in the dilute compartment is one of the most crucial parameters. (c) Salts *solubility* is another important property: the higher the solubility, the higher the achievable concentration of the solution feeding the concentrate compartment (C_{high}), thus, the higher the salinity gradient available.

Increasing the stack voltage via suitable activity coefficients and concentration ratios across the membranes and decreasing R_{stack} via a suitable solution conductivity results into an enhancement of the RED unit power output.

(a) Activity Coefficients

Activity coefficients as a function of the salt molality were evaluated through the Pitzer model for pure salts [33] for the salts in Table 1 and reported in the supplementary information section. The salts including the ion Li⁺, such as LiCl and LiNO₃, practically exhibit the highest activity coefficients at any molality.

Interestingly, combinations between kosmotrope and chaotrope ions (e.g. LiCl, LiNO₃ and NaCl) give rise to salts with higher activity coefficients in water, while salts formed by either two chaotrope (e.g. NH₄Cl, CsCl and NH₄NO₃) or two kosmotrope ions exhibit lower activity coefficients. Moreover, the activity coefficient vs. molality trend is found to exhibit a minimum at low molality for the case of salts given by the combination of chaotrope and kosmotrope ions (see in particular Li⁺ salts). On the contrary, salts given by the combination of two chaotrope ions reveal a monotonically decreasing behaviour in the entire range of molality explored. According to the Nernst potential equation [34] (equation 5 in the supporting information section), the presence of a minimum in the low

concentration range should be regarded as an advantage since the lower the activity of the salt-water solution flowing in the dilute compartment, the higher the resulting electric voltage in the cell pair.

(b) Conductivity

Equivalent conductivity at 25°C was calculated with the Jones and Dole's equation [35], whose coefficients are available for a wide range of salts. The equation and a chart containing the conductivity values for the salts of Table 1 are reported in the supporting information section.

The salts composed of chaotropes ions such as NH₄Cl, KCl and CsCl, exhibit the highest values of conductivity in the entire range of investigated concentrations, while the salts presenting a kosmotrope ion have a much lower conductivity. As a matter of fact, the chaotrope ions are less hydrated and they move faster than the kosmotrope ions, determining a higher conductivity of the electrolyte solution [30]. However, it should be kept in mind that the higher differences are found at high concentrations, while at lower concentrations, and in particular for concentrations lower than 0.5M, the trends are closer to each other.

(c) Solubility

Solubility data were found in database available in the literature [36,37] and are reported in the supporting information section. For the purpose of the present work where both pure salt- and salt binary mixture-solutions have to be tested, such data have been employed just to discard all cases exhibiting solubility in water lower than the NaCl one (which is used as the reference case in this work) and to have an idea of the potential enhancement achievable at the saturation concentration.

Moreover, when the salt saturation point allows to reach higher concentrations, as in the case of LiCl, the corresponding activity coefficients is also greatly enhanced, thus ensuring a further increase of the theoretical cell potential difference.

All the information reported above were used to guide the choice of some pure salt-water solutions to be tested in the experiments. More precisely, on the basis of the activity coefficient along with relevant cell electric potential, the LiCl was considered as the most interesting choice. Similarly, NH₄Cl was judged as the most promising by referring to the solutions conductivity data. NaCl was selected as a reference case as it is the most

used and studied salt in RED systems. Note that the above salts where chosen also because they share the same anion thus reducing the number of parameters involved in results discussion. Moreover, both LiCl and NH₄Cl have a solubility higher than the NaCl case thus not representing a limit in the binary mixture tests (see next section). In particular, the really high solubility of LiCl could represent a breakthrough in RED technology potential, as already suggested for the case of Pressure Retarded Osmosis technology [38]. The salts selected for the experimental campaign are indicated in redbold in Table 1.

2.2 Salt binary mixture selection

This section is devoted to recognizing which combination of two different salts could enhance the process performance. In order to reduce the high number of possible combinations of Table 1 salts, some assumptions were made:

- considering only binary mixtures of salts in water;
- considering only 50%-50% molar salt mixtures, i.e. each mixture is composed of the same molar amount of the two salts;
- considering only mixtures of salts sharing either the same anion or the same cation.

Following the procedure reported for the pure salt selection, similarly, the selection of the binary mixture was again performed by referring to activity coefficients, conductivity and solubility.

(a) Activity coefficients

The activity coefficients of salts in mixture are calculated through the Pitzer model adapted to multicomponent systems [39] which is briefly summarized in the supporting information section.

According to Pitzer's model, the activity coefficient of a pure salt in water is modified when mixed with another salt in the same solution due to interaction forces. In particular, for all the salts (and all possible binary mixtures) tested in the present work, their activity coefficient (γ_{MX}) as pure compound in water, can exhibit either an enhancement or a reduction when mixed with another salt depending on the activity coefficient of the latter ($\gamma_{M'X'}$) as pure compound in water. More precisely, when $\gamma_{MX} < \gamma_{M'X'}$, $\gamma_{MX,mix}$ (activity coefficient of the former in the mixture solution) will be higher than γ_{MX} , while $\gamma_{M'X',mix}$

(activity coefficient of the latter in the mixture solution) will be lower than $\gamma_{M'X'}$. This model outcome is shown in Figure 2 for the case of a 50%-50% mixture of NH₄Cl-LiCl: as it can be observed in the figure, since $\gamma_{NH_4Cl} < \gamma_{LiCl}$, $\gamma_{NH_4Cl,mix} > \gamma_{NH_4Cl}$, while $\gamma_{LiCl,mix} < \gamma_{LiCl}$.

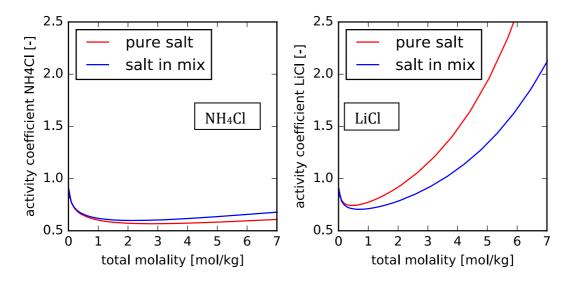


Figure 2. Activity coefficients of NH₄Cl (left) and LiCl (right) in water vs solution molality as pure salts and in 50%-50% NH₄Cl-LiCl mixture.

As already discussed for the pure salt cases, once activity coefficients of ions in water have been calculated, the cell potential difference can be assessed. For binary salt mixtures and ideal membranes (i.e. permselectivity $\alpha_p=1$), the multicomponent Nernst equation reported in [40,41] was derived as follows:

$$\Delta\phi_{cell} = \frac{RT}{2F} \ln\left(\frac{a_{c1}^{high}a_{c2}^{high}a_{a1}^{high}a_{a2}^{high}}{a_{c1}^{low}a_{c2}^{low}a_{a1}^{low}a_{a2}^{low}}\right) = \frac{RT}{F} \ln\left(\frac{a_{salt1}^{high}a_{salt2}^{high}}{a_{salt1}^{low}a_{salt2}^{low}}\right)$$
(2)

where the number 2 visible at the denominator is relevant to the number of salts present in the solution.

Figure 3 shows the ideal cell potential difference calculated (i) for some of the analysed salt binary mixture-water solutions and (ii) for the corresponding pure salt-water solutions at a given operating condition (i.e. $C_{high} = 5M$ and $C_{low} = 0.05M$, T=25°C, $\alpha_p=1$). As expected on the basis of the activity coefficients found for the salts in the mixtures, the mixture- $\Delta \phi_{cell}$ is found to be included in the range between the two pure-

 $\Delta \phi_{cell}$ cases. Notably, in many cases the mixture- $\Delta \phi_{cell}$ results closer to the lowest pure- $\Delta \phi_{cell}$.

However, the salt mixtures with LiCl are shown to provide the highest mixture- $\Delta \phi_{cell}$ thanks to the high γ_{LiCl} as pure salt in water: in particular its mixtures with NH₄Cl and NaCl appear as the most promising among those sharing the same anion.

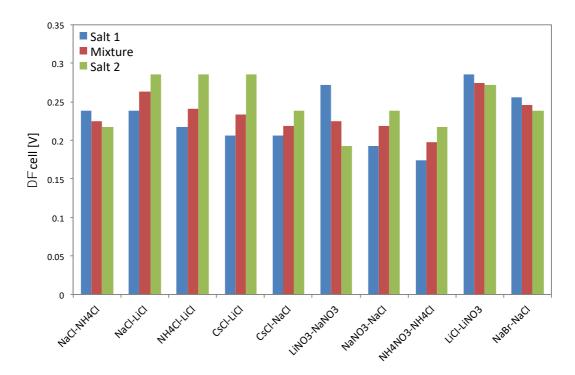


Figure 3. Theoretical cell potential difference values calculated for binary 50%-50% mixture-water solutions and for corresponding pure salt-water solutions ($C_{high} = 5M$; $C_{low} = 0.05M$, ideal membranes: $\alpha_p = 1$).

(b) Conductivity

The conductivity of the two salt-water solutions was measured via some laboratory experiments purposely carried out. As expected, the values were found to be intermediate between the two pure salt-cases. Following this evidence, the solutions including the NH₄Cl are expected to be able to mostly reduce the stack electrical resistance.

(c) Solubility

Given the fact that the salt mixtures investigated include salts sharing either the same anion or the same cation, considerations concerning the solubility strictly follow those already discussed for case of the pure salts: mixtures including salts whose solubility is lower than the NaCl one were discarded in the selection.

On the basis of the findings of this section 2.2 and also following the selection already made for the pure salt-water cases (section 2.1), it was decided to investigate binary mixture composed of the salts selected in section 2.1, i.e. NaCl-LiCl, NaCl-NH₄Cl, NH₄Cl-LiCl.

3. EXPERIMENTAL

3.1. Experimental apparatus

The lab-stack (manufactured and provided by REDstack BV) used for the experiments reported in this work is composed of 5 cell pairs, each one consisting of two channels where the solutions at different concentration are forced to flow. These channels are separated by Fujifilm[®] membranes (E1 type, 250 μ m thick): an anionic exchange membrane (AEM) and a cationic exchange membrane (CEM) whose area is equal to $0.1 \times 0.1 \text{m}^2$. Channel dimensional stability and flow mixing enhancement are guaranteed by woven-spacers 150 μ m thick provided by Deukum[®].

The experimental apparatus (Figure 4) is composed of the RED unit, two bottles containing the concentrate and dilute feed solutions forced to circulate within the stack by two peristaltic pumps (by MasterFlex Cole-Parmer[®]), two bottles in which the outlet solutions are collected and a tank containing the electrode-rinse solution recirculating in a closed-loop thanks to another peristaltic pump. This solution contains the redox couple hexacyanoferrate(III)/hexacyanoferrate(II) [Fe(CN)₆]⁴⁻/[Fe(CN)₆]³⁻ was employed in the experiments as it was judged as suitable for RED applications, thanks to its very high stability (in absence of light and oxygen) and very low toxicity [42].

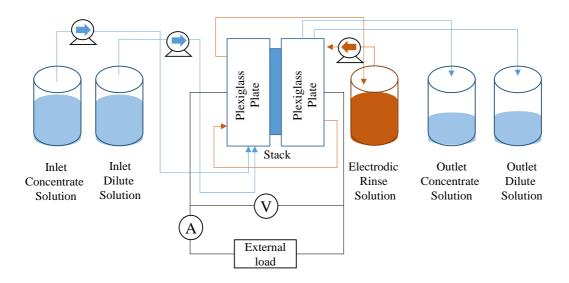


Figure 4. Scheme of the experimental apparatus employed for the experiments.

The electrodic rinse solution also contains 0.25 moles per liter of NaCl, as supporting electrolyte. The two ends of the stack are connected to a variable external load (by Sfernice[®]). The external circuit contains also an amperometer (by Fluke[®]) in series with the stack and a voltmeter (by Fluke[®]) in parallel, in order to read the current and the voltage, respectively, corresponding to the imposed external load.

The employed solutions and operating conditions investigated throughout the present work are shown in Table 2. Different values of C_{high} were tested because in a RED closed-loop arrangement, the regeneration unit thermal duty is expected to be lower, the lower C_{high} , possibly resulting into higher cycle efficiency.

	· · · · · · · · · · · · · · · · · · ·		=	
		v _{low} =v _{high} [cm/s]	C _{low} [mol/l]	C _{high} [mol/l]
	NaCl	0.5; 1; 2	0.05	0.5; 2; 5
Pure salts	NH ₄ Cl	0.5; 1; 2	0.05	0.5; 2; 5
	LiCl	0.5; 1; 2	0.05	0.5; 2; 5
Salt mixtures	NaCl-NH ₄ Cl	2	0.05	0.5; 2; 5
	NH ₄ Cl-LiCl	2	0.05	0.5; 2; 5
	NaCl-LiCl	2	0.05	0.5; 2; 5

Table 2. Summary of the experiments carried out in the present work

3.2. Methodology

Each experiment concerns the measurements of the voltage and of the current density across the stack as a function of the resistance of the external load (R_u). The trend of the voltage vs. the current is reported in Figure 5.

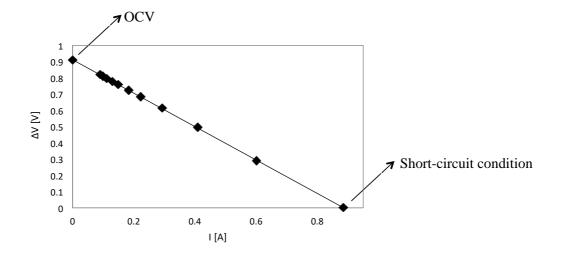


Figure 5. Trend of the stack voltage versus electric current for the case of NaCl-water solutions. Stack features and conditions: 5 cell pairs-stack, A= $0.1 \times 0.1 \text{m}^2$, C_{low} =0.05M, C_{high} =5M, v_{low} = v_{high} =2 cm/s, T= 25° C.

$$\Delta V = OCV - R_{stack}I \tag{3}$$

The slope of this trend gives the value of the stack resistance.

Once the values of current density and voltage are known, it is possible to calculate the corresponding values of Power Density P_D (equation 4):

$$P_D = R_u \cdot I^2 = \Delta V \cdot I = \Delta V \frac{OCV - \Delta V}{R_{stack}} = -\frac{\Delta V^2}{R_{stack}} + \frac{OCV \cdot \Delta V}{R_{stack}}$$
(4)

The maximum of P_D - ΔV trend corresponds to the condition in which the imposed R_u is equal to R_{stack} . This condition will be adopted in all the experiments carried out. Just as an example, in Figure 6 the P_D versus ΔV trend is reported for the case of NaClwater solutions: at a given solution velocity ($v_{low}=v_{high}=2$ cm/s) and dilute compartment concentration ($C_{low} = 0.05$ M), three different concentrations of the concentrate solutions were tested ($C_{high} = 0.5$ M, 2M, 5M). Clearly, in the investigated range of concentrations, the higher the salinity gradient available across the membranes, the higher the resulting P_D . The above described procedure was adopted for all the experiments summarized in Table 2. All experiments were carried out twice and very similar results were obtained thus guaranteeing a good reliability of the experimental procedure: in particular, discrepancies between variables measured in two runs of the same experiment were found always lower than 6%. These discrepancies are shown in the figures of Results and Discussion section in the form of error bars.

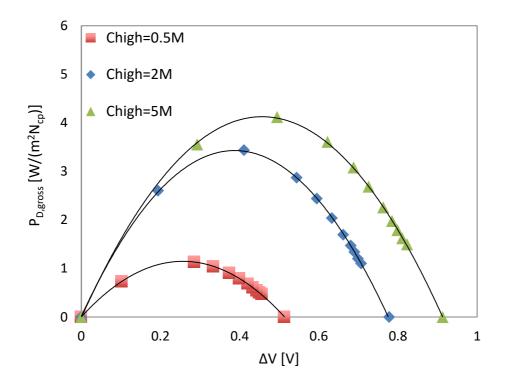


Figure 6. Experimental trends of Power density vs stack voltage for the case of NaClwater solutions. Stack features and conditions: 5 cell pairs-stack, A= $0.1 \times 0.1m^2$; C_{low}=0.05M; C_{high}=0.5M, 2M, 5M; v_{low}=v_{high}=2 cm/s, T= 25° C.

The Stack Resistance R_{stack} , which can be inferred from the $\Delta V vs I$ line, can be considered as the sum of five different resistances [43]:

$$R_{stack} = R_{blank} + N_{cell} \left(R_{low} + R_{high} + R_{AEM} + R_{CEM} \right)$$
(5)

where R_{blank} was assessed by employing a suitable stack containing only one cation exchange membrane and fed by the above mentioned electrodic rinse solution only. By imposing an increasing voltage and measuring the corresponding electric current as shown in Figure 7, R_{blank} can be assessed as the slope of the resulting linear trend and was found equal to 0.0327 Ω m².

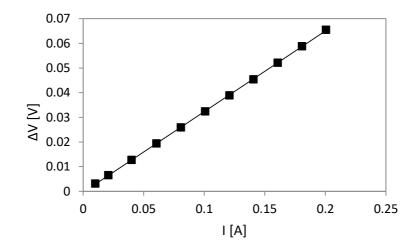


Figure 7. Imposed voltage vs. measured electric current for a stack composed of one CEM only and fed by the electrodic solution (containing the redox couple $[Fe(CN)_6]^{4-}$ / $[Fe(CN)_6]^{3-}$ at a concentration of 0.1M and NaCl as supporting electrolyte at a concentration of 0.25M), T=25°C, A=0.1×0.1m².

Once the value of R_{blank} is known, it is possible to correct the measured value of P_D as reported in equation 6, where $P_{D,corr}$ represents the power density obtainable for a large number of cell pairs (as in a full scale stack) where R_{blank} contribution is negligible and $R_u = R_{stack}$.

$$P_{D,corr} = \left(\frac{OCV}{2 R_{stack} - R_{blank}}\right)^2 \frac{R_{stack}}{N_{cell} A} \tag{6}$$

4. RESULTS AND DISCUSSION

4.1. Experiments with pure salts

The three salts selected in section 2.1 were tested in RED unit experiments according to the procedure described in section 3: as already shown in Figure 6, in these experiments C_{low} was kept constant while three different values of C_{high} were tested. Figure 8 shows, for each pure salt-water solution, the effect of solution velocity (set equal in all compartments) and Chigh on the main figures of a RED unit: OCV, Rstack and PD, corr. Independently of the pure salt taken into account, similar dependences of OCV, Rstack and $P_{D,corr}$ on solution velocity were found. In particular, OCV is always shown to increase with the velocity, while R_{stack} in most cases decreases as the velocity increases (Figure 8). These cooperative effects clearly results into a $P_{D,corr}$ increase with v. OCV increase with v is due to the lower solution residence time within the stack: the lower the residence time, the lower the concentration change along the channels, thus resulting into a driving force, which poorly reduces along the streamwise direction [20]. This phenomenon has an effect also on R_{stack} , and in particular on the overall resistance of the dilute channels R_{dil} which, at low C_{low} , is often the main contribution to R_{stack} . More precisely, solution velocity mainly affects both the ohmic and non-ohmic contributions to R_{low} [2,44]. The former is again related to the streamwise variation of the concentration along the compartment: practically, the lower v, the higher the streamwise concentration increase, which results in a lower mean- R_{low} . Conversely, the non-ohmic contribution is due to the cross-stream concentration change relevant to the boundary layer: clearly, the higher the flow rate within the channel, the higher the cross-stream velocity components, which can reduce the polarization effect [45]. The slightly decreasing R_{stack} vs v trend shown in Figure 8 suggests that the effect of v on the boundary layer is prominent with respect to that on the ohmic contribution, as expected on the basis of the low channel thickness investigated in the present work [46]. Clearly, as it can be seen in Figure 8, OCV, R_{stack} and $P_{D,corr}$ are approaching a plateau as v increases as expected: this occurs because at high v the mixing within the channel is highly enhanced, thereby resulting into really low concentration gradients throughout each channel. Based on these considerations a velocity of 2cm/s was adopted for all the other experiments.

Figure 8 shows also the effect of C_{high} on OCV, R_{stack} and $P_{D,corr}$. OCV is higher as C_{high} increases due to a higher driving force. Conversely, R_{stack} generally decreases as C_{high}

increases for NH₄Cl and LiCl, while a decreasing-increasing behaviour is observable for NaCl, as already found in other literature works [47,48]. Notably, although much less evident, the same behaviour was also observed for NH₄Cl at v=2cm/s. This decreasingincreasing trend can be explained by referring to R_{low} and R_{IEM} only, since R_{high} is negligible. R_{low} is known to decrease as C_{high} increases due to a larger amount of ions crossing the membranes. The membranes are in contact with solutions at different concentrations and their electrical resistance is determined by both the two solutions, although some studies demonstrated that the effect of the dilute solution is prominent [49,50]. The membrane resistance can be considered as the equivalent of two resistances in series: i.e. the one of the micro pores in which the solution flows and the other of the gel phase, which depends on the membrane swelling degree. The former is a decreasing function of the external solution concentration, while the latter increases at larger external solution concentration [47]. Summarizing, these competitive effects coupled with the concentration effect on R_{low} may or may not lead to a minimum in the R_{stack} - C_{high} trend, depending on which are the main contributions to R_{stack} .

The combination of the effects of C_{high} on OCV and R_{stack} leads to an increase of $P_{D,corr}$ as C_{high} is increased.

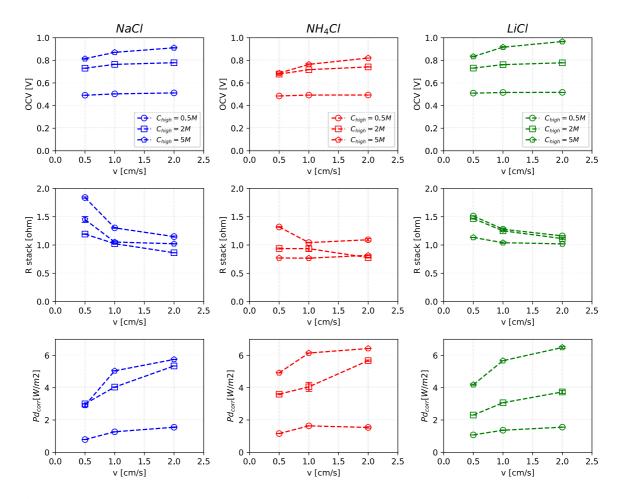


Figure 8. Experimental OCV, R_{stack} and $P_{D,corr}$ as functions of C_{high} and v. 5 cell pairs stack fed with solutions of NaCl (left column), NH4Cl (middle column) and LiCl (right column), A=0.1×0.1m²; C_{low}=0.05M; C_{high}=0.5M, 2M and 5M; v_{low}=v_{high}=0.5 cm/s, 1 cm/s and 2 cm/s; T=25°C.

Figure 9 shows *OCV*, R_{stack} and $P_{D,corr}$ values for the three salts at a given solution velocity (v = 2cm/s) for comparison purposes.

As regards the *OCV* values, it is possible to observe that the highest *OCV* was obtained for LiCl solutions especially at high C_{high} , followed by NaCl, while NH₄Cl exhibits the lowest values. This hierarchy is a direct consequence of the activity coefficients of these salts reported in the supporting information section (Figure 15), somehow confirming the outcomes of the Pitzer model for the pure salt-water solutions. However, it is worth noting that the difference between NaCl and LiCl is not as high as expected because of membrane permselectivity effects: LiCl exhibits a lower permselectivity, with respect to NaCl, as it is predictable from the comparison of the diffusion coefficients of the counter-ions (D _{Li+} < D_{Na+}) [51]. R_{stack} values reported in Figure 9 somehow confirms the hierarchy observable in the conductivity data reported in the supporting information section: being NH₄Cl-water solutions the most conductive, corresponding measured R_{stack} were the lowest at any C_{high} .

As it concerns $P_{D,corr}$, it is not possible to recognize a pure salt-water solution able to provide the highest $P_{D,corr}$ at any C_{high} . At C_{high} =0.5M and 5M the lower R_{stack} exhibited by NH₄Cl-water solutions and the higher *OCV* typical of LiCl ones somehow counterbalance each other, thus yielding similar $P_{D,corr}$ values. Conversely, the really higher R_{stack} value observable at C_{high} =2M for LiCl leads to the lowest $P_{D,corr}$.

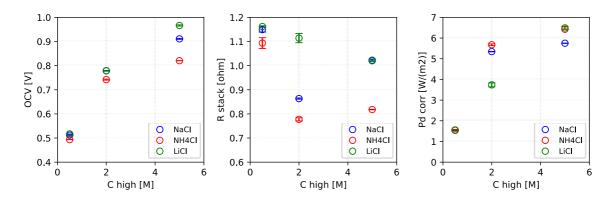


Figure 9. *OCV*, R_{stack} and $P_{D,corr}$ for the three different salts (NaCl, NH₄Cl or LiCl) at different C_{high}. 5 cell pairs stack; A=0.1×0.1m²; C_{low} =0.05M; C_{high} =0.5M, 2M and 5M; $v_{low}=v_{high}=2$ cm/s; T=25°C.

On overall, on the basis of the results collected here with Fujifilm IEMs (developed for NaCl), the use of NH₄Cl is suggested in the range of C_{high} investigated, while better performance in terms of power production are expected with the use of LiCl at larger C_{high} (i.e. $C_{high} > 6M$ not investigated in the present work).

4.2. Experiments with mixtures of salts

Water solutions prepared with the three salts mixture selected in section 2.2 were used as feed in the RED unit experiments described in the present section.

The mixture selection was performed assuming that the binary mixture-water solutions conductivity was intermediate between the two pure salt-water cases. This assumption was validated by the conductivity measurements reported in Figure 10. As it is shown in the figure, binary mixture-water solutions conductivity was always found about midway between the conductivities of the two pure salt-solutions.

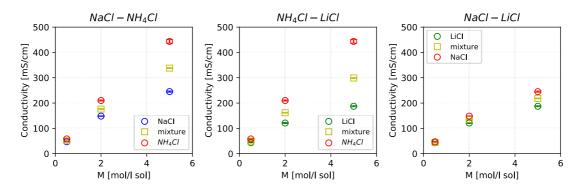


Figure 10. Experimental values of the conductivity obtained with the mixtures and with the corresponding pure salts at different concentrations (0.5M; 2M; 5M), temperature of 25°C.

All the experiments with salt mixtures (summarized in Table 2) reported in the following figures were carried out adopting the same procedure described in section 3.

In Figure 11 the *OCV* values obtained with the salt mixtures are compared with the corresponding ones relevant to the pure salts solutions.

The *OCV* values measured in the salt binary mixture-water solutions are always included between the *OCVs* of the two corresponding pure salt-water solutions. From a close inspection of the figure, it can be inferred that the mixture-*OCVs* are a bit closer to the lowest pure-*OCVs*. This experimental evidence somehow confirms the theoretical analysis outcomes, where a similar behaviour was observed both in the activity coefficient prediction and in the $\Delta \phi_{cell}$ values calculated (see Figure 3).

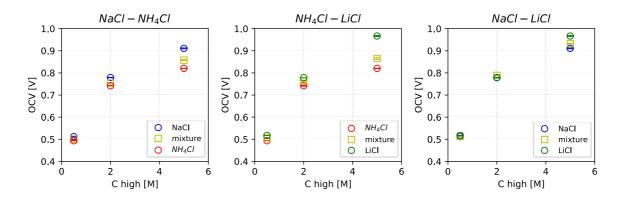


Figure 11. Comparison of the experimental values of *OCV* obtained with the mixtures and with the corresponding pure salts at different C_{high} . Stack composed of 5 cell pairs; A=0.1×0.1m²; C_{high} =0.5M, 2M, 5M; C_{low} =0.05M; v_{low} = v_{high} =2 cm/s; T= 25°C.

Results concerning the measurement of R_{stack} for the salt mixture-water solution are shown in Figure 12, where a comparison with R_{stack} values measured with the pure salt cases is also provided.

The three mixtures exhibit an analogous behaviour: quite surprisingly, when C_{high} is equal to 0.5M and 5M, the R_{stack} measured for the salt binary mixture is lower than both the two values measured for the pure salts. This finding probably derives from a complex interaction among ions, water and membrane fixed charges [47] and it is not easy to provide a robust explanation for this phenomenon only on the basis of the results collected here. In all the experiments carried out in the present work, the average R_{IEM} is always the most significant contribution to R_{stack} . In particular, the R_{stack} reduction encountered is allegedly due to a reduction of R_{CEM} that may result from an enhanced cation transport inside the pores. It is like that the transport of one cation type inside the pores was enhanced thanks to the presence of the other and vice-versa. Practically, the presence of a second cation modifies the above complex interaction: according to Geise et al. [52] the presence of cations with large binding affinity (as Na^+ and NH_4^+) may enhance the passage of other cations due to a fixed-charge concentration reduction and a consequent Donnan exclusion weakening. This also shows how much the membrane properties, and in particular the swelling degree and the concentration of fixed charges in the membrane, can affect the overall performances. In this regard, additional experiments with different membranes (e.g. membranes with a different ion exchange capacity) could add useful information to understand better the phenomenon. The above reduction of R_{stack} measured in the salt mixture with respect to the pure salt was not recognized at $C_{high} = 2M$. This different behaviour at 2M may be linked to the fact that at this concentration a minimum in R_{stack} - C_{high} trend was observed for the pure salt cases.

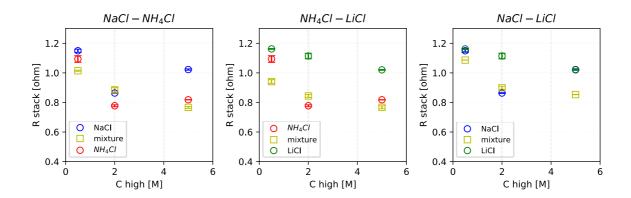


Figure 12. Comparison of the experimental values of R_{stack} obtained with the mixtures and with the corresponding pure salts at different C_{high} . Stack composed of 5 cell pairs; A=0.1×0.1m²; C_{high} =0.5M, 2M,5M; C_{low} =0.05M; v_{low} = v_{high} =2 cm/s; T= 25°C.

The above discussed surprising reduction of R_{stack} with the salt binary mixtures leads to a $P_{D,corr}$ being higher than both those relevant to the two pure salts at $C_{high} = 0.5$ and 5M as shown in Figure 13. Therefore, according to the findings reported in this figure, it is possible to increase the power produced by a RED unit operating under typical conditions (i.e. NaCl-water solutions, $C_{low} = 0.05$ M, $C_{high} = 0.5$ M (seawater) or 5M (brine), $v_{low} = v_{high} = 2$ cm/s) just by adding an equivalent molar quantity of another salt as LiCl or NH₄Cl. Clearly, this makes sense only in the case of applications where the RED unit is employed in a closed-loop, as it occurs in the REDHE in which an *ad hoc* feed solution can be employed and then regenerated in the separation stage.

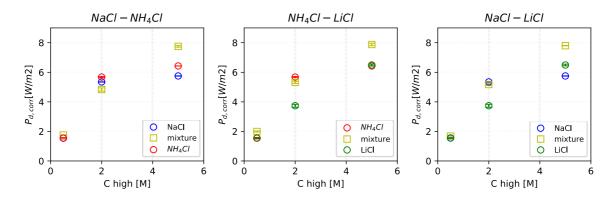


Figure 13. Comparison of the experimental values of $P_{D,corr}$ obtained with the mixtures and with the corresponding pure salts at different C_{high} . Stack composed of 5 cell pairs; A=0.1×0.1m²; C_{high} =0.5M, 2M, 5M; C_{low} =0.05M; v_{low} = v_{high} =2 cm/s; T= 25°C.

In order to have a more quantitative estimate of the figures variation, the values of R_{stack} and $P_{D,corr}$ collected for the mixtures were compared with the average values between the ones collected for the corresponding pure salts. Remarkably, R_{stack} shows a decrease by around 10% in almost all cases and the maximum decrease is found at the highest C_{high} , being around 17% for all the three mixtures. As a consequence, $P_{D,corr}$ reaches the highest percentage increase in correspondence to the same C_{high} . Concluding, for the three investigated mixtures, the produced $P_{D,corr}$, in the case of a stack fed by a mixture with C_{high} equal to 5 M and C_{low} equal to 0.05 M, increases by around 30% with respect to the $P_{D,corr}$ given by the average value between the ones producible by the single salts.

Finally, in Figure 14 the measured values of OCV, R_{stack} and $P_{D,corr}$ for the three binary mixtures are reported for comparison purposes.

As it concerns the *OCV*, the NaCl-LiCl mixture provides the highest values, as expected since the activity coefficients of the two pure salts in water are much higher than the NH₄Cl ones. On the other hand, the NaCl-LiCl mixture yields the largest R_{stack} as it does not contain the NH₄Cl salt, which exhibits the highest conductivity in water. These opposite properties provided by the binary salt mixtures investigated lead to a $P_{D,corr}$ similar for the three cases independently of C_{high} , although the NH₄Cl-LiCl mixture appears as the most promising.

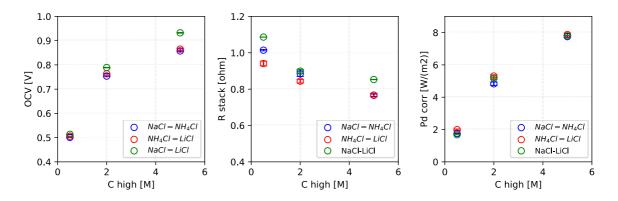


Figure 14. Comparison of the values of *OCV* (left graph), R_{stack} (middle graph) and $P_{D,corr}$ (right graph) for the mixtures NaCl-NH₄Cl, NaCl-LiCl and NH₄Cl-LiCl (stack composed of 5 cell pairs; C_{high} =0.5M, 2M, 5M; C_{low} =0.05M; v_{high} = v_{low} =2cm/s; T=25°C; A=0.1×0.1m²).

CONCLUSIONS

In the present work the behaviour of non-conventional aqueous solutions of pure uniunivalent salts and salt equimolar binary mixtures in a Reverse Electrodialysis Unit was investigated via experiments. The idea was that of enhancing the power produced by a RED unit to be employed within a closed-loop arrangement to convert low-grade heat into electricity (Reverse Electrodialysis Heat Engine).

A preliminary analysis based on (i) activity coefficients, (ii) conductivity and (iii) solubility was performed in order to select the most suitable pure salt-water solutions for power production enhancement. This analysis resulted in the choice of LiCl, NH₄Cl and NaCl: LiCl was chosen for its really high activity coefficients and solubility, NH₄Cl for its high conductivity in water, while NaCl was used as reference salt. A preliminary

analysis was carried out also for the choice of the salt binary mixtures by taking into account the same properties analysed for the pure salt cases. In particular, the multicomponent Pitzer model was used for assessing the salt activity coefficients in the mixture and the multicomponent Nernst equation was suitably modified for dealing with the salt binary mixtures to be investigated. On the basis of the results collected and also for comparison purposes with the pure salt cases, mixtures composed of the above three salts (i.e. NaCl-LiCl, NH4Cl-LiCl, NH4Cl-NaCl) were identified as the most interesting. As regards the pure salt-water solutions, results collected in a lab-scale RED stack equipped with Fujifilm[®] IEMs (developed for NaCl) do not show a solution providing the highest corrected power density ($P_{D,corr}$) at any operating condition. However, the use of NH4Cl is suggested in the range of C_{high} investigated, while better performance in terms of power production are expected with the use of LiCl for larger C_{high} .

Concerning the salt mixture experiments, the *OCV* values measured were always found included between the *OCVs* of the two corresponding pure salt solutions. Conversely, quite surprisingly, when C_{high} is equal to 0.5M and 5M, the R_{stack} measured for the salt binary mixtures was found lower than both the two values measured for the pure salts, thus resulting into a $P_{D,corr}$ being higher than both those relevant to the two pure salts.

This experimental evidence suggests that it could be possible to increase the power produced by a RED unit operating under typical conditions (as those investigated in the present work) and fed with NaCl-water solutions just by adding an equivalent molar quantity of another salt as LiCl or NH₄Cl.

Comparing the salt mixtures results collected, similar $P_{D,corr}$ were obtained for the three cases independently of C_{high} , although the NH₄Cl-LiCl mixture appears as the most promising.

On overall, the present work shows for the first time that RED stack performance in terms of power production can be enhanced by employing aqueous solutions of different salts. However, there is still large room for further investigations in order to understand better the complex interaction mechanism between ions, membrane fixed charges and water. This would allow guiding the choice of the salt combination features, in terms of salt type and quantity, to be used in a RED unit in order to maximize the electric power produced. Furthermore, the membrane properties can be tuned in order to optimize the membranes for salts different from NaCl and salt mixtures, as it is evident how dramatically the stack performances are affected by the diffusion coefficients of the ions

through the membranes and the ion-fixed group interactions. Moreover, given the final aim to convert waste heat into power in a Reverse Electrodialysis Heat Engine, tests will also be needed to evaluate the performance of the regeneration unit fed by these salt mixture-water solutions.

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NOMENCLATURE					
membrane area [m ²]					
A _{ϕ} , α , b Pitzer model constant [(kg/mol) ^{1/2}]					
$A_{\Lambda}, B_{\Lambda}, C_{\Lambda}$ coefficients of Jones and Dole's equation					
C solution molarity [mol/l]					
m solution molality [mol/kg]					
I ionic strength [mol/kg]					
Z modified ionic strength [mol/kg]					
f_{γ} coefficient of Pitzer's model [-]					
B_{γ} , C_{γ} coefficients of Pitzer's model for pure salt-water solutions					
B _{MX} , B' _{MX} , C _{MX} coefficients of Pitzer's model for binary mixture-water solutions					
ΔV stack voltage [V]					
stack current [A]					
number of cell pairs [-]					
Power Density $[W/(m^2N)]$					
P _{D,corr} Corrected Power Density [W/(m ² N)]					

- R universal gas constant (8.314 J/(mol K))
- Rblank blank resistance $[\Omega]$

$R_{BL} \\$	electrical resistance of the boundary layer $[\Omega]$
R _{IEM}	electrical resistance of ionic exchange membrane $[\Omega]$
Rstack	stack electrical resistance $[\Omega]$
R_u	electrical resistance of the external load $[\Omega]$
r	Jone and Dole's viscosity coefficient [(l/mol) ^{0.5}]
S	Jone and Dole's viscosity coefficient [l/mol]
Т	temperature [°C]
v	fluid velocity [cm/s]
z_M, z_X	cation and anion charge [-]

Greek letters

α_p permselectivity [-]

- η solution viscosity [Pa s]
- γ_{MX} salt activity coefficient [-]

 $\beta^{\square\square}, \beta^{\square\square}, \phi_{cc'}, \phi_{\square}$ Pitzer model second order interaction parameters

 ψ_{Mca}, ψ_{Xca} Pitzer model third order interaction parameters

 $\Delta \Phi_{cell}$ cell potential difference [V]

 v_M , v_X cation and anion stoichiometric coefficients [-]

 Λ_0 salt equivalent conductivity at infinite dilution [mS/(cm mol)]

 Λ salt equivalent conductivity [mS/(cm mol)]

Subscripts

- HIGH concentrate compartment
- LOW dilute compartment
- *c*, *c*' generic cation index
- *a*, *a*' generic anion index
- cell cell pair

Acronyms

- AEM anion exchange membrane
- CEM cation exchange membrane
- IEM ion exchange membrane
- OCV Open Circuit Voltage

- PRO pressure retarded osmosis
- RED reverse electrodialysis
- SGP salinity gradient power

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SUPPLEMENTARY INFORMATION

a) Activity coefficients of pure salts in water solutions

The activity coefficients of the pure salts in water solutions are evaluated through the Pitzer model for pure salts, reported in equations (1-4):

$$f_{\gamma} = -A_{\phi} \left[\frac{\sqrt{m_{MX}}}{1 + b \sqrt{m_{MX}}} + \frac{2}{b} \ln(1 + b \sqrt{m_{MX}}) \right]$$
(1)

$$B_{\gamma} = 2 \beta^{(0)} + 2 \beta^{(1)} \frac{\left(1 - \left(1 + \alpha \sqrt{m_{MX}} - \alpha^2 \frac{m_{MX}}{2}\right) \exp(-\alpha \sqrt{m_{MX}})\right)}{\alpha^2 m_{MX}}$$
(2)

$$C^{\gamma} = \frac{3}{2} C^{\phi} \tag{3}$$

$$\gamma_{MX} = \gamma_{M^+} = \gamma_{X^-} = \exp(f_{\gamma} + m_{salt} B_{\gamma} + m_{salt}^2 C^{\gamma})$$
(4)

where:

 A_{ϕ} , α and *b* are Pitzer's model parameters (values reported in Appendix A only for the salts finally selected);

 $\beta^{(0)}$, $\beta^{(1)}$ and C^{ϕ} are parameters specific for each salt (values reported in Appendix A only for the salts finally selected);

 m_{MX} is solution molality;

 γ_{cat} and γ_{an} are ions activity coefficients.

The chart below reports the trends of the activity coefficients for the salts listed in Table 1.

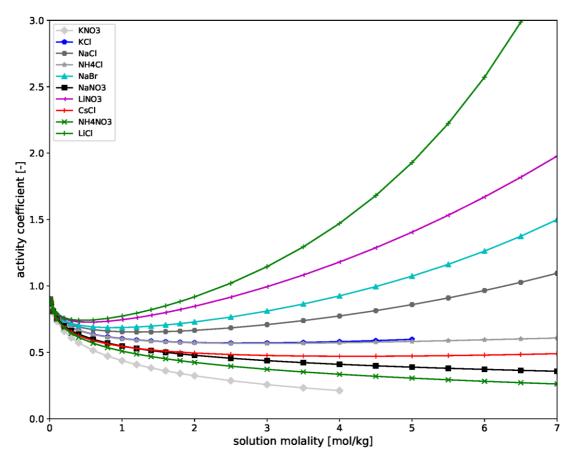


Figure 15. Activity coefficients vs. solution molality for the investigated salts

b) Cell potential difference with pure salts-water solutions

The cell potential difference is evaluated through the Nernst equation:

$$\Delta\phi_{cell} = \frac{RT}{F} ln\left(\frac{a_c^{high} a_a^{high}}{a_c^{low} a_a^{low}}\right) = \frac{2RT}{F} ln\left(\frac{a_{salt}^{high}}{a_{salt}^{low}}\right)$$
(5)

Some theoretical cell potential difference data relevant to the pure salt-water solutions investigated (see Table 1) are reported in Figure 16 as examples: these were calculated at 25°C, at given concentrations in the dilute and concentrate compartment (i.e. $C_{low} = 0.05$ M and $C_{high} = 5$ M, respectively) and for ideal membranes (i.e. permselectivity $\alpha_p = 1$). Among the investigated salts, LiCl is shown to provide the highest cell potential difference.

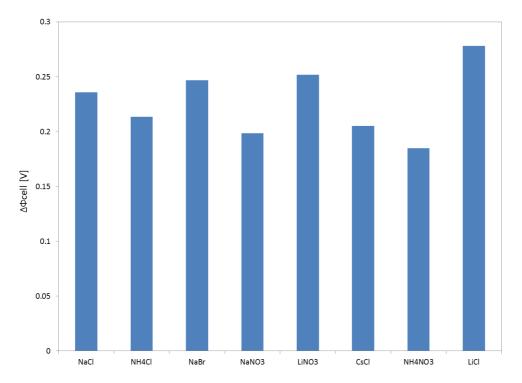


Figure 16. Theoretical cell potential difference with different salts. Calculation conditions: 1 cell pair, C_{high} = 5M, C_{low} =0.05M, T=25°C, α_p =1.

c) Conductivity of pure salts-water solutions

The conductivity of the water-pure salts solutions is evaluated through the Jone and Dole's equation:

$$\Lambda = \Lambda_0 - \frac{A_\Lambda \sqrt{C_{MX}}}{1 + B_\Lambda \sqrt{C_{MX}}} - C_\Lambda C_{MX}$$
(6)

where

 Λ_0 is the equivalent conductivity of the salt at infinite dilution (values reported in Appendix 1 for the selected salts only);

 A_{Λ} , B_{Λ} and C_{Λ} are parameters specific for each salt (values reported in Appendix 1 for the selected salts only);

 C_{MX} is the molarity of the salt.

Figure 17 reports the conductivity values estimated via equation 6 for the salts of Table 1. As it can be seen, NH₄Cl and KCl show the highest conductivity, although the latter has a limited range of solubility (see also next paragraph).

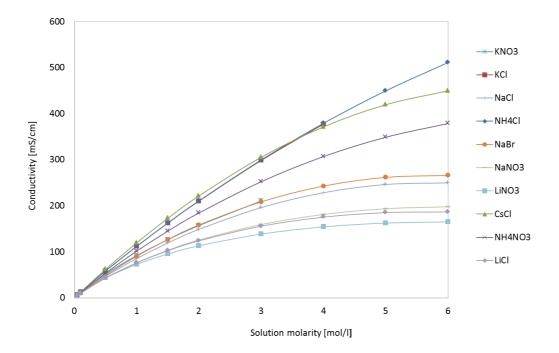


Figure 17. Conductivity vs. solution molarity for the investigated salts with a zoom in the range of concentrations between 0 and 0.5M.

d) Solubility of salts in water

The solubility values of the salts listed in Table 1 have been found in literature.

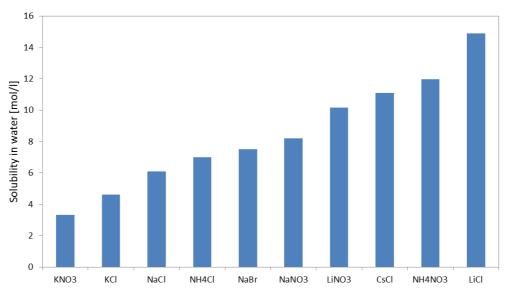


Figure 18. Solubility in water for the investigated salts (T=25°C)

e) Pitzer's Model for the activity coefficients of salts in binary mixtures

Considering a mixture containing a certain number of ions *i* with a molality equal to m_i and an ionic charge z_i , it is possible to calculate the ionic strength and the modified ionic strength:

$$I = \frac{1}{2} \sum_{i} m_i z_i^2 \tag{7}$$

$$Z = \sum_{i} m_i |z_i| \tag{8}$$

Once the ionic strength is known, the interaction parameter f^{γ} can be assessed as follows:

$$f^{\gamma} = -A_{\phi} \left[\frac{I^{1/2}}{1+b I^{1/2}} + \frac{2}{b} \ln(1+b I^{1/2}) \right]$$
(9)

Then, the interaction parameters B_{MX} , B'_{MX} and C_{MX} specific for each salt present in the system can be calculated according to equations (10-12):

$$B_{MX} = \beta_{MX}^{0} + \left(\frac{\beta_{MX}^{1}}{\alpha^{2}I}\right) \left[1 - \left(1 + \alpha\sqrt{I}\right)\exp\left(-\alpha\sqrt{I}\right)\right]$$
(10)

$$B'_{MX} = \frac{2 \beta_{MX}^{1}}{\alpha^{2} I^{2}} \left[-1 + \left(1 + \alpha \sqrt{I} + \frac{1}{2} \alpha^{2} I \right) \exp(-\alpha \sqrt{I}) \right]$$
(11)

$$C_{MX} = \frac{C^{\phi}}{2 |z_M z_X|^{1/2}} \tag{12}$$

where:

 β_{MX}^0 , β_{MX}^1 are the "observable parameters" typical of each salt (values reported in Appendix 1 for the selected salts only);

 α is a constant (value reported in Appendix 1 for the selected salts only);

 C^{ϕ} is a parameter specific for each salt (value reported in Appendix 1 for the selected salts only).

A combination of these parameters provides the values of the activity coefficients for each salt present in the solution according to equation 13. In particular, for the generic salt *MX*, the activity coefficient is defined as follows.

$$\ln \gamma_{MX} = |z_{M} z_{X}| f^{\gamma} + + \left(2\frac{\nu_{M}}{\nu}\right) \sum_{a} m_{a} \left(B_{Ma} + Z C_{Ma} + \frac{\nu_{X}}{\nu_{M}} \phi_{Xa}\right) + + \left(2\frac{\nu_{X}}{\nu}\right) \sum_{c} m_{c} \left(B_{cX} + Z C_{cX} + \frac{\nu_{M}}{\nu_{X}} \phi_{Mc}\right) + + \sum_{c} \sum_{a} m_{c} m_{a} \{|z_{M} z_{x}| B'_{ca} + \nu^{-1} [2 \nu_{M} z_{M} C_{ca} + \nu_{M} \psi_{Mca} + \nu_{X} \psi_{cXa}]\} + + \frac{1}{2} \sum_{c} \sum_{c'} m_{c} m_{c'} \left[\frac{\nu_{X}}{\nu} \psi_{cc'X} + |z_{M} z_{x}| \phi'_{cc'}\right] + + \frac{1}{2} \sum_{a} \sum_{a'} m_{a} m_{a'} \left[\frac{\nu_{M}}{\nu} \psi_{Maa'} + |z_{M} z_{x}| \phi'_{aa'}\right]$$
(13)

where

c is the index used for the cations present in the solution;

a is the index used for the anions present in the solution;

 v_M and v_X are the cation and anion stoichiometric coefficients respectively, both equal to 1 for uni-univalent salt;

 z_M and z_X are the cation and anion charge respectively;

 B_{Ma} and C_{Ma} are the second order interaction parameters relevant to the salt composed of the the cation M⁺ and a generic anion *a*;

 B_{cX} and C_{cX} are the second order interaction parameters relevant to the salt composed of the the anion X⁻ and a generic cation *c*;

 B'_{ca} is the interaction parameter between the generic anion and cation;

 ϕ_{Mc} is the second order interaction coefficients between the cation M⁺ and the other generic cation *c*;

 ϕ_{Xa} is the second order interaction coefficients between the anion X⁻ and the other generic anion *a*;

 $\phi_{cc'}$ is an interaction parameter between two different cations, usually set equal to zero;

 $\phi_{aa'}$ is an interaction parameter between two different anions, usually set equal to zero;

 ψ_{Mca} is the third order interaction parameter among the cation M⁺, a generic cation *c* and a generic anion *a*;

 ψ_{Xac} is the third order interaction parameter among the anion X⁻, a generic cation *c* and a generic anion *a*.

APPENDIX A

Pure salt solution parameters					
		NaCl	NH ₄ Cl	LiCl	
Activity coefficient parameters	$\beta^{(0)}$	0.0765	0.0522	0.1494	
	$\beta^{(1)}$	0.2664	0.1918	0.3074	
	C^{Φ}	0.00127	-0.00301	0.00359	
Equivalent conductivity parameters	λ_0	126.5	149.6	114.97	
	A_{Λ}	91.0239	149.6	42.975	
	${ m B}_{\Lambda}$	1.6591	3.4498	0.1045	
	C_{Λ}	6.8041	4.3620	0.00735	

Table A1: Parameters relevant to the calculation of the activity coefficient and the equivalent conductivity of pure salt-water solutions.

Table A2: Parameters relevant to the calculation of the activity coefficients of salts in salt binary mixture-water solutions.

Salt mixture parameters for activity coefficient calculation							
Common parameters		Specific mixture parameters					
$\frac{A_{\Phi}}{[(kg/mol)^{1/2}]}$	0.3915		NaCl-	NH4Cl-LiCl	LiCl-NaCl		
$[(kg/mol)^{1/2}]$			NH4Cl				
b [(kg/mol) ^{1/2}]	1.2	$\Phi_{\text{cat-cat}}$	0.0044	-0.0563	0.012		
α [(kg/mol) ^{1/2}]	2	$\Psi_{ ext{cat-cat-an}}$	-0.0031	0.0089	-0.003		