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6 **Integration of ion-exchange and crystallisation processes to recover**
7 **boric acid and magnesium hydroxide from saltworks bitterns**

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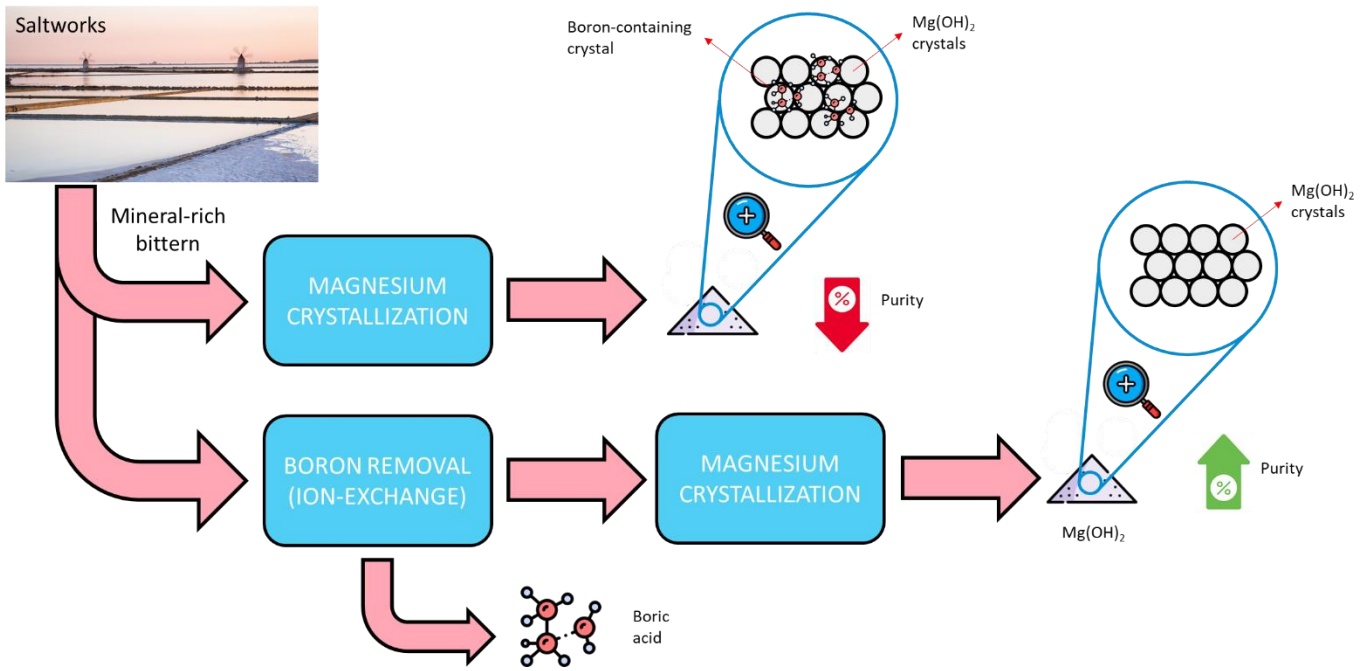
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GRAPHICAL ABSTRACT



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25

LIST OF ABBREVIATIONS

BE	Backscattered Electrons
CRMs	Critical Raw Materials
CF	Concentration factor
EU	European Union
FESEM-EDS	Field Emission Scanning Electron Microscopy Energy Dispersive X-ray Spectroscopy
ICP-MS	Inductively Coupled Plasma Mass Spectrometry
ICP-OES	Inductively Coupled Plasma Optical Emission Spectroscopy
PV	Pore volume
PVC	Polyvinyl chloride
<i>q</i>	Resin capacity
RP	Recovery percentage
SEI	Secondary Electron Imaging
TEs	Trace Elements
TG	Thermogravimetric analysis
XRD	X-ray diffraction

ABSTRACT

The lack of primary sources of the so-called Critical Raw Materials within the European Union is directing research towards alternative mining to extract them. Among the different potential alternative sources, the brines generated in traditional saltworks (denominated *bitterns*) can be a very promising option. In fact, several elements can be up to 50 times more concentrated in *bitterns* than in seawater. Magnesium, for example, can present concentrations above 50 g/L, and its recovery can be pursued as hydroxide by using crystallization processes. However, the presence of boron even at relatively low concentrations (100 mg/L – 150 mg/L) can contaminate the final magnesium hydroxide, thus making it not suitable for certain applications, such as the refractory industry (target $< \sim 0.11$ mg B/g of magnesium hydroxide). Because of boron speciation (as boric acid), only chelating ion-exchange resins based on N-methylglucamine functional groups can selectively remove boron from aqueous solutions. In this work, the integration of ion-exchange and crystallization processes is carried out to produce pure magnesium hydroxide from real *bitterns* collected in Trapani (Sicily). Two different *bitterns* were treated with two commercial B-selective chelating ion-exchange resins (S108 and CRB05), and the boron-free *bittern* was later used for $\text{Mg}(\text{OH})_2(\text{s})$ crystallization. The effect of pH on $\text{Mg}(\text{OH})_2(\text{s})$ crystallization was studied and data was compared (in terms of purity) in the cases with or without B-removal pre-treatment. Moreover, once the resin was saturated, elution with HCl allowed to recover H_3BO_3 via evaporative crystallization. Results showed the possibility of recovering pure $\text{Mg}(\text{OH})_2(\text{s})$ (>98%) with low B-content (<0.10 mg B/g), matching the specifications for refractory industry, and H_3BO_3 with 95% purity.

KEYWORDS: Brine valorisation; Minerals recovery; magnesium hydroxide; chelating resins; N-methylglucamine; precipitation.

54 **1. Introduction**

55 The first list of Critical Raw Materials (CRMs), including 14 elements and minerals, was presented
56 by the European Union (EU) in 2011. These materials have attracted a growing concern due to their
57 supply risk and economic importance. The list of CRMs has been reviewed several times, and in its
58 last version, released in 2023, it includes up to 34 CRMs [1]. Boron (B) and Magnesium (Mg) have
59 been included among the CRMs since the first list [2].

60 Seawater has emerged as a promising alternative source for recovering critical elements through sea
61 mining, as its composition covers nearly every element in the periodic table [3,4]. However, most of
62 these elements exist in seawater at concentrations of a few mg/L, or even below, being in fact called
63 Trace Elements (TEs) [5]. It has been demonstrated that only the most concentrated components in
64 seawater (i.e. Na, K, Mg, Cl) can be extracted through economically viable approaches [6–8].
65 Conversely, the feasibility of recovering TEs from seawater is compromised by the energy-intensive
66 extraction processes involved [9,10].

67 In this context, concentrated brines are promising alternatives to explore. EU is investing, through
68 sea mining, towards the extraction of various raw materials, critical or not, from concentrated brines
69 from either (i) desalination plants or (ii) seawater solar saltworks, as in the case of the EU-funded
70 project SEArcularMINE [11]. In the latter scenario, brine is originated in *saltworks*, which are
71 extensive areas where seawater fills shallow ponds. Here, solar and wind action cause seawater to
72 evaporate and concentrate, leading to the crystallization of calcium compounds, first, and sea salt
73 (NaCl) eventually [12,13]. The mother liquor remaining after salt crystallisation, known as *bittern*,
74 becomes significantly concentrated (20 to 50 times more than seawater for some elements) and devoid
75 of Ca. For instance, in Trapani (Italy), Vicari et al. [14] performed the characterization of bittern in
76 saltworks ponds. The authors evaluated the composition along the ponds and reported that Mg and B
77 concentrations increased from 1480 mg/L and 4.5 mg/L (in seawater) to 22000 mg/L and 79 mg/L (in
78 bittern), respectively. Randazzo et al. [15] provided a more extensive characterization of different
79 *bitterns* along the Mediterranean basins from different sources, showing that final composition
80 depends on the collecting period and production process. Authors reported concentrations up to 75
81 g/L Mg and 400 mg/L B. The high B and Mg concentrations in bitterns could offer a viable alternative
82 route for these element-based compounds production, especially considering that 98% of Europe's
83 demand for B in the form of borates is currently provided by Turkey, whereas 97% of the European
84 demand for Mg is provided by China [16].

85 Different methods are reported in the literature for recovering B from aqueous saline solutions [17–
86 19], including evaporation-crystallisation, precipitation-coagulation, ion exchange or membrane
87 technologies, such as reverse osmosis or electrodialysis. However, B separation is challenging with
88 the latter option as, in aqueous solution, B can be found as boric acid or borate ion, depending on the
89 solution pH ($pK_a(25^\circ\text{C}) = 8.76$) [18].

90 N-methylglucamine resins have been widely studied for B removal and/or recovery from aqueous
91 streams [20–23], including brines [24–26], as they have higher selectivity towards B than other ion
92 exchange resins and they can be regenerated with strong acids as sulphuric and hydrochloric [27].
93 The Diaion CRB03 and CRB05 (Mitsubishi Chemical Corporation), S108 (Purolite) or Amberlite
94 IRA743 (Dupont) are commercially available examples of macroporous styrene-divinyl benzene
95 resins containing N-methylglucamine functional groups. Excluding the latter one, Figueira et al. [26]
96 applied these resins for recovering B from seawater RO brines at pH 5.9, reporting that Langmuir
97 maximum adsorption capacities were 10.9, 12.9 and 16.6 mg_B/g for S108, CRB05 and CRB03,
98 respectively. However, the use of N-methylglucamine resins for the specific treatment of solar
99 saltworks bitterns has not been extensively studied yet. Up to 30 sorbents, including different
100 functional groups, were evaluated in batch mode by Vallès et al. [28] concluding that, apart from B,
101 N-methylglucamine resins presented also high affinity for Ga, Ge and Co. Recently, the same authors
102 have evaluated three B-selective resins (Purolite S108, Diaion CRB03 and Diaion CRB05) in column
103 mode aiming to recover B, Co, Ga and Ge from synthetic bitterns mimicking different real scenarios
104 [29]. In that study, an adsorption capacity of 8.3 mg_B/g for S108 and 11 mg_B/g for both CRB03 and
105 CRB05 was reported, being normally able to recover >90% of the B retained by the resins.

106 After B extraction by the chelating resins, it can be recovered in an elution step with HCl solutions.
107 In these streams, B concentration can increase up to 15 times more than in the treated bittern [26,29].
108 Consequently, a precipitation stage could be applied in order to recover B as a solid. B could be
109 precipitated as borate or boric acid, or by coagulation using AlCl_3 or FeCl_3 [30], typically with low B
110 concentrations (e.g. 120 mg/L). However, a large quantity of chemicals is required and a huge amount
111 of sludge is generated [31]. When treating solutions with higher B contents (e.g. 4.1 g/L), precipitation
112 in the form of $\text{Ca}_2\text{B}_2\text{O}_5 \cdot \text{H}_2\text{O}$ (parasibirskite) using $\text{Ca}(\text{OH})_2$ is preferred [32]. Alternatively, H_3BO_3
113 could be crystallised by evaporation [33,34]. This procedure was successfully applied to a multi-
114 component solution containing 1.8 g_B/L , in which 76% of B was recovered after evaporating 90% of
115 the water at 70 °C [35].

116 Boron extraction from saline solutions is desirable also if high-purity Mg is going to be recovered
117 from the same stream. Mg has been successfully recovered from bittern in the form of magnesium
118 hydroxide, $\text{Mg}(\text{OH})_2(\text{s})$, by the addition of alkaline reactants [36]. $\text{Mg}(\text{OH})_2(\text{s})$ is a white odourless
119 compound, extensively employed in numerous industrial fields, e.g. as neutralising and antibacterial
120 agent in wastewater treatment, primary raw material for the refractory industry, nontoxic flame
121 retardant filler in polymeric materials [37]. The impact of boron content in $\text{Mg}(\text{OH})_2$ powders has
122 been widely discussed in the scientific and patent literature. For example, it has been reported that,
123 the maximum equivalent boron oxide, B_2O_3 , content must be lower than 1 mg $\text{B}_2\text{O}_3/\text{g-MgO}$ on the
124 ignited basis, i.e. namely referred to the magnesium oxide (MgO) compound, thus being ~ 0.11 mg
125 B/g- $\text{Mg}(\text{OH})_2(\text{s})$, for solids applicability in the refractory sector [38]. In 1985, Spoons et al. [39]
126 presented a treatment process scheme for seawater brines or aqueous Mg-containing solutions based
127 on the use of adsorptive magnesium hydroxide to remove boron species and increase $\text{Mg}(\text{OH})_2(\text{s})$
128 purity. The brine was mixed with adsorptive magnesium hydroxide solids in a series of counter-
129 current stages. Some years later, Wilkomirsky et al. [40] proposed the addition of hydrochloric acid
130 to the saline solutions to precipitate boron as boric acid. Li et al., [41] investigated the possible use
131 of chelating resins (e.g. Purolite S108) for the adsorption of boron from the residual brines of Chinese
132 salt lakes with the aim to prepare boron-free magnesia compounds. Recently, Bonin et al. [42] treated
133 lithium-rich brines through Amberlite IRA743 resins. The pre-treatment successfully reduced the
134 boron content in the brine leading to (i) a decrease of the brine loss caused by mother liquor intake in
135 $\text{Mg}(\text{OH})_2$ solids and (ii) an increase of the purity of synthesized $\text{Mg}(\text{OH})_2(\text{s})$ products.

136 In the present work, the proposed process aims to integrate B-selective chelating resins and
137 crystallization processes to demonstrate the technical feasibility of recovering high purity products
138 from *bitterns*. Several operation conditions were explored, aiming at improving the purity of the
139 $\text{Mg}(\text{OH})_2(\text{s})$ recovered with the objective to make it suitable for the refractory industry ($< \sim 0.11$ mg
140 B/g- $\text{Mg}(\text{OH})_2(\text{s})$). In the experimental campaign, different resins were evaluated for boron and
141 germanium, whereas for $\text{Mg}(\text{OH})_2(\text{s})$ crystallization, the effect of final pH was studied. The results
142 achieved showed that by integrating these two technologies it was possible to recover highly pure
143 boric acid and magnesium hydroxide, the latter one characterized by a low boron concentration.

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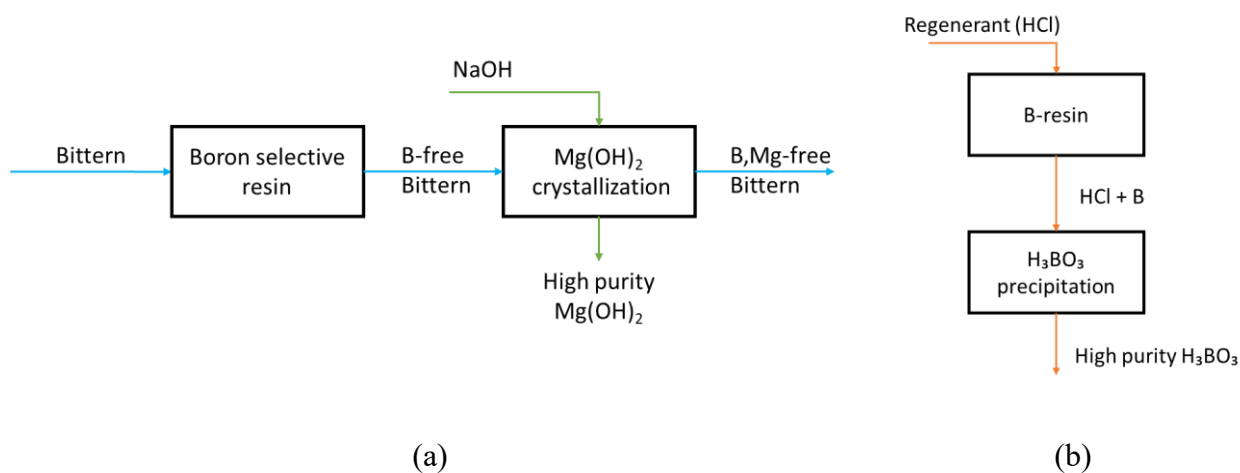
2. Material and Methods

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Figure 1 shows a block flow diagram of the investigated bittern treatment chain for the simultaneous recovery of boron (as boric acid) and magnesium (as magnesium hydroxide) from real saltworks bitterns.



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Figure 1 Bittern treatment steps for the production of high purity (a) $Mg(OH)_2(s)$ and (b) $H_3BO_3(s)$ from the eluate.

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In order to recover pure $Mg(OH)_2(s)$, ion exchange resins are first adopted to extract boron directly from the bittern generated at the solar saltworks (see Figure 1.a). B-selective chelating resins were employed to capture and concentrate B from bitterns in a sorption-desorption cycle. Specifically, the performances of two commercial resins (e.g. S108 and CRB05), were investigated by treating two real bitterns collected from Margi and Galia saltworks, both located in the district of Trapani, Italy. The boron-free bittern is further treated with sodium hydroxide (NaOH) solutions to precipitate Mg ions in the form of $Mg(OH)_2(s)$. The solids were precipitated from treated and untreated bitterns at two final pH values of 10.8 (stoichiometric conditions) and 12 (alkaline excess) with NaOH solutions. Following boron breakthrough (see Figure 1.b), a regenerant aqueous HCl solution is employed to extract the boron from the resins before using an evaporation-crystallisation method to recover boric acid ($H_3BO_3(s)$).

163 **2.1. Solutions and Chemicals**

164 Two real bitterns, collected from Margi and Galia saltworks (Trapani, Italy), were employed in the
 165 experimental campaign. Table 1 presents their composition in terms of major and minor elements.

166

167 **Table 1** Margi and Galia bitterns composition assessed via Ion Chromatography (IC), Inductively
 168 Coupled Plasma Optical Emission Spectrometry (ICP-OES) and Inductively Coupled Plasma Mass
 169 Spectrometry (ICP-MS) techniques.

Analytical		Margi	Galia
Technique			
IC (mg/L)	Na ⁺	54190	67638
	K ⁺	12749	10532
	Cl ⁻	185405	180149
	Br ⁻	2084	1573
	*SO ₄ ²⁻	60799	45663
ICP-OES (mg/L)	B	161.2	133.3
	Ca	142.9	157.7
	Mg	49551	37499
	**S	24131	18516
	K	-	-
ICP-MS (µg/L)	Li	7519	5801
	Co	< 10	< 10
	Ga	< 25	< 25
	Ge	< 10	< 10
	Rb	4083	3283
	Sr	12004	25611
	Cs	4.78	2.59

170 * SO₄²⁻ refers to sulphate ions measured by IC

171 ** S refers to total elemental sulphur measured by ICP-OES

172

173 NaOH solutions were prepared by dissolving pellets of analytical grade (Honeywell|Fluka™, with a
 174 purity of >98 %) in deionized water. NaOH solution concentrations were checked via titration by

175 adopting a standard HCl solution. 1 M HCl solutions were obtained from 37 % wt HCl solution
176 (Honeywell) diluted in deionized water.

177 2.2. Experimental set-up and procedure

178 2.2.1. Boron adsorption and resin regeneration

179 Two different resins were employed to recover boron: Purolite® S108 and Mitsubishi DIAION
180 CRB05. Both resins present the same chemistry, based on N-methylglucamine functional groups, but
181 differing in particle size, density and capacity (see Table 2).

182

183 **Table 2** Main properties of the N-methylglucamine sorbents used in this study.

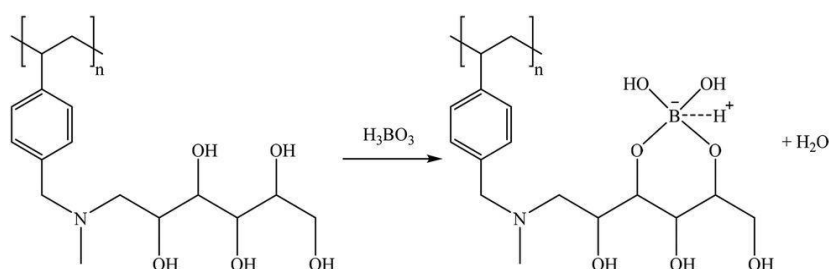
Sorbent (abbreviation)	Supplier	Ionic form	Capacity (eq/L)	Humidity content (%)	Particle size (mm)	Density (g/L)	Ref.
Purolite S108 (S108)	Purolite	F.B.	0.60	61-67	0.43-0.63	670-730	[43]
Diaion CRB05 (CRB05)	Mitsubishi Chemical	F.B.	0.95	45-53	0.55	750	[44]

184 F.B.: free base

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186 Based on the resin functional groups, the complexation mechanism between of boron follows the
187 reaction shown in Figure 2 [28]

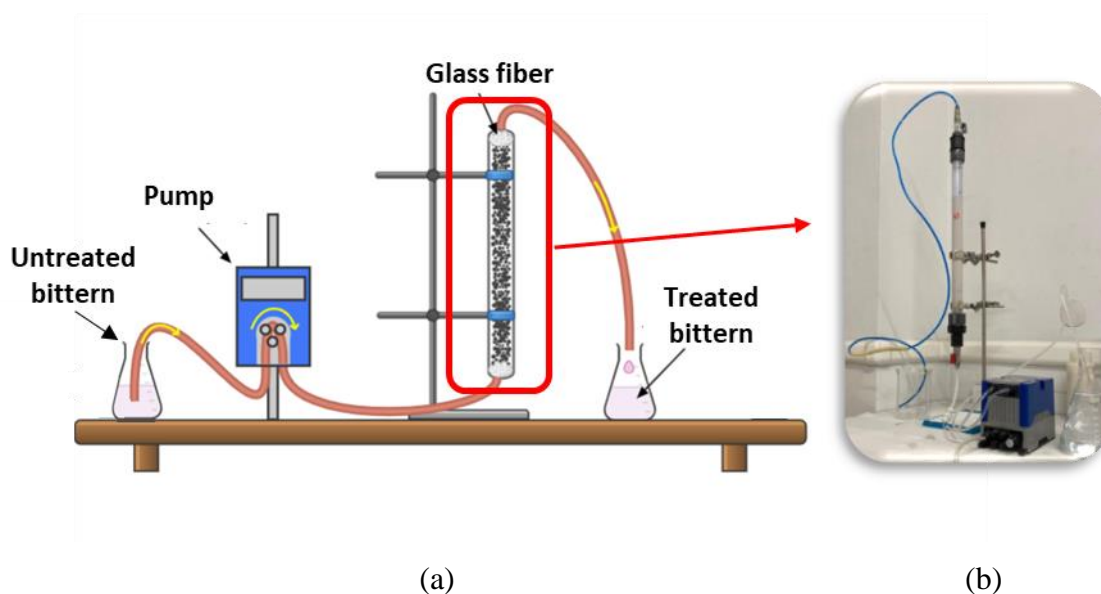
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189

190 **Figure 2** Complexation mechanism leading the formation of monoborate complex in the adopted
191 functionalized resins [28]

192 Resins were packed in a polyvinyl chloride (PVC) column of 49.7 cm length, with an inner diameter
193 of 2.7 cm. 75% of the column volume was occupied with the resin (c.a. 128 g of resin), leaving the
194 rest un-occupied to account for resin expansion during acid regeneration. At the top and bottom of
195 the column glass fiber was allocated. Figure 3 shows a picture and a schematic representation of the
196 experimental set-up. The brine was fed from the feed tank to the bottom of the column by using a
197 KRONOS 50 peristaltic pump, which was manually adjusted to the desired flow-rate. At the outlet of
198 the column, another tank was placed to collect the treated bittern for carrying out $Mg(OH)_2(s)$
199 crystallization tests. Samples were periodically collected at the outlet of the column to be analyzed.
200



206 **Figure 3** (a) Schematic representation of the experimental set-up employed for the boron removal
207 step from real saltworks bittern. (b) A picture of the experimental set-up.

208 Before starting the experimental campaign, and once the resin was packed, the pore volume of the
209 column was measured. To do that, 0.05 M NaCl was circulated across the experimental set-up at 10
210 mL/min and the conductivity of the outlet solution was measured to determine the residence time and,
211 therefore, the pore volume.

212 Each experimental test consisted of: (i) bittern feeding the column and relevant saturation in boron
213 (ii) displacement of the bittern inside the column with distilled water, (iii) boron elution from the
214 resin using 1 M HCl, and (iv) displacement of HCl with water before starting another cycle. It must
be highlighted that resin operation was carried out using the H^+ form, rather than in the Na^+ form to
avoid $NaCl(s)$ precipitation inside the column.

215 Analyzing the B-content in the outlet samples, breakthrough curves were obtained and plotted,
 216 whereas during regeneration, the elution profiles were determined. The data collected was used to
 217 calculate the resin capacity (q , mg/g resin), the concentration factor (CF, dimensionless) and the
 218 recovery percentage (RP, %). The resin capacity (Eq. 1) accounts for the amount of boron that was
 219 sorbed per gram of resin, while the CF (Eq. 2) is used to express how much boron was concentrated
 220 in the eluate with respect to the feed:

$$q = C_0 \frac{\int_0^V \left(1 - \frac{C}{C_0}\right) dV}{m_{resin}} \quad (1)$$

$$CF = \frac{\frac{1}{V_{el}} \int_0^{V_{el}} C dV}{C_0} \quad (2)$$

221 Where C_0 is the initial concentration of the species in the brine (mg/L), V is the volume of brine that
 222 circulated through the column (L), m_{resin} is the mass of resin (g), C is the concentration of the species
 223 at the exit of the column (mg/L), and V_{el} is the volume of solution used during the elution (L).

224 Finally, the RP, used to assess if the resin was completely regenerated, is calculated according to Eq.
 225 3:

$$RP = \frac{\int_0^{V_{el}} C dV}{q \cdot m_{resin}} \cdot 100 \quad (3)$$

226 Four different tests were performed for the boron removal step, varying type of bittern, adopted resin
 227 and flow rate, as illustrated in Table 3. Initially, the Margi bittern was tested with the two resins with
 228 the objective to evaluate resins performance toward boron and possible other element extraction
 229 (namely tests MP1 and MD1). During these tests, the brine was fed at a flow rate of 2 PV/h (11.4
 230 mL/min for the Purolite S108 and 10.7 mL/min for Diaion CRB05). Following saturation, desorption
 231 was carried out at 0.5 PV/h (2.85 mL/min for the Purolite S108 and 2.67 mL/min for Diaion CRB05).
 232 Considering that Purolite S108 was the only one able to extract both B and Ge, it was later used to
 233 treat the Galia bittern. In this case, the influence of solution flow rate was also investigated.
 234 Specifically, a series of tests (GP1) were carried out keeping the same operating conditions as those
 235 employed for Margi cases, while another set of tests was performed at higher flow rate (GP2) for both
 236 saturation (2.5 PV/h) and elution (0.8 PV/h).

237 **Table 3** Boron removal tests from real bitterns for two different brines (Margi(M) and Galia (G))
 238 using two different chelating resins (Purolite S108(P) and Diaion CRB05(D))

	MP1	MD1	GP1	GP2
Resin type	Purolite S108	Diaion CRB05	Purolite S108	Purolite S108
Bittern	Margi	Margi	Galia	Galia
Saturation flow rate	2 PV/h - 11.42 mL/min	2 PV/h - 10.7 mL/min	2 PV/h - 11.42 mL/min	2.5 PV/h - 14.66 mL/min
Regeneration flow rate	0.5 PV/h - 2.85 mL/min	0.5 PV/h - 2.67 mL/min	0.5 PV/h - 2.85 mL/min	0.8 PV/h - 4.89 mL/min

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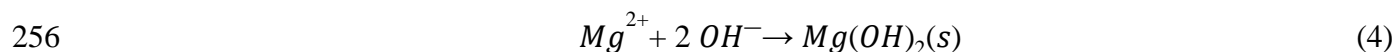
240 In each test, 1L of treated bittern was collected at the first PV, which was further used for Mg(OH)₂(s)
 241 synthesis. Other bittern samples were collected during GP2 within the first 6 PV to further investigate
 242 the influence of boron extraction on Mg(OH)₂(s) powder purity.

243 During the elution, the eluate was collected in a separate beaker from 1 PV to 1.5 PV (given that the
 244 B peak was centered at 1.5 PV) to assess boric acid recovery. However, due to the low volume
 245 collected (c.a. 150 mL), the evaporative route for boric acid crystallization was carried out with a
 246 synthetic solution mimicking the eluate composition from the MP1 and MD1. Then, an initial volume
 247 (1000 mL) was placed on a hot plate magnetic stirrer (C-MAG HS 7, IKA) to keep the solution
 248 continuously stirred at 70 °C. A sample was taken every 100 mL of evaporated water to monitor the
 249 composition change during the experiment. The test was stopped after 900 mL were evaporated, and
 250 the solution was cooled down to room temperature to promote the precipitation of salts. Then, the
 251 suspension was filtered using a 0.22 µm pore size filter and the solids collected were dried at 100°C
 252 for 24h before analysis. The clarified was then analysed to determine the recovery of the boric acid.

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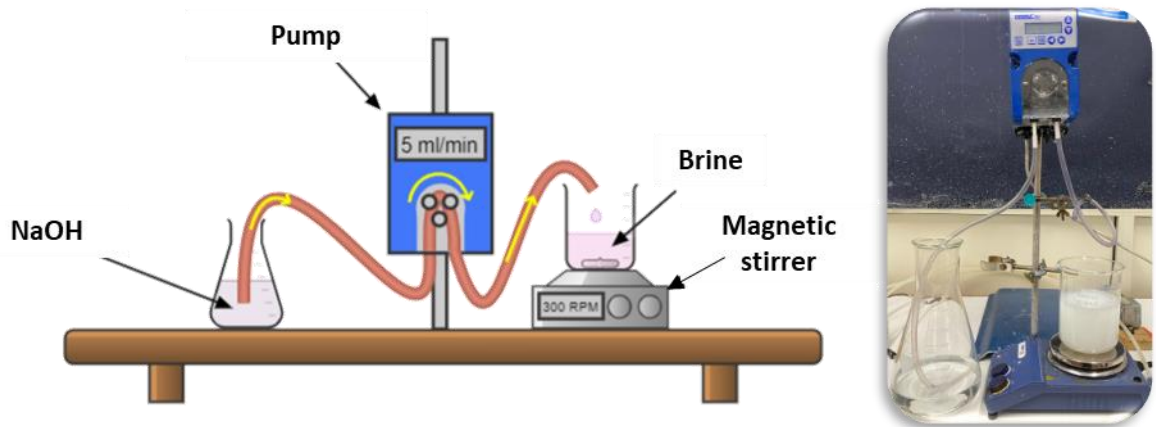
254 **2.2.2. Magnesium hydroxide precipitation**

255 Mg(OH)₂(s) precipitation occurs through the reaction of magnesium and hydroxide ions:



257 A schematic representation of the Mg(OH)₂(s) experimental set-up is shown in Figure 4. The bittern
 258 was placed into a 1L beaker and NaOH solution was fed at a flow rate of 5 mL/min through a
 259 peristaltic pump (KRONOS 50). Bittern and, then, Mg(OH)₂(s) suspension were stirred at 300 rpm

260 by magnetic stirrer (ARGO LAB M2-A). Precipitation tests were carried out by adopting (i) a
261 stoichiometric ratio between Mg^{2+} and OH^- amount, targeting a final suspension pH of ~ 10.8 , and (ii)
262 a 20 % OH^- excess. In the latter case, the final suspension pH ranged between 12 and 13. In all tests,
263 0.5 M NaOH solutions were employed as alkaline reactant. A final suspension volume of 800 mL was
264 always targeted, and initial bittern and NaOH volumes were calculated consequently, taking into
265 account also Mg^{2+} and OH^- content in the feed solutions.
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267
268 **Figure 4** Schematics of the experimental set-up for $Mg(OH)_2(s)$ precipitation tests.

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270 Tests were carried out using pristine bittern and the treated one, after boron removal, collected at
271 different times (pore volumes passed in the column) during the sorption tests. All tests were
272 performed at a room temperature. Table 4 reports the details of the $Mg(OH)_2(s)$ precipitation tests.

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280 **Table 4** $Mg(OH)_2(s)$ precipitation tests. Tests were performed at a room temperature, using a 0.5 M
 281 NaOH solutions and by stirring bitterns and $Mg(OH)_2(s)$ suspensions at 300 rpm. Numbers from 0 to
 282 3 refer to the PV value at which the bittern was collected (0 is the untreated bittern). The last letters
 283 S and E indicate OH/ Mg^{2+} stoichiometric and excess amounts.

Cases	Bittern	Bittern volume [mL]	NaOH volume [mL]	Pore Volume fraction
M_0S	Margi (Mg^{2+} 2.04 M)	87.4	712.6	-
MP1_1S	Margi (Mg^{2+} 2.04 M)	87.4	712.6	1-3
MD1_1S	Margi (Mg^{2+} 2.04 M)	87.4	712.6	1-3
M_0E	Margi (Mg^{2+} 2.04 M)	69.9	730.1	-
MP1_1E	Margi (Mg^{2+} 2.04 M)	69.9	730.1	1-3
MD1_1E	Margi (Mg^{2+} 2.04 M)	69.9	730.1	1-3
G_0S	Galia (Mg^{2+} 1.54 M)	111.5	688.5	-
GP1_1S	Galia (Mg^{2+} 1.54 M)	111.5	688.5	1-3
GP2_1S	Galia (Mg^{2+} 1.54 M)	111.5	688.5	1-2
GP2_2S	Galia (Mg^{2+} 1.54 M)	111.5	688.5	3-4
GP2_3S	Galia (Mg^{2+} 1.54 M)	111.5	688.5	4-6
G_0E	Galia (Mg^{2+} 1.54 M)	89.2	710.8	-
GP1_1E	Galia (Mg^{2+} 1.54 M)	89.2	710.8	1-3
GP2_1E	Galia (Mg^{2+} 1.54 M)	89.2	710.8	1-2
GP2_2E	Galia (Mg^{2+} 1.54 M)	89.2	710.8	3-4
GP2_3E	Galia (Mg^{2+} 1.54 M)	89.2	710.8	5-6

284

285 2.3. Analytical techniques

286 2.3.1. Analysis of liquid samples

287 The aqueous samples (bittern, eluate and clarified solution) were analyzed via Inductively Coupled
 288 Plasma Mass Spectrometry (ICP-MS, 7800 ICP-MS from Agilent Technologies) and Inductively
 289 Coupled Plasma Optical Emission spectroscopy (ICP-OES, Optima 2100 DV PerkinElmer
 290 spectrometer and 5100 ICP-OES from Agilent Technologies) techniques, for which samples were

291 previously filtered and diluted in 2% HNO₃. Samples were also analyzed using ion chromatography
292 (IC) using, for cations, a Dionex ICS-1000 equipped with a CS16 column using 30 mM
293 methanesulphonic acid, whereas for anions, a Dionex Aquion equipped with an IonPac™ AS11-HC
294 column and 25 mM KOH.

296 **2.3.2. Analysis of solid samples: Mg(OH)₂(s) and H₃BO₃(s)**

297 The Mg(OH)₂ powder purity was assessed through three different analytical techniques: (i) X-ray
298 diffraction, XRD; (ii) boron concentration assessment; (iii) thermogravimetric analysis, TG. X-ray
299 analyses were conducted in the 2θ range of 10–70° (CuKα radiation 1.54 Å, 40 kV, 40 mA) at a step
300 size of 1°/min using the RIGAKU model D.MAX 2500 HK. Boron concentration in solid samples
301 was assessed through ICP-MS, after Mg(OH)₂ powder acid digestion. For such purpose, 100 mg of
302 Mg(OH)₂ powder were dissolved in 50 ml of 2 wt% HNO₃. TG analyses were carried out at a heating
303 rate of 10 °C/min from 30 °C to 1000 °C, under a constant nitrogen flow of 20 mL/min using the STA
304 449 F1 Jupiter analyzer, NETZSCH. From TG data, the mass purity was calculated as the ratio
305 between the mass loss recorded in the temperature range between 320 °C and 800 °C ($\Delta m_{320-800^\circ\text{C}}$)
306 and the theoretical one ($\Delta m_{theoretical}$, 30.87 %wt, [45]) according to eq.(5):

$$307 \quad \text{Mass Purity} = \frac{\Delta m_{320-800^\circ\text{C}}}{\Delta m_{theoretical}} \quad (5)$$

308 In the temperature range between 320 °C and 480 °C, Mg(OH)₂(s) decomposes into MgO(s) [45].
309 However, a continuous mass loss was observed between 480 °C and 800°C. Many authors have
310 investigated this continuous loss, which has been related to the slow OH⁻ groups release from the
311 MgO lattice [46–48]. Therefore, if no other impurities are identified in DTG curves (e.g. due to
312 carbonate decomposition), namely the derivate curves of the TG ones with respect to temperature,
313 the mass loss between 320 °C and 800 °C can be considered for Mg(OH)₂(s) mass purity estimation.

314 Boric acid samples were analysed by Field Emission Scanning Electron Microscopy Energy
315 Dispersive X-ray Spectroscopy (FESEM-EDS) (JEOL JSM-7001F) at an acceleration voltage of
316 20.0 keV using Secondary Electron Imaging (SEI) or Backscattered Electrons (BE) to obtain their
317 morphology. Apart from that, the mineral phases presented in the solid were identified with XRD,
318 after grinding the sample into powder. A D8 Advance diffractometer (Bruker) was used with a Bragg-
319 Brentano configuration θ-2θ and a vertical goniometer. The equipment has a Cu X-ray tube, which
320 allows to work up to 40 kV and 40 mA. The spectrum was recorded from 15° to 60° with steps of

321 0.020°. The identification of mineral phases was performed with EVA software (Bruker). Finally,
322 samples were digested in 2% HNO₃ and then analysed by ICP to assess the solid purity.

323

324

3. Results and discussion

325

3.1. Performance of the ion-exchange resins for boron removal

326

3.1.1. Comparison of Purolite S108 and Diaion CRB05 for treating the Margi bittern

327

Boron, lithium, cobalt, gallium, germanium, rubidium, strontium and cesium breakthrough (C/C_0)

328

and elution (using 1 M HCl) curves as a function of the volume treated by the column for the Margi

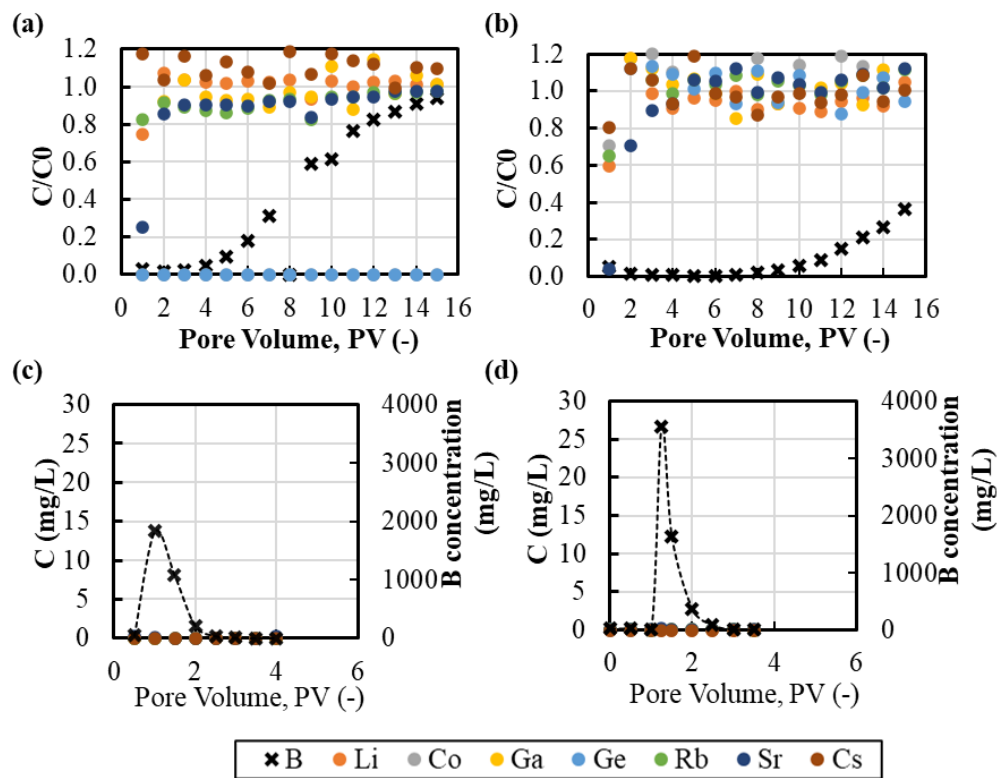
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bittern, expressed as PVs, are reported in Figure 5 for tests MP1 and MD1. Data for major ions is not

330

shown, as they were not retained by the resin ($C/C_0=1$).

331



332

Figure 5 (a,b) Breakthrough and (c,d) Elution curves for the trace elements (B, Li, Co, Ga, Ge, Rb,

333

Sr and Cs) as function of pore volume for: (a,c) MP1 and (b,d) MD1

334

Figure 5.a shows the performance of the Purolite S108 when treating the Margi bittern at 2 PV/h. In

335

this case, the breakthrough of boron started around 5 PV ($C/C_0 = 0.1$), being the resin completely

336

saturated on it at 16 PV. Moreover, the resin was able to extract completely the germanium in solution

337

along the whole test. The Diaion CRB05 showed significant different performance, see Figure 5.b.

338

As matter of fact, it can be noticed the higher capacity of the CRB05 resin, as the breakthrough for

339 boron started at 11 PV ($C/C_0=0.1$), versus the 5 PV of the S108. Moreover, in this case, germanium
340 was not retained.

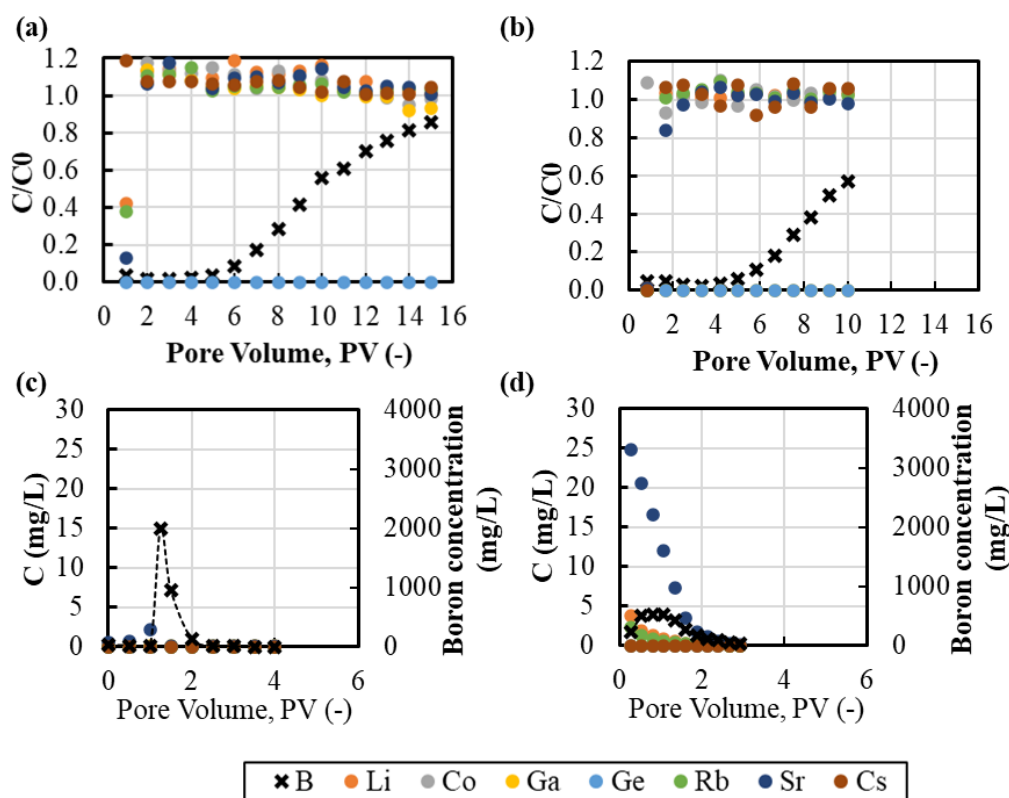
341 From a generic perspective, it can be observed that the two resins presented a similar behavior,
342 confirming the high selectivity of the N-methylglucamine resins towards boron (see Figure 5.a and
343 5.b). It must be noted that germanium was also co-extracted by the Purolite resin, thanks to the similar
344 chemistry of Ge and B in aqueous solutions, both forming an uncharged species (i.e. $H_4GeO_4(aq)$ and
345 $H_4BO_4(aq)$). The Ge speciation explains why it was also extracted by the N-methylglucamine
346 functional groups, as reported by Vallès et al. [28] with an extraction mechanism similar as that
347 described in Figure 2 for $H_3BO_3(aq)$. This behavior for the CRB05, not reported in batch experiments
348 with both resins and similar brines [28], was actually reported for column experiments later on [29].
349 The main reason may be associated to the structure changes recently introduced in the CRB05 resin,
350 also selective for B extraction, aiming to improve the B extraction and re-extraction performance.
351 The modification of the nature of the N-methylglucamine functional groups and the different size of
352 the $Ge(OH)_4(aq)$ molecules compared to the $B(OH)_3(aq)$ molecules could therefore explain the
353 different extraction efficiency in column mode with respect to batch mode. Apart from that, it should
354 be highlighted the large equilibrium times used by Vallès et al. [28] during the batch experiments
355 (24h), which are higher than the ones used under column mode in the present work (30 min).

356 Following elution, in the test MS1 (see Figure 5.c), the boron concentration slowly increased reaching
357 the maximum value of 1831 mg/L at 1 PV, eventually decreasing to 0 mg/L at 3 PV, due to the
358 continuous replacement of boron ions by H^+ . In the case of other elements, their concentration
359 remained below 0.05 mg/L. Similarly, due to the higher capacity of the CRB05, it was possible to
360 reach a higher peak of boron during elution, being 3557 mg/L (see Figure 5.d).

361

362 **3.1.2. Performance of Purolite S108 when treating the Galia bittern**

363 Considering that Purolite S108 allows to target both boron and germanium, apart from its lower cost
364 (half of the price in comparison to Diaion CRB05), its performance was studied with also the Galia
365 bittern. In this case, the effect of flow rate was investigated, working at 2 PV/h and 2.5 PV/h during
366 saturation. Boron, lithium, cobalt, gallium, germanium, rubidium, strontium and cesium breakthrough
367 (C/C_0) and elution (using 1 M HCl) curves as a function of the volume treated by the column for the
368 Margi bittern, expressed as PVs, are reported in Figure 6 for tests GP1 and GP2. Data for major ions
369 is not shown, as they were not retained by the resin ($C/C_0=1$).



370 **Figure 6** (a,b) Breakthrough and (c,d) Elution curves for the trace elements (B, Li, Co, Ga, Ge, Rb,
 371 Sr and Cs) as function of pore volume for: (a,c) GP1 and (b,d) GP2.

372

373 In the first test (Purolite S108 treating Galia bittern, with inlet flow-rate of 2 PV/h, Figure 6.a), the
 374 breakthrough for boron started at around 6 PV ($C/C_0=0.1$), while Ge was completely extracted
 375 ($C/C_0=0$) during the whole test (10 PV). In comparison to the previous test (MP1), the breakthrough
 376 started later, likely due to a slightly lower boron concentration (133 mg/L vs 161 mg/L). Ge sorption
 377 was quantitative as in the other test with Purolite resin. When the flow rate was increased to 2.5 PV/h,
 378 during the resin saturation, already in the initial phase of the test, boron was not completely removed,
 379 as the C/C_0 was around 0.05, likely due to the high velocity inside the column.

380 Following saturation of the resin, elution was carried out using 1 M HCl and the concentration profiles
 381 plotted in Figure 6 were found, as a function of the volume of HCl used (converted to PVs). In the
 382 test GP1, where elution was performed at 0.5 PV/h, the resin presented a similar trend as the MP1
 383 test, reaching a boron peak of 2000 mg/L at 1.25 PV. However, during the elution at 0.8 PV/h, the
 384 boron concentration slowly increased reaching the maximum value of 500 mg/L at 1 PV, eventually
 385 decreasing to 0 mg/L at 3 PV. It should be noted that a wide peak was obtained rather than a clearly
 386 defined peak due to the higher velocity of HCl inside the column. In the case of other elements, the

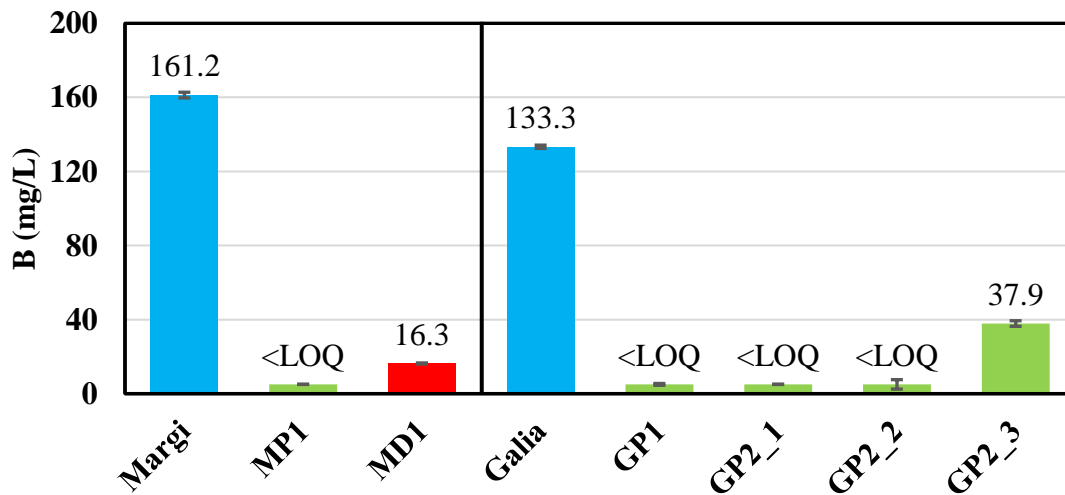
387 strontium concentration decreased from 25 mg/L to 0 in the first 2PV. Traces of gallium, lithium and
 388 rubidium were observed in the first 2 PV (from ~4 mg/L to <0.1 mg/L). The presence of these
 389 elements in the eluate, that were not extracted by the resin, were likely related to an un-efficient
 390 bittern washing-out step between saturation and elution.

391

392 3.1.3. Comparison among scenarios: boron removal, resins capacity, concentration 393 factor and recovery percentage

394 As mentioned previously, the solution after being treated by the resin was collected to be later used
 395 for Mg(OH)₂(s) crystallization. Figure 7 shows the boron concentrations in the initial bitterns and in
 396 the samples collected for both Galia (Figure 7.a) and Margi (Figure 7.b) bittern. The boron content
 397 was considerably reduced in samples collected at the first 3 PV regardless the treated bittern (Margi
 398 or Galia) or the adopted flow rate (GP1 and GP2 cases). With the samples collected from 1 to 3 PV,
 399 it was possible to reduce boron concentration to values lower than 17 mg/L (MD1) or below the
 400 quantification limits of ICP, namely 7.2 and 26.78 mg/L for Margi and Galia bitterns analyses.
 401 However, in the test GP2, the boron concentration increased to a value of 37.9 mg/L (GP2_3) at the
 402 sample collected from 4 to 6 PV, indicating the start of the breakthrough curve.

403

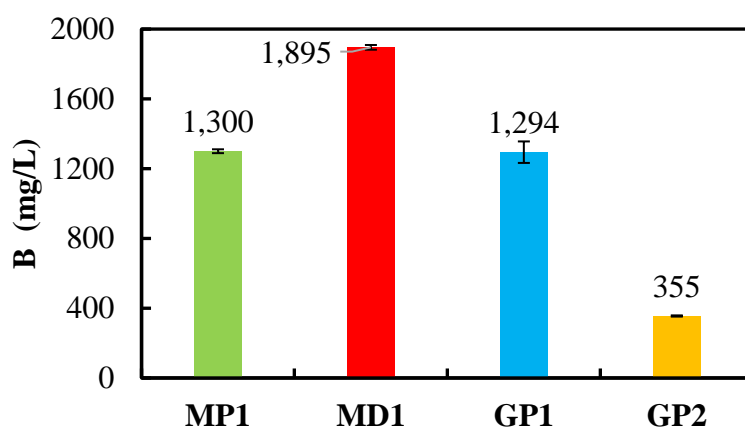


404

405 **Figure 7** Boron concentration in Margi and Galia Margi bitterns with and without the treatment
 406 using ion-exchange resins. GP1_1, 2, 3 PV refer to samples withdrawn within 0-2, 2-4 and 4-6 PV
 407 treated in the resin, while all the other samples were collected within 1 and 3 PV.

408

409 Figure 8 shows the final boron concentration in the collected eluate. In this case, in order to maximize
 410 boron concentration, the eluate was collected from 1 to 1.5 PV, which is the region where the peak
 411 was centered. As expected, the lowest concentration was in the GP2 due to the higher flow rate during
 412 elution, while decreasing elution flow-rate to 0.5 PV/h, higher concentration values were obtained
 413 ranging from 1.3 g/L for the S108 resin up to 1.9 g/L for the CRB05. The higher concentration factors
 414 achieved in test MD1 reflects the improvements done in CRB05 to optimize its extraction-re-
 415 extraction systems.



416

417 **Figure 8** Boron concentration in the eluate solutions collected from 1 to 1.5 PV for the four B
 418 recovery/removal tests performed.

419 From the analysis of results presented, the main process performance indicators were calculated,
 420 namely resin capacity, B concentration factor and B-recovery, and are reported in Table 5 for all tests.

421

422 **Table 5** Resin capacity, B concentration factor and B-recovery

	Resin capacity (mg/g)	Concentration factor (CF)	% B recovery
MD1	1.6	11.8	>99.9
MP1		8.1	>99.9
GP1	1.2±0.1	9.7	96.8
GP2		2.7	97.6

423

424 The Purolite S108 resin exhibited a capacity of ~1.2 (±0.1) mg B/g, which was consistent along the
 425 different tests performed (tests MP1, GP1 and GP2). The Diaion CRB05 exhibited the highest resin

426 capacity, with a value of 1.6 mg/g (MD1). In terms of concentration factor, it was also observed the
427 effect of decreasing the flow-rate during elution, as it was possible to increase it from 2.7 to 9.7 (test
428 GP2 to test GP1). By comparing the performance of the two resins, it was also noticed that the CRB05
429 allowed to achieve higher CF values (11.8) in front of S108 (8.1) under the same operating conditions.
430 With regard to the efficacy of the regeneration process, more than 97% of the boron extracted was
431 later recovered in the elution for all tests.

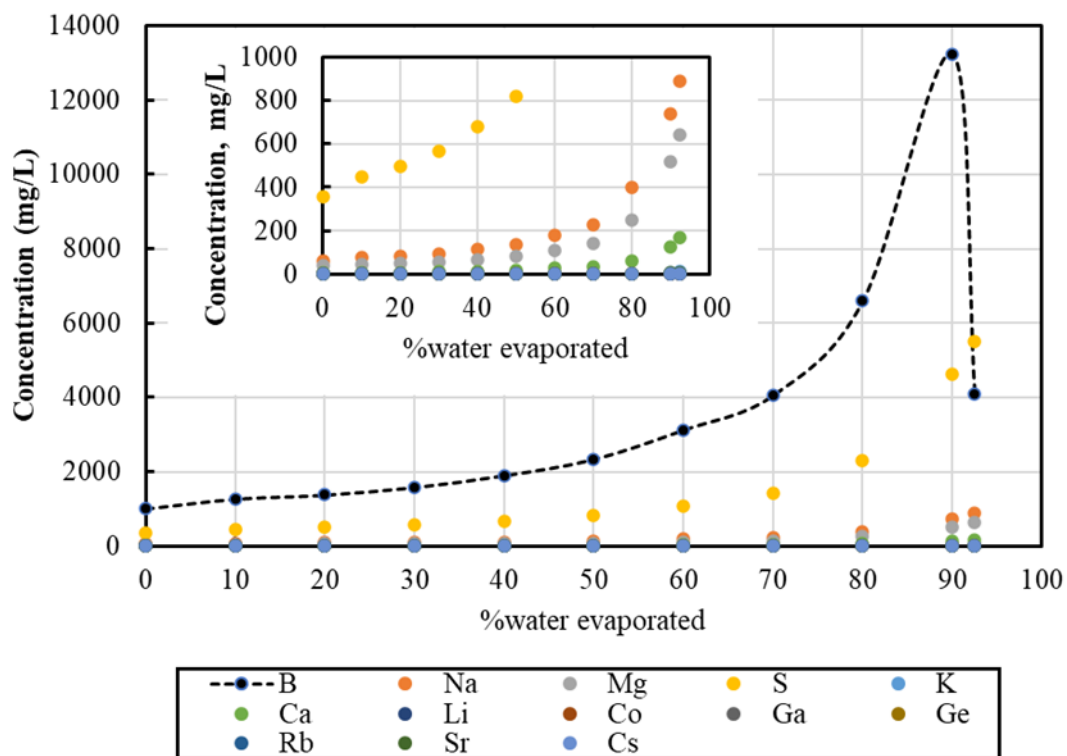
432 The capacities obtained were lower than the ones from the literature. For instance, Figueira et al. [26]
433 reported an adsorption capacity around 13 mg/g for CRB03 (differences with CRB05 are related to
434 the porous support) after testing it in column mode. Apart from that, Vallès et al. [29] obtained
435 adsorption capacity values from 3.8 to 9.0 mg B/g for S108 and from 9.1 to 12 mg B/g resin for
436 CRB05. It should be mentioned that the discrepancies between the values arise due to the fact that
437 the ones present in **Table 4** were determined using the data till the breakthrough point ($C/C_0 = 0.1$),
438 whereas the data from the literature was reported after reaching a complete saturation of the resin.
439 With regard to the concentration factor, Vallès et al. [29] reported the possibility to concentrate boron
440 up to 7.4 for S108 and up to 9.6 for CRB05, which are in agreement with the data here obtained.
441 Finally, with respect to the desorption efficiency, similar values were achieved as Jung and Kim [49]
442 and Vallès et al. [29].

443

444 **3.1.4. Boron recovery from the eluate**

445 A synthetic solution mimicking the eluate from MP1 and GP1 3 was used to crystallize B via an
446 evaporative route, as reported by Vallès et al. [35].

447 Figure 9 shows the concentration profiles as function of the water evaporated (in %). It can be
448 observed that the concentration of different elements tended to increase as water was evaporated until
449 reaching a value of 90%. Once this point was reached, the solution was cooled down, which caused
450 the precipitation of boron, evident in the figure by the B concentration decrease from 13.2 g/L to 4.1
451 g/L. It should be highlighted that the other elements in solution did not precipitate.



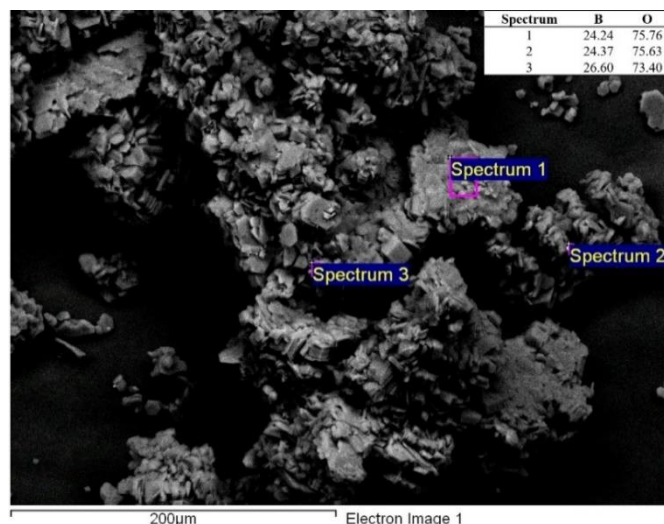
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453 **Figure 9** Boron and other Trace Elements concentration in the eluate solutions during the
 454 evaporation/concentration step. The inset shows a zoom in the low-concentration range for the trace
 455 elements.

456

457 The solids collected were analyzed by FESEM-EDAX (Fig. 10), showing small (<10 μm), flat and
 458 uniform crystals. When the solids were analyzed by EDAX, only the presence of B was noticed. It
 459 should be noted that the presence of oxygen by EDAX might be related to the H₃BO₃(s), but also to
 460 the polymeric support used.

461



462

463 **Figure 10** FESEM-EDAX analysis, showing crystals morphology and elemental composition of the
 464 solid (B and O can be related to the boric acid nature of crystals)

465

466 When acid digestion was performed, followed by ICP analysis, the solid revealed a high content of
 467 B, which was equal to 973.2 ± 5.9 mg $\text{H}_3\text{BO}_3/\text{g}$, see Table 6. With regard to the impurities within the
 468 solid, it was observed that they were mostly related to S and Sr, which could be related to any likely
 469 precipitation of $\text{SrSO}_4(\text{s})$. other elements remained below 0.6% (Table 6).

470

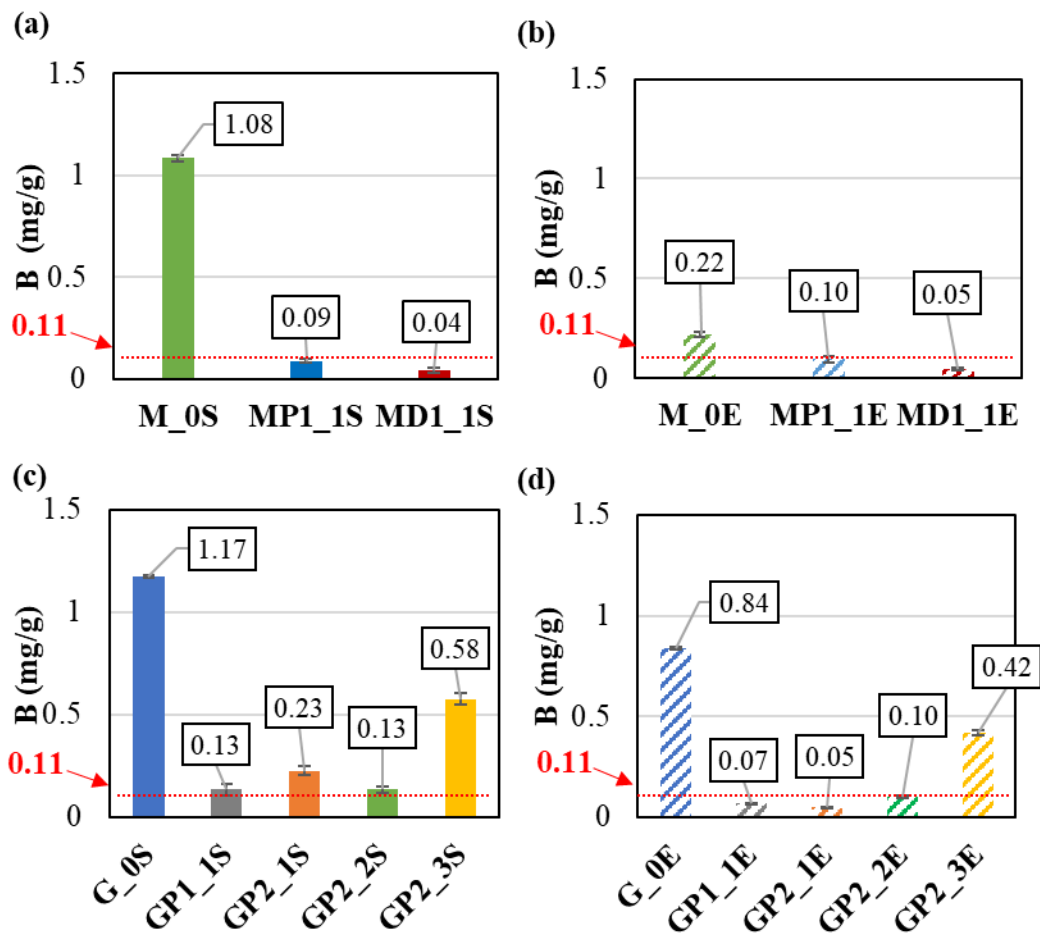
471 **Table 6** Composition of the solids following acid digestion 2% HNO_3 and analysis by ICP. No traces
 472 of Li, Ga, Rb and Cs were detected.

Element	mg/g	%
B	170.2 ± 1.1	95.6 ± 2.5
Ca	0.36 ± 0.11	0.20 ± 0.05
Mg	0.18 ± 0.09	0.10 ± 0.05
Na	0.99 ± 0.39	0.55 ± 0.20
S	1.57 ± 0.98	0.88 ± 0.52
K	0.16 ± 0.04	0.09 ± 0.02
Co	0.99 ± 0.24	0.55 ± 0.12
Ge	0.73 ± 0.33	0.40 ± 0.17
Sr	2.91 ± 1.74	1.62 ± 0.93

473 **3.2. Analysis of precipitated Mg(OH)₂(s) samples**

474 **3.2.1. Boron content in Mg(OH)₂(s) samples**

475 The major focus of precipitation experiments from the B-treated bitterns was to identify whether the
 476 B presence in the precipitated Mg(OH)₂(s) could be effectively reduced by the proposed pre-
 477 treatment. With this respect, the boron content in synthesized Mg(OH)₂ powders was measured by
 478 ICP-MS technique for all precipitation experiments performed and results are reported in **Figure 11**.



479
 480 **Figure 11** Boron concentration in Mg(OH)₂(s) samples precipitated from virgin and treated (boron-
 481 free) bitterns. Experimental conditions for each tests are reported in **Table 4**. The red dotted line
 482 indicates the boron threshold concentration of ~0.11 mg B/g for the refractory industry [39].

483
 484 Boron content ranged between 1.2 and 1.1 mg B/g in Mg(OH)₂(s) samples synthesized from un-
 485 treated Margi and Galia bitterns by adopting OH⁻/Mg²⁺ stoichiometric amounts, namely M_OS and
 486 G_OS samples (Figure 11 a and c), while it was almost one order of magnitude lower, i.e. ~0.1-0.2

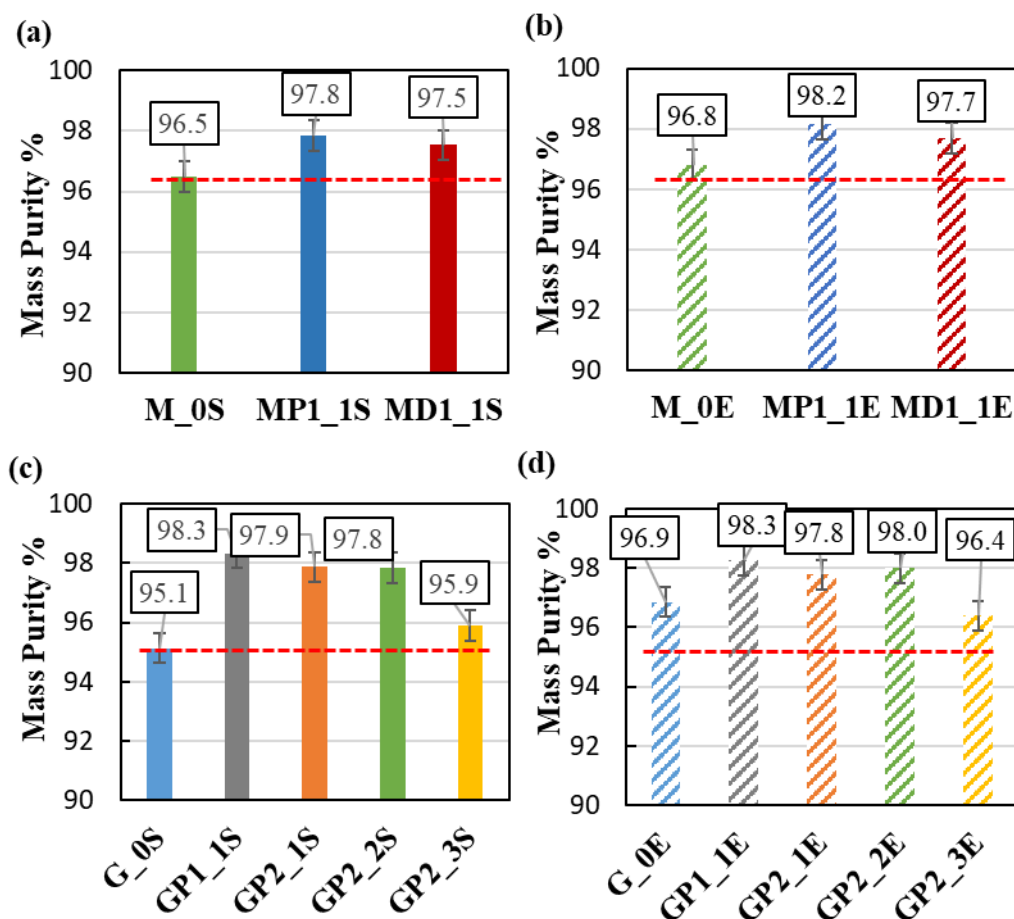
487 mg B/g, in samples produced from bitters collected at the first 4 PVs (Figure 11 a and c). It can be
488 observed, in fact, that the boron content in the sample GP2_3S, which was synthesized by using the
489 bittern collected at 4-6 PVs, increased in accordance with the boron content measured in the treated
490 bitters. Mg(OH)₂ powders synthesized by adopting OH⁻/Mg²⁺ excess amounts exhibited lower boron
491 contents. This was somehow expected [50]. The pH of the reaction environment, in fact, strongly
492 influences the boron adsorption on Mg(OH)₂(s) surfaces. The boron adsorption mechanism has been
493 described to occur between OH⁻ groups of Mg(OH)₂(s) compounds and B(OH)₄⁻ ions [51]. Mg(OH)₂
494 particles are characterized by a positive and negative electric charge below and above pH 12
495 (isoelectric point) [52]. The different charge of the particles favors or hinders the interaction with
496 B(OH)₄⁻ ions. Below the isoelectric point, B(OH)₄⁻ ions are adsorbed onto Mg(OH)₂ particles, while
497 above the isoelectric point, B(OH)₄⁻ ions are mostly rejected. The highest boron concentrations were
498 ~0.84, ~0.42 and ~0.22 mg B/g in G_0E, GP2_3E and M_0E samples, respectively, see Figure 11 b
499 and d. Conversely, the pH environment did not significantly affect the boron content in Mg(OH)₂(s)
500 samples produced from treated bitters collected at the first 0-3 PVs that was always lower than ~0.10
501 mg B/g. In these samples, boron content was almost the same as that observed in samples synthesized
502 under stoichiometric reagents conditions. This result confirms the effective boron removal by the
503 resins.

504 As discussed in the introduction section, the boron content in Mg(OH)₂ powders can limit their
505 applicability in several industrial sectors. As an example, in the refractory industry, the boron
506 concentration must be lower than a threshold value of ~0.11 mg B/g [39]. As can be seen in Figure
507 11, powders synthesised from treated bitters collected in the first 1-4 PVs reported boron
508 concentrations lower or slightly above, i.e. 13 mg B/g against 11 mg B/g, the threshold one. This
509 threshold value was always considerably exceeded, when adopting untreated bitters even using OH⁻
510 /Mg²⁺ excess amounts, thus making the resin adsorption pre-treatment in all cases a reliable step for
511 boron removal and Mg(OH)₂ particles production for refractory applications.

512

513 **3.2.2. Mg(OH)₂(s) purity determination by TG analysis**

514 Boron content in Mg(OH)₂ powders is expected to affect their mass purity. Mg(OH)₂(s) mass purity
515 values measured via TG analysis for samples synthesized from treated and untreated bitters are
516 reported in Figure 12.



517

518 **Figure 12** Mg(OH)₂(s) purity values determined by TG of samples synthesized from treated and
 519 untreated bitterns. Red dashed line is the mass purity value evaluated for cases M_0S and G_0S.

520

521 The mass purity trend very well agreed with the boron content reduction in solids. The lowest mass
 522 purity values were measured in samples synthesized from the untreated bitterns under OH⁻/Mg²⁺
 523 stoichiometric conditions, namely 96.5% and 95.1% in M_0S and G_0S samples, respectively. Mass
 524 purity increased in powders synthesized from virgin bitterns by adopting an OH⁻/Mg²⁺ amount excess
 525 reaching values of ~96.8% in both M_0E and G_0E samples. Mg(OH)₂ solids produced from bitterns
 526 collected between the first 0-4 PVs showed mass purities always higher than 97.5 % under OH⁻/Mg²⁺
 527 stoichiometric and OH⁻ amount excess. One again, mass purity of samples GP2_1S, GP2_2S and
 528 GP2_3S followed the boron content evidence of **Figure 11**. Specifically, mass purity decreased in
 529 sample GP2_3S due to the saturation of the resin.

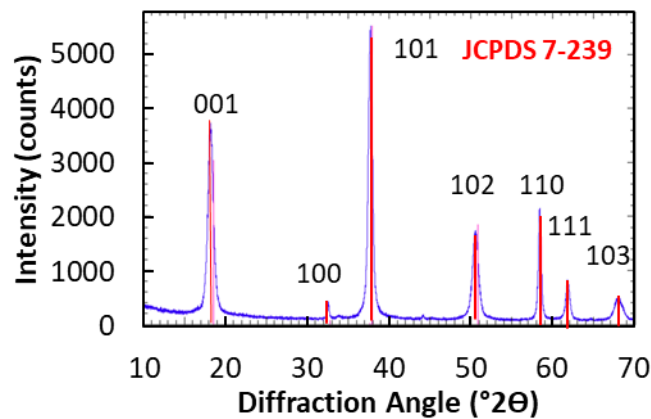
530 Unfortunately, it is difficult to predict the possible mass purity percentage attributed to boron
 531 compounds. H₃BO₃ and B(OH)₄⁻ species, in fact, are expected to interact with Mg(OH)₂(s)
 532 compounds to form more stable multi-coordination compounds [53]. Due to the special coordination

533 property of boron, many kinds of boron oxygen coordination anions in boron aqueous solution (such
534 as $[B_3O_3(OH)_4]^{2-}$, $[B_4O_5(OH)_4]^{2-}$) can be formed leading to the uncertainty of the formation of
535 different boron magnesium compounds [53].

536

537 3.2.3. Mineralogical characterization of $Mg(OH)_2(s)$ samples by XRD

538 The possible boron presence in synthesized $Mg(OH)_2$ powders was also investigated through XRD
539 analyses. Figure 13 shows the XRD pattern of the $Mg(OH)_2$ powder synthesized in the M_0S test.



540

541 **Figure 13** XRD pattern of the $Mg(OH)_2$ powder synthesized in the M_0S test. Characteristic peaks
542 of magnesium hydroxide (brucite) mineral are highlighted in red (JCPDS 7-239).

543

544 Only characteristic peaks of the brucite mineral are identified in the XRD pattern. This can be
545 attributed to the low boron content that could not be detected by the adopted technique. Similar
546 patterns were identified in all other cases, here omitted for the sake of brevity.

547

548 **4. Conclusions**

549 In this study, the integration of ion-exchange technology and crystallization was evaluated to recover
550 boric acid and magnesium hydroxide from *bitterns*. The results indicated the possibility to recover
551 pure magnesium hydroxide (>98%) with a low content of boron (<~0.11 mg B/g), which can make
552 possible to use it in the refractory industry.

553 Initially, the performance of N-methylglucamine based resins was evaluated to treat two different
554 *bitterns*, differing on initial concentrations. It was observed that both resins evaluated (S108 and
555 CRB05) effectively removed boron, being the CRB05 the one that showed a best performance in
556 terms of capacity and concentration factor achieved. However, it should be noted that Purolite S108
557 was the only one that was able to target both boron and germanium. It should be also highlighted the
558 fact that resins were effectively regenerated using 1 M HCl. Following elution, it was possible to
559 recover the boron via an evaporative crystallization as boric acid, resulting on a purity of
560 $95.61 \pm 2.45\%$.

561 In the case of magnesium crystallization, it was observed that the solids presented between 1.2 and
562 1.1 mg B/g if the *bittern* is treated as it is. However, the solids presented concentrations below 0.1 mg
563 B/g by pre-treating the resins with ion-exchange resins. Apart from that, the integration of ion-
564 exchange resins resulted in an increase of the magnesium hydroxide purity from 95.1% (no pre-
565 treatment) to ~98 %.

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592

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595 and SMEs, (2023).

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