

# Recovery of Lithium Carbonate from Dilute Li-Rich Brine via Homogenous and Heterogeneous Precipitation

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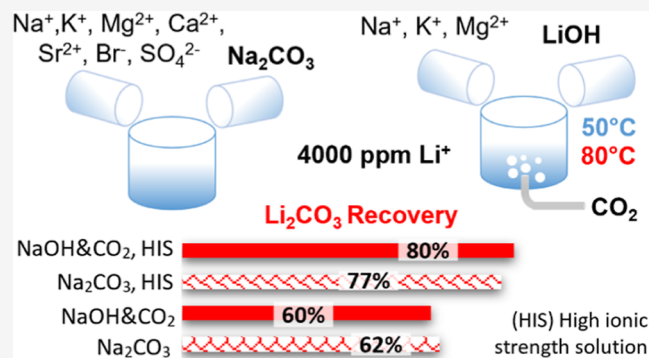
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**ABSTRACT:** An extensive experimental campaign on Li recovery from relatively dilute LiCl solutions (i.e.,  $\text{Li}^+ \sim 4000$  ppm) is presented to identify the best operating conditions for a  $\text{Li}_2\text{CO}_3$  crystallization unit. Lithium is currently mainly produced via solar evaporation, purification, and precipitation from highly concentrated Li brines located in a few world areas. The process requires large surfaces and long times (18–24 months) to concentrate  $\text{Li}^+$  up to 20,000 ppm. The present work investigates two separation routes to extract  $\text{Li}^+$  from synthetic solutions, mimicking those obtained from low-content  $\text{Li}^+$  sources through selective  $\text{Li}^+$  separation and further concentration steps: (i) addition of  $\text{Na}_2\text{CO}_3$  solution and (ii) addition of NaOH solution +  $\text{CO}_2$  insufflation. A Li recovery up to 80% and purities up to 99% at 80 °C and with high-ionic strength solutions was achieved employing NaOH solution +  $\text{CO}_2$  insufflation and an ethanol washing step.



## 1. INTRODUCTION

The increasing demand of raw materials has pushed researchers and industrials to seek for new alternative solutions to overcome the limited availability from typical sources (e.g., mines and ores). Seawater, brines, and bitterns have been extensively studied as promising alternatives for the extraction and recovery of valuable and crucial elements<sup>1–4</sup> such as magnesium ( $\text{Mg}^{2+}$ ), lithium ( $\text{Li}^+$ ), rubidium ( $\text{Rb}^+$ ), strontium ( $\text{Sr}^+$ ), and so forth. Seawater contains almost all the elements of the periodic table, although many elements are present in very low concentrations. Seawater bitterns, such as those generated in saltworks, are more concentrated than seawater. Within saltworks, seawater goes through a natural process of evaporation and fractional crystallization, aiming at producing sea salt and very concentrated brine (bittern) as a byproduct.<sup>5</sup>

Lithium, recently defined as “the new white gold”,<sup>6</sup> is extensively employed for the production of lithium-ion batteries, which are widely used thanks to their high specific energy density (100–265 W h/kg) and lifespan cycles (400–1200), making them the most suitable technology for electrical vehicles and portable electronic devices.<sup>7</sup> The industrial lithium demand has increased sharply, and it is foreseen to increase from 237,000 tons of lithium carbonate equivalent (LCE) in 2018 to 4.4–7.5 million tons of LCE by 2100.<sup>8</sup>  $\text{Li}^+$  is the 14th most abundant element in seawater with an average concentration of 0.17 ppm. From statistics, it can be estimated that a total amount of elementary lithium between 230,000 and 250,000 megatons (Mt) is contained in seawater,<sup>9</sup> equivalent

to 1,200,000–1,300,000 Mt of lithium carbonate (LCE), thus orders of magnitude higher than present and future world demand. However, novel and innovative processes have to be developed to recover and extract  $\text{Li}^+$  from low-grade and unfavorable sources. So far, most of the exploited world's  $\text{Li}^+$  reserves are high-content  $\text{Li}^+$  brines located at few geographically specific sites, for example, Chile, Bolivia, China, and Argentina.<sup>6,8</sup> An example is the Salar de del Hombre Muerto brines (north-western Argentina) that contain more than 1000 ppm  $\text{Li}^+$ .<sup>10</sup>

In the last 20 years, research efforts have been put for the development of novel processes for the recovery of lithium from low-grade and unfavorable deposits as for lithium end-life waste batteries,<sup>11–14</sup> wastewaters from oil and gas fields,<sup>15</sup> and low-lithium-content brines/bitterns.<sup>16–18</sup> Although  $\text{Li}^+$  content in bitterns is lower than that in salty brines reserves, as it reaches values from 2–3 ppm up to 20 ppm in Egyptian bitterns,<sup>16</sup> saltwork bitterns are generated every year starting from seawater and are, therefore, a more sustainable and continuous source of  $\text{Li}^+$  compared to salty brines accumulated in thousands of years. In this context, the SEArCircularMINE

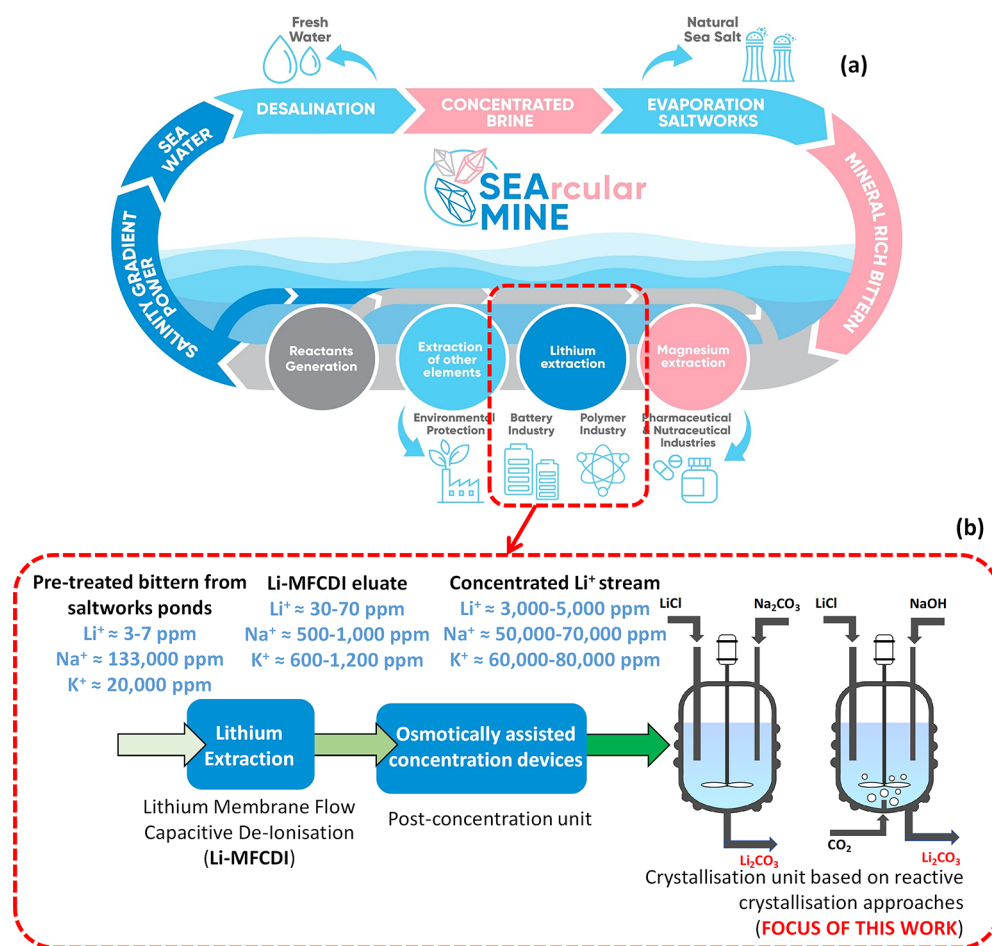
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**Figure 1.** Schematic representation of the general SEArctularMINE-integrated treatment chain (a) and a detailed description of the lithium separation/concentration/recovery steps within the chain (b).

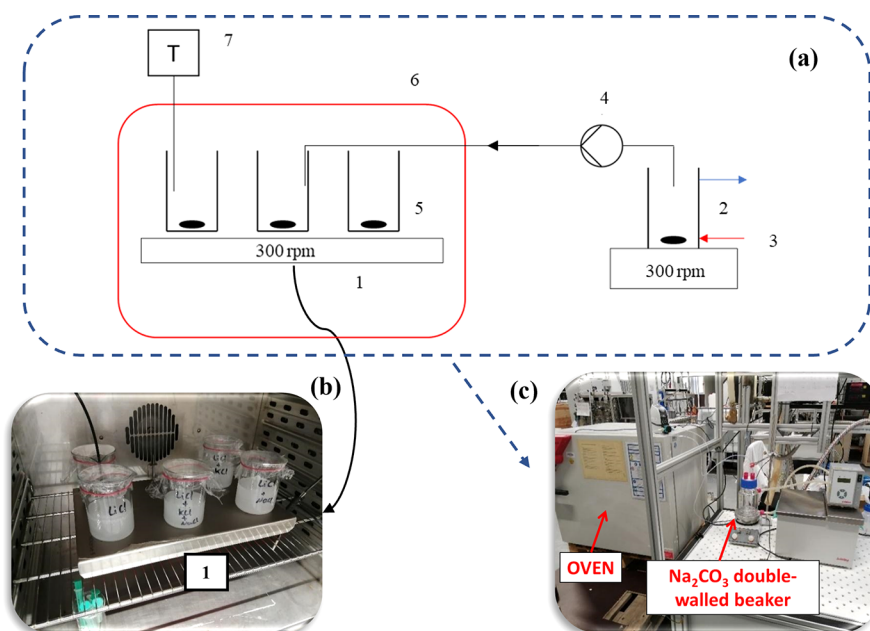
European project aims at valorizing spent bitterns produced by the traditional and still widely employed saltworks (a schematic of the SEArctularMINE-integrated treatment chain is shown in Figure 1a). Among the other minerals, lithium is going to be recovered for the first time employing a novel membrane-based electrochemical Li<sup>+</sup> separator (Li-MFCDI), which separates lithium ions from the bittern into a receiving solution. The Li-rich MFCDI eluate is further concentrated using osmotically assisted concentration devices, and finally, the Li<sup>+</sup>-concentrated solution is fed into a crystallizer unit to recover Li<sup>+</sup> in the form of carbonate salt (a scheme of the lithium separation/concentration/recovery steps within the chain is shown in Figure 1b). The overall Li<sup>+</sup> recovery stage allows concentrating the Li<sup>+</sup> from 3 to 7 ppm, in the original bittern, to a final concentration of 3000–5000 ppm, thus enabling the possibility of solids separation in the crystallizer. It is worth noting that the Li-MFCDI separator is not expected to be ideally selective toward the passage of Li<sup>+</sup>, especially with the extremely high starting concentration of other monovalent ions; thus, a significant presence of other ions in the Li-MFCDI eluate is expected too, within the range of concentration qualitatively indicated in the scheme in Figure 1b.

**1.1. Overview of Current Strategies for Li<sub>2</sub>CO<sub>3</sub>(s) Production and Motivation of This Work.** The most important commercial Li<sup>+</sup> compound is Li<sub>2</sub>CO<sub>3</sub>(s) that

accounts for 60% of the market share of lithium-based commercial products,<sup>19</sup> followed by lithium hydroxide LiOH(s) (23% market share).<sup>7</sup>

Starting from Li-rich brines, the major process for recovering lithium from brines is the lime soda evaporation process that typically consists of stages starting with concentration by evaporation, impurity removal, and precipitation. Li<sup>+</sup> is then recovered by using soda ash (Na<sub>2</sub>CO<sub>3</sub>) to obtain Li<sub>2</sub>CO<sub>3</sub> with a 99.5% purity. In Section 3.4, several precipitation approaches using Na<sub>2</sub>CO<sub>3</sub> as a precipitant agent are discussed. Further processes based on adsorption, precipitation, and on ion exchange/solvent extraction processes were also presented in the literature.<sup>16,20,21</sup>

The possibility of using CO<sub>2</sub> to recover lithium as a contribution to the circular economy and environmental sustainability was also addressed in the literature by several fundamental studies, which, however, have not been brought to the testing level by the proposed precipitation route with real Li-rich brines. Matsumoto<sup>22</sup> used a waveguide-type microwave apparatus to produce CO<sub>2</sub> microbubbles in an aqueous solution containing lithium ions (starting from LiNO<sub>3</sub> salt) to obtain lithium carbonate (Li<sub>2</sub>CO<sub>3</sub>(s)) nanoparticles. Sun et al.<sup>23</sup> employed a spinning disk reactor to precipitate Li<sub>2</sub>CO<sub>3</sub>(s) by gas–liquid reactive crystallization of LiOH and CO<sub>2</sub> using an ultrasound field. The ultrasound field, the temperature, and the CO<sub>2</sub> flow rate were found to significantly



**Figure 2.** (a) Schematic representation of the employed experimental setup for lithium precipitation with sodium carbonate: (1) six-position magnetic stirrer, (2) double-walled beaker, (3) heating water from a thermostatic bath, (4) peristaltic pump, (5) 250 mL volume beakers, (6) oven, (7) PT100 temperature probe. Pictures of the experimental setup; (b) six-position magnetic stirrer with precipitated lithium carbonate placed in an oven. (c) Whole experimental set up.

influence the  $\text{Li}_2\text{CO}_3(\text{s})$  particle size. The use of a falling film column was also investigated, some years later, by Sun et al.<sup>24</sup> for the same  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation process in the  $\text{LiOH}-\text{CO}_2$  system. Tian et al.<sup>25</sup> studied the influence of ammonium hydroxide ( $\text{NH}_3\cdot\text{H}_2\text{O}$ ) in the gas–liquid reactive crystallization of  $\text{Li}_2\text{CO}_3(\text{s})$ . The ammonium ions were believed to greatly influence the  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation process by inhibiting the re-carbonation of  $\text{Li}_2\text{CO}_3(\text{s})$ . Zhou et al.<sup>26</sup> used a coupled reaction and solvent extraction process to produce  $\text{Li}_2\text{CO}_3(\text{s})$  from the  $\text{LiCl}$  and  $\text{CO}_2(\text{g})$  system. HCl was removed, to increase the reaction yield, by solvent extraction using tri-*n*-octyl amine and iso-octanol as solvent. Han et al.<sup>19</sup> presented a comparison between homogenous  $\text{Li}_2\text{CO}_3$  precipitation using only soda ash and heterogeneous  $\text{Li}_2\text{CO}_3$  precipitation employing NaOH and the addition of  $\text{CO}_2(\text{g})$  from  $\text{Li}_2\text{SO}_4$  solutions mimicking a waste solution of lithium-containing electrical and electronic equipment. Results showed that both methods can be feasible to recover lithium as lithium carbonate salt from  $\text{Li}_2\text{SO}_4$  solutions.

On the basis of the above literature review, it is clear how the  $\text{Li}_2\text{CO}_3$  precipitation process has been extensively studied in the past. However,  $\text{Li}^+$  precipitation has been mostly studied in highly Li-concentrated solutions, with  $\text{Li}^+$  concentrations higher than 10,000 ppm,<sup>11,19,23,27</sup> with less studies addressing low Li-containing ones, with concentrations lower than 5000 ppm (as in ref 28). Nevertheless, lithium extraction from seawater, brines, and bitterns requires a preliminary concentration step to increase lithium concentrations from tens to thousands of ppm, highlighting the importance of characterizing the precipitation phenomena at low concentration than in conventional processes.

The present paper aims at reporting an extensive experimental campaign to prove the feasibility and provide the most favorable strategies for the recovery of  $\text{Li}^+$  from low-concentration solutions ( $\text{Li}^+$  concentration  $\sim 4000$  ppm). Here, attention is on  $\text{Li}^+$  recovery and purity determined in

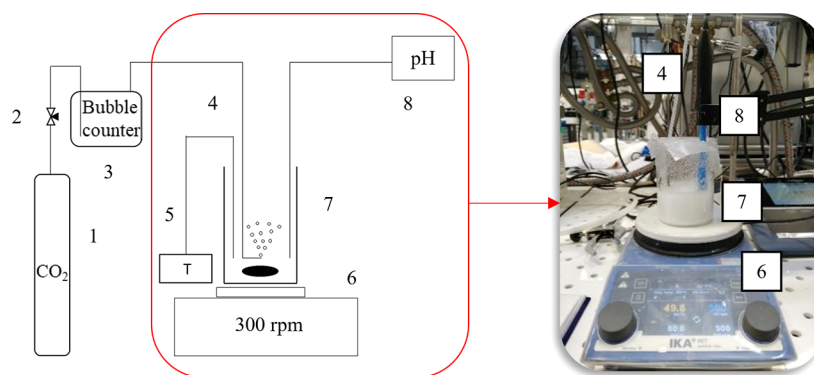
several precipitation cases. Specifically,  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation was studied following two precipitation routes: (i) using  $\text{Na}_2\text{CO}_3$  solution and NaOH solution and  $\text{CO}_2(\text{g})$  insufflation. Several parameters affecting both precipitation routes were investigated, such as  $\text{Li}^+$ /precipitant ratios, solution temperature, and the presence of dissolved monovalent and divalent ions, which can be present in the eluate of Li-MFCDI from the feed bittern (e.g.,  $\text{Na}^+$ ,  $\text{K}^+$ ,  $\text{Cl}^-$ ,  $\text{SO}_4^{2-}$ , etc.) and could be further concentrated before crystallization. A purification step using ethanol was also studied to enhance  $\text{Li}_2\text{CO}_3$  solid purity.

In regard to the NaOH solution and  $\text{CO}_2(\text{g})$  insufflation route, to the best of the author knowledge's, there are no other studies reporting  $\text{Li}^+$  purity and recovery in Li solutions containing dissolved monovalent and divalent ions mimicking real  $\text{Li}^+$  solutions. Results provide straightforward and useful information for the design of  $\text{Li}_2\text{CO}_3$  crystallizers for the recovery of lithium from low-Li-concentration solutions.

## 2. MATERIALS AND METHODS

All precipitation experiments were performed on a laboratory-scale setup, preparing synthetic solutions of LiCl, plus other salts (as simulated feed brine) and  $\text{Na}_2\text{CO}_3$  or NaOH as precipitation inducing reactants. Details on materials, experimental setups, and procedures are reported in the following sections, while for the sake of brevity, a complete description of the two investigated precipitation routes and a literature overview of previous studies focused on  $\text{Li}_2\text{CO}_3$  precipitation fundamentals are reported in the [Supporting Information](#).

**2.1. Materials.** Table S1 in the [Supporting Information](#) lists all chemicals used in the  $\text{Li}^+$  precipitation experiments. The reagents were of analytical grade and were employed without further purification. Deionized water was used for all experiments. Synthetic solutions were prepared by dissolving the desired salts weighted using a precision balance (Sartorius BCE 653) in a beaker filled with deionized water to a defined total mass of salts and water of  $\sim 110$  g. The precise mass for



**Figure 3.** (a) Schematic representation of the experimental setup employed for lithium carbonate precipitation with sodium hydroxide and carbon dioxide insufflation: (1) carbon dioxide bottle, (2) needle valve, (3) bubble counter with a regulator, (4) PE hose for CO<sub>2</sub> insufflation Ø 0.5 mm, (5) PT100 thermocouple probe (6) magnetic stirrer with a heating plate, (7) 250 mL beaker, (8) pH electrode with a measuring device. (b) Picture of the experimental setup during Li<sub>2</sub>CO<sub>3</sub> precipitation.

each experiment is reported in the relevant tables in the **Results and Discussion** section. The total volume was determined by measuring the solution density with a DMA 35 density meter (Anton Paar) and knowing the total mass of the solution. LiCl solutions of ~5000 ppm (0.70 M) were prepared aiming at obtaining an initial Li<sup>+</sup> concentration of ~4000 ppm (0.59 M) after reactant solution addition (which generates a further dilution of the initial feed solution at time  $t_0$ , at which reaction has not started yet due to the low precipitation kinetics). Exact concentrations for each experiment are reported in the relevant tables in the **Results and Discussion** section.

**2.2. Experimental Setup and Procedure for Li<sup>+</sup> Precipitation with Na<sub>2</sub>CO<sub>3</sub>.** The employed experimental setup for Li<sub>2</sub>CO<sub>3</sub> precipitation tests using Na<sub>2</sub>CO<sub>3</sub> solutions is presented in **Figure 2**. The synthetic brines were stirred steadily in a thermostatic room on a six-position magnetic stirrer and covered with Parafilm to avoid evaporation losses. The temperature of the samples was indirectly checked by measuring the temperature of a blank sample consisting of a beaker filled with a comparable amount of water, via a Pt100 temperature probe. All solutions were stirred at a speed of 300 rpm. The temperature of the Na<sub>2</sub>CO<sub>3</sub> solution, to be injected into the abovementioned samples, was controlled using a double-walled beaker connected to a thermostat and set to the same temperature as that of the thermostatic room where the precipitation took place. After reaching the desired constant temperature, the desired volume of a 2.0 M Na<sub>2</sub>CO<sub>3</sub> solution was added to the Li<sup>+</sup>-containing solution with a peristaltic pump (SIMDOS 02) at a flow rate of 10 mL/min; the same flow rate and solution concentration were used in all the experiments, unless stated otherwise. In all experiments, the reaction time is considered to start after the complete addition of the Na<sub>2</sub>CO<sub>3</sub> solution volume.

**2.3. Experimental Setup and Procedure for Li<sup>+</sup> Precipitation with NaOH and CO<sub>2</sub>(g).** The experimental setup employed for Li<sub>2</sub>CO<sub>3</sub>(s) precipitation with NaOH and CO<sub>2</sub>(g) insufflation is shown in **Figure 3**. In this case, an 8.0 M NaOH solution (32 % wt) was employed. The NaOH/LiCl solution was placed in a 250 mL beaker heated and stirred using a RET control-visc white stirrer from IKA, which offers a heating plate whose temperature is controlled based on a feedback signal acquired by a submersed Pt100 temperature probe. When the solution reached the desired temperature, CO<sub>2</sub>(g) was supplied through a polyethylene (PE) hose with an inner diameter of 0.5 mm. The hose was placed close to the

stirrer to better disperse the gas bubbles and prevent any clogging. To minimize water losses due to evaporation, the beaker was covered with Parafilm. The CO<sub>2</sub>(g) feed rate was adjusted by using a needle valve and a downstream bubble counter. The pH was continuously monitored in the precipitation beaker via a temperature-compensated SenTix precision electrode from WTW.

**2.4. Sampling and Analytical Procedures.** For the quantitative determination of cation concentration in the reacting solution, from which Li<sup>+</sup> recovery can be calculated, samples were withdrawn with pre-heated syringes (kept at the reaction temperature, to prevent any Li<sub>2</sub>CO<sub>3</sub>(s) dissolution). After sampling, the solution was filtered with a Berytec nylon syringe filter (0.22 μm) and directly diluted 1:100 to interrupt the precipitation kinetics. The solutions were further diluted, and their composition was measured by employing a multiparameter optical emission spectrometer (ICP–OES, Varian 720-ES type).

Multiple determinations of individual measurement points were carried out with a standard deviation of 3%. ICP–OES measurement accuracy was also verified by comparing ICP–OES concentration, measured at the beginning of the experiment, with the one expected from the mass of lithium dissolved in the feed. A deviation lower or equal to 4% was determined in all cases. For the sake of graphical clarity in all plots, the relevant error bars are not reported as they would coincide with the size of the symbols.

To determine Li<sub>2</sub>CO<sub>3</sub> solid purity, the precipitated solid samples were separated by vacuum filtration with a Büchner funnel using a cellulose acetate filter having a pore size of 0.45 μm. After filtration, the crystals were dried in a moisture analyzer (DLB-160-3A by Kern) at 105 °C for 12 h. Part of the dried precipitate was re-dissolved in a 1% HNO<sub>3</sub> solution and further diluted with deionized water. Subsequently, the concentration of dissolved lithium was determined by ICP–OES (see above).

In selected experiments, the precipitate was washed in order to increase its purity. For this purpose, ~0.1 g of Li<sub>2</sub>CO<sub>3</sub> was weighted and then suspended in 50 mL of ethanol ( $w = 70\%$ ) solution at room temperature for 1 h. After this step, the precipitate was filtered again, and the purity in Li<sup>+</sup> was determined by ICP–OES.

**2.5. Precipitation Performance Parameters.** In all the performed experiments, the recovery of lithium was assessed. It was calculated as the difference between the initial and final

mass of lithium in solution divided by its initial mass (eq 1). The final solution volume was inferred as the sum of the volumes of the feed Li-rich brine and the precipitant solution ( $\text{Na}_2\text{CO}_3$  or  $\text{NaOH}$ ).

$$\text{recovery} = \frac{c_{\text{initial}} \times V_{\text{initial}} - c_{\text{final}} \times V_{\text{final}}}{c_{\text{initial}} \times V_{\text{initial}}} \quad (1)$$

The mass purity of precipitate in  $\text{Li}^+$  was calculated according to eq 2

$$\text{purity} = \frac{\text{mass of } \text{Li}_2\text{CO}_3(\text{s})}{\text{mass of precipitate}} \quad (2)$$

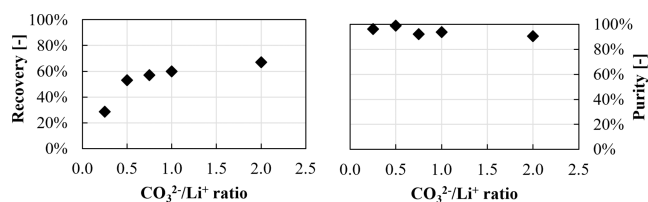
where the equivalent mass of  $\text{Li}_2\text{CO}_3$  was determined from the measured  $\text{Li}^+$  concentration in the collected precipitate samples (approximately 100 mg of the dried precipitate, see Section 2.4).

### 3. RESULTS AND DISCUSSION

**3.1. Lithium Precipitation with  $\text{Na}_2\text{CO}_3$ .** The influence of several operating parameters on lithium precipitation using  $\text{Na}_2\text{CO}_3$  was analyzed, addressing in particular (i) the effect of different  $\text{CO}_3^{2-}/\text{Li}^+$  molar ratios, (ii) the effect of solution temperature and ionic strength (given by  $\text{NaCl}$  and  $\text{KCl}$  dissolved salts) and (iii) the effect of the presence of divalent cations (namely, calcium, magnesium, and strontium) and anions (namely, sulfate and bromide ions) in the Li-rich feed brine.

**3.1.1. Influence of the  $[\text{CO}_3^{2-}]/[\text{Li}^+]$  Ratio.** The influence of the  $[\text{CO}_3^{2-}]/[\text{Li}^+]$  operating ratio on  $\text{Li}^+$  recovery and purity was investigated. Five precipitation scenarios were carried out within the  $[\text{CO}_3^{2-}]/[\text{Li}^+]$  range from 0.25 to 2 (mol/mol). Note that the  $[\text{CO}_3^{2-}]/[\text{Li}^+]$  value of 0.5 represents the stoichiometric precipitation condition, while lower and upper ratio values refer to under- and over-stoichiometric conditions with respect to the excess or lack  $\text{CO}_3^{2-}$  ions, respectively. A constant temperature of 50 °C and a 300 rpm stirring rate were maintained in all experiments. Details of the reacting quantities for each test are reported in Table S2 in the Supporting Information.

$\text{Li}^+$  recovery, eq 1, and purity, eq 2, observed at the end of all experiments (after 2 h) are shown in Figure 4.



**Figure 4.**  $\text{Li}_2\text{CO}_3$  recovery and purity as a function of the  $[\text{CO}_3^{2-}]/[\text{Li}^+]$  ratio.

$\text{Li}^+$  recovery significantly increases from  $\sim 30$  to  $\sim 60\%$  using a  $\text{CO}_3^{2-}/\text{Li}^+$  ratio of 0.25 and 1, respectively. On the other hand, only a slight increase is noticed when increasing the  $\text{CO}_3^{2-}/\text{Li}^+$  ratio from 1 to 2, that is, from  $\sim 60$  to  $\sim 65\%$ . Therefore, all the hereinafter reported experiments were carried out using a  $\text{CO}_3^{2-}/\text{Li}^+$  ratio of 1. Purity ranges between 98 and 90%, slightly decreasing at high  $\text{CO}_3^{2-}/\text{Li}^+$  ratios. In all these cases, the impurities are attributed mainly to trapped  $\text{Na}_2\text{CO}_3$ , remaining in the liquor entrained within the particle cakes after filtration.

**3.1.2. Influence of Temperature and Ionic Strength.**  $\text{Li}_2\text{CO}_3(\text{s})$  solubility decreases when the temperature is increased (see also the Supporting Information); thus, a beneficial effect of temperature on the precipitation rate is expected. In particular, the influence of temperature on the  $\text{Li}_2\text{CO}_3$  precipitation process was studied by performing experiments at 50 °C and at 80 °C with and without the presence of other monovalent ions in solution, namely,  $\text{Na}^+$  and  $\text{K}^+$ . The presence of dissolved ions (e.g.,  $\text{Na}^+$  and  $\text{K}^+$ ) increases solution ionic strength, which can be calculated as

$$I = 0.5 \sum_{i=1}^{i=n} c_i z_i^2 \quad (3)$$

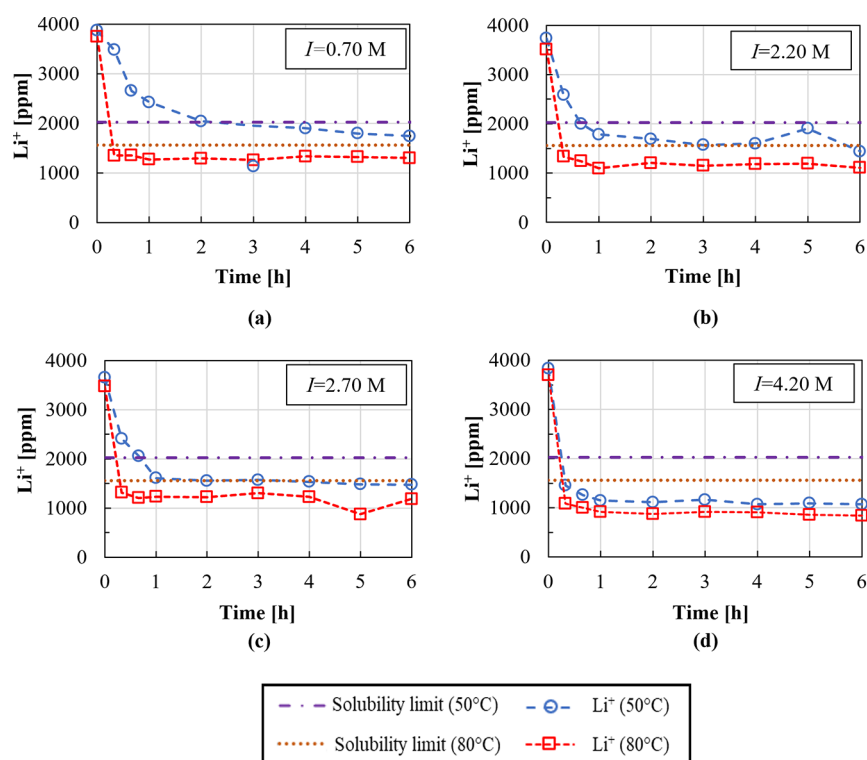
where  $I$  is the solution ionic strength and  $c_i$  and  $z_i$  are the  $i$ -th ion concentration and valence, respectively.

Four precipitation tests were carried out using a starting (before  $\text{Na}_2\text{CO}_3$  solution addition) 0.70 M  $\text{LiCl}$  solution (i) as a pure salt ( $I = 0.70$  M) or with (ii) 1.5 M  $\text{KCl}$  ( $I = 2.20$  M), (iii) 2.0 M  $\text{NaCl}$  ( $I = 2.70$  M), and (iv) both 2.0 M  $\text{NaCl}$  and 1.5 M  $\text{KCl}$  ( $I = 4.20$  M). Such  $\text{NaCl}$  and  $\text{KCl}$  concentrations were chosen based on preliminary calculation regarding the actual selectivity properties of the Li-MFCDI against monovalent and divalent ions present in the treated brine, as discussed in the introduction and shown in Figure 1. Details for all the four investigated cases are reported in Table S3 in the Supporting Information. In all experiments, solutions were stirred at 300 rpm and a double excess of a 2.0 M  $\text{Na}_2\text{CO}_3$  solution ( $\text{CO}_3^{2-}/\text{Li}^+$  ratio of 1), fed at a flow rate of 10 mL/min, was employed.

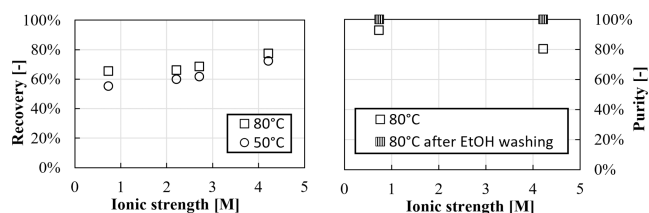
$\text{Li}^+$  concentration evolution over time during the precipitation tests is shown in Figure 5.

A final  $\text{Li}^+$  concentration of  $\sim 15\%$  lower than the ideal solubility value is obtained in pure  $\text{LiCl}$  solutions at 50 and 80 °C (Figure 5a), thanks to the over-stoichiometric amount of  $\text{CO}_3^{2-}$ . Note that, in Figure 5a, the experimental point determined at 3 h was likely affected by some measurements errors, for example, a possible wrong dilution before analysis; therefore, it was excluded from the interpolated Li concentration trend. When other ions are present, Li concentration further decreases reaching values  $\sim 25\%$  lower than the ideal solubility value for the case of single  $\text{K}^+$  or  $\text{Na}^+$  ions added (Figure 5b,c). This is induced by the ion salting-out effect between  $\text{Na}^+$ ,  $\text{K}^+$ , and  $\text{Li}^+$  ions that leads to a  $\text{Li}_2\text{CO}_3$  solubility decrease. The lower  $\text{Li}_2\text{CO}_3$  solubility induces a higher precipitated  $\text{Li}_2\text{CO}_3$  mass (higher reaction yield) and, in turn, a lower final  $\text{Li}^+$  concentration in the solutions. The observed results are in accordance with data reported in the literature<sup>29,30</sup> and better discussed in the Supporting Information. Finally, the simultaneous presence of  $\text{Na}^+$  and  $\text{K}^+$  ions causes a considerable drop in  $\text{Li}^+$  concentration, in the range of  $\sim 50$ – $60\%$  lower than the ideal solubility at 50 and 80 °C (Figure 5d). It should be also observed that  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation is more than two times faster at 80 °C ( $\sim 20$  min) than that at 50 °C ( $\sim 1$  h), but with high ionic strength solutions, the kinetics of the precipitation at medium temperatures seems to be enhanced and the precipitation occurs at a comparable time.

Figure 6 shows the Li recovery and purity as a function of solution ionic strength and temperature. For the tests at 80 °C at 0.70 and 4.20 M ionic strength, also recovery and solid purity after the EtOH washing step are reported.



**Figure 5.** Lithium concentration over time at 50 °C (dashed lines with circle symbols) and 80 °C (dotted lines with square symbols): (a) in pure LiCl ( $I = 0.70$  M) solution and in 0.70 M LiCl solutions adding (b) 1.5 M KCl ( $I = 2.20$  M), (c) 2.0 M NaCl ( $I = 2.70$  M), and (d) 2.0 M NaCl and 1.5 M KCl ( $I = 4.20$  M). Stirring speed = 300 rpm,  $\text{CO}_3^{2-}/\text{Li}^+$  ratio = 1, and  $\text{Na}_2\text{CO}_3$  solution flow rate = 10 mL/min.



**Figure 6.** Recovery and purity of  $\text{Li}_2\text{CO}_3(\text{s})$  as a function of ionic strength for  $\text{Li}_2\text{CO}_3$  precipitation experiments performed with and without the presence of  $\text{Na}^+$  and  $\text{K}^+$  ions in solution.

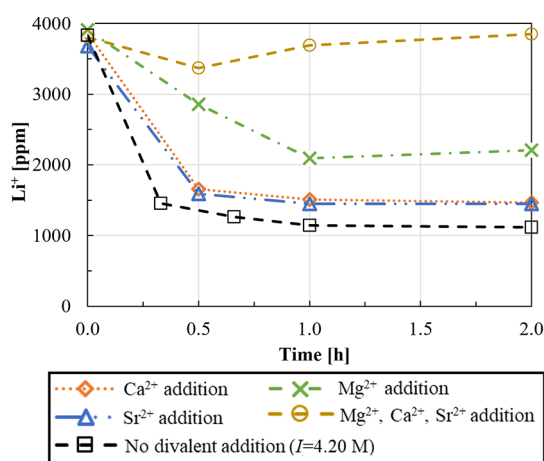
As already commented, the salting-out effect leads to a higher reaction yield, with a  $\text{Li}^+$  recovery increase passing from values around 55 and 65%, for pure LiCl solution, to 72 and 77% (at 50 and 80 °C, respectively), in the case of simultaneous dissolution of  $\text{Na}^+$  and  $\text{K}^+$  ions. Purity of solids obtained in the two extreme cases was analyzed, showing a significant drop from ~95 to ~80%, due to the presence of  $\text{Na}^+$  and  $\text{K}^+$  salts in the liquor entrapped in the crystals and on the surface of the crystals, which precipitate during the drying process. However,  $\text{Li}_2\text{CO}_3(\text{s})$  purities can be enhanced up to 100% via solid washing with ethanol, causing, on the other hand, a loss of product, resulting in an equivalent reduction of Li recovery from 77 to 57% at 80 °C.

**3.1.3. Influence of Divalent Cations:  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$  and  $\text{Sr}^{2+}$ .** The influence of dissolved divalent cations, that is,  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$ , and  $\text{Sr}^{2+}$  ions, in LiCl solutions on the  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation process was studied. Such ions can form poorly soluble compounds in basic  $\text{CO}_3^{2-}$ -containing solutions. 0.70 M LiCl solutions were prepared also by dissolving 2.0 M NaCl and 1.5 M KCl to increase solution ionic strength. Also, 0.17 M  $\text{CaCl}_2$ , 0.25 M  $\text{MgCl}_2$ , and 0.17 M  $\text{SrCl}_2$  salts were added

simultaneously and once at time. Details for all the investigated cases are reported in Table S4 in the Supporting Information. Note that all salt concentrations refer to the feed before the addition of  $\text{Na}_2\text{CO}_3$  solution.

All precipitation tests were carried out at 50 °C with a stirring velocity of 300 rpm and a double excess of a 2.0 M  $\text{Na}_2\text{CO}_3$  solution ( $\text{CO}_3^{2-}/\text{Li}^+$  ratio of 1), fed at a flow rate of 10 mL/min. Figure 7 shows  $\text{Li}^+$  concentration, after the complete addition of  $\text{Na}_2\text{CO}_3$  solutions, over time for the cases reported in Table S4.

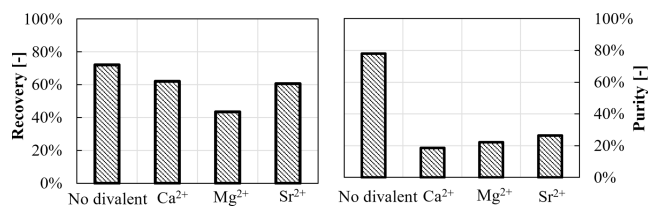
From Figure 7, in the presence of  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  single salts, a final 37% higher lithium concentration, ~1500 mg/L, is attained with respect to that in the case of no divalent ion addition. An even higher  $\text{Li}^+$  concentration, that is, ~2000 mg/L (which means much lower recovery, ~45%), is measured in the presence of  $\text{Mg}^{2+}$  salt. This can be attributed to the different influences of divalent ions on the  $\text{Li}_2\text{CO}_3$  solubility. Ma et al.<sup>31</sup> reported a  $\text{Li}_2\text{CO}_3$  solubility decrease in the presence of dissolved  $\text{Mg}^{2+}$  ions, although to a lesser extent with respect to monovalent ion cases. Therefore, it can be expected that also  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  reduce  $\text{Li}_2\text{CO}_3$  solubility, thus inducing a decrease in the final  $\text{Li}^+$  concentration in the solution. The higher final  $\text{Li}^+$  concentration in the  $\text{Mg}^{2+}$  case, however, can be attributed to the greater initial  $\text{Mg}^{2+}$  concentration and a possible superior influence of  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  on  $\text{Li}_2\text{CO}_3$  solubility. In all cases, it must stress that,  $\text{Ca}^{2+}$ ,  $\text{Sr}^{2+}$ , and  $\text{Mg}^{2+}$  carbonate compounds have a low solubility that likely causes a  $\text{CO}_3^{2-}$  consumption. This is also confirmed by results presented by King et al.<sup>32</sup> that detected traces of  $\text{CaCO}_3$  and  $\text{MgCO}_3$  in  $\text{Li}_2\text{CO}_3$  compounds precipitated from Li solutions containing 0.033 M  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$ . The simultaneous presence of the three interfering cations ( $\text{Ca}^{2+}$ ,  $\text{Sr}^{2+}$ , and  $\text{Mg}^{2+}$ ) inhibits  $\text{Li}_2\text{CO}_3$  precipitation, most likely due



**Figure 7.** Lithium concentration vs time without any divalent dissolved ions ( $I = 4.20$  M, dashed line with square symbols) and with addition of (i) 0.17 M  $\text{CaCl}_2$  (dotted line with rhombus symbols), (ii) 0.25 M  $\text{MgCl}_2$  (dashed lines with cross-symbols), (iii) 0.17 M  $\text{SrCl}_2$  (dot-dashed lines with triangle symbols), and (iv) 0.17 M  $\text{CaCl}_2 + 0.25$  M  $\text{MgCl}_2 + 0.17$  M  $\text{SrCl}_2$  (dashed lines with circle symbols). Stirring speed = 300 rpm,  $\text{CO}_3^{2-}/\text{Li}^+$  ratio = 1, and  $\text{Na}_2\text{CO}_3$  solution flow rate = 10 mL/min.  $T = 50$  °C.

to the complete consumption of carbonates ions by precipitation of the added divalent cation salts.

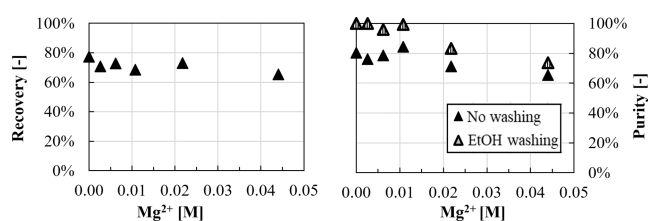
$\text{Li}^+$  recovery and purity values in the presence of divalent cations are shown in Figure 8.



**Figure 8.** Recovery and purity for  $\text{Li}_2\text{CO}_3$  precipitation experiments in the presence of divalent cations in high-ionic strength solutions. No recovery was calculated in the simultaneous presence of  $\text{Ca}^{2+}$ ,  $\text{Sr}^{2+}$ , and  $\text{Mg}^{2+}$  since no precipitation occurred.

As already commented in Figure 6,  $\text{Li}^+$  recovery can reach a value around 70% for high-ionic strength solutions without any divalent ions. Here, the presence of divalent ions causes a  $\text{Li}^+$  recovery decrease to ~60 and ~40% in the case of  $\text{Ca}^{2+}$  or  $\text{Sr}^{2+}$  and  $\text{Mg}^{2+}$  ions, respectively.  $\text{Li}^+$  recovery is totally inhibited in the simultaneous presence of all three divalent salts (no recovery). The negative impact of the presence of divalent ions can be also observed on the low  $\text{Li}_2\text{CO}_3(\text{s})$  purity, never exceeding 28% due to the co-precipitation of other carbonate compounds. Due to the considerable impact of divalent ion presence on the  $\text{Li}_2\text{CO}_3$  precipitation process, the influence of  $\text{Mg}^{2+}$  concentration was further investigated considering only  $\text{Mg}^{2+}$  traces, which are likely to be present in the Li-MFCDI eluates of the actual SEArcularMINE treatment chain. In this case, precipitation was carried out at 80 °C (again, to focus on the expected condition in the actual treatment chain) by varying the  $\text{Mg}^{2+}$  concentration from ~0.003 to ~0.044 M. For the sake of brevity, only Li recovery and purity are reported in Figure 9 as functions of the initial Mg concentration.

In this case,  $\text{Li}^+$  recovery values are close to ~70% for all  $\text{Mg}^{2+}$  concentrations, thanks to the higher employed temper-



**Figure 9.** Recovery and purity as a function of initial magnesium concentration. LiCl solutions of 0.70 M with added salts: 2.0 M NaCl and 1.5 M KCl.  $T = 80$  °C. Stirring speed = 300 rpm,  $\text{CO}_3^{2-}/\text{Li}^+$  ratio = 1, and  $\text{Na}_2\text{CO}_3$  solution flow rate = 10 mL/min.

ature; although, also in this case, they result in a lower recovery than that obtained with monovalent salts solutions (78%). A non-monotonic  $\text{Li}^+$  purity trend is observed with increasing  $\text{Mg}^{2+}$  concentration. Specifically, the purity increases from ~80 to ~90% up to a  $\text{Mg}^{2+}$  concentration of 0.01 M, which further decreases at higher  $\text{Mg}^{2+}$  concentrations. Purity decreases to values around 60% even at a low Mg concentration of 0.044 M, indicating that the presence of  $\text{Mg}^{2+}$  ions represents a crucial issue in  $\text{Li}_2\text{CO}_3$  recovery processes from  $\text{Mg}^{2+}$ -containing sources (a better combined strategy to by-pass this issue will be presented in Section 3.2.3). After the purification step with ethanol, purity values increase, leading to an almost monotonical decreasing trend, when increasing  $\text{Mg}^{2+}$  concentration. However, for higher  $\text{Mg}^{2+}$  concentrations, the washing step was unable to reach the 100% purity observed in the previous tests, thus again indicating the dramatic influence of Mg salts co-precipitation on the product purity. Also in this case, a loss of product is observed, resulting in an equivalent reduction of Li recovery from 70 to 57%.

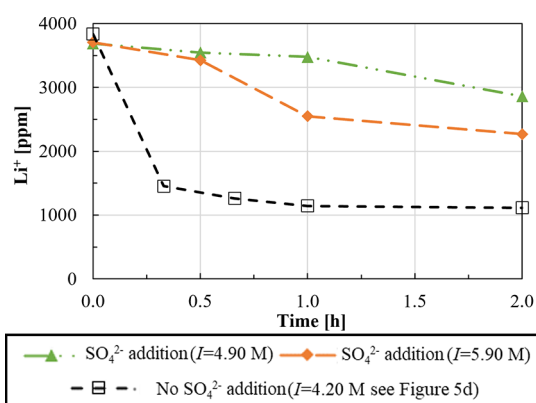
**3.1.4. Influence of Sulfates and Bromides on  $\text{Li}_2\text{CO}_3(\text{s})$  Precipitation.** The influence of sulfate and bromide anions on the  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation was studied by preparing six different solutions containing 0.70 M LiCl plus

- 1.4 M  $\text{Na}_2\text{SO}_4$  ( $I = 4.90$  M)
- 1.0 M KCl and 1.4 M  $\text{Na}_2\text{SO}_4$  ( $I = 5.90$  M)
- 1.0 M NaBr ( $I = 1.70$  M)
- 1.1 M KCl and 1.0 M NaBr ( $I = 2.80$  M).

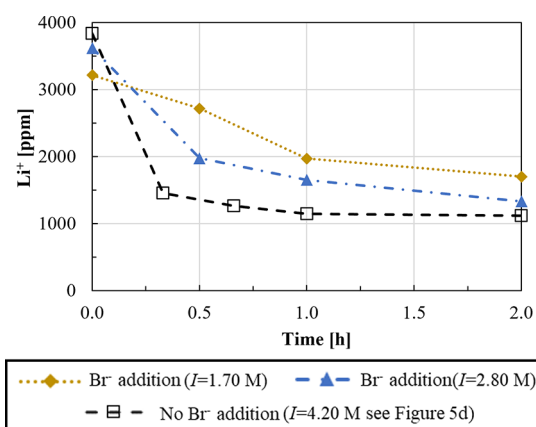
Note that all salt concentrations refer to solutions before  $\text{Na}_2\text{CO}_3$  solution addition. All precipitation tests were carried out at 50 °C with a stirring velocity of 300 rpm and a double excess of a 2.0 M  $\text{Na}_2\text{CO}_3$  solution ( $\text{CO}_3^{2-}/\text{Li}^+$  ratio of 1), fed at a flow rate of 10 mL/min. The  $\text{Li}^+$  concentration trends during the precipitation time in the presence of sulfate and bromide ions are shown in Figures 10 and 11, respectively.

From Figure 10, it can be seen that the  $\text{Li}_2\text{CO}_3$  precipitation rate considerably decreases in the presence of sulfate, in accordance with the reported delaying effect of sulfate ions on  $\text{Li}_2\text{CO}_3(\text{s})$  nucleation.<sup>32</sup> The delaying effect is reduced in high-ionic strength solutions, although no precipitation occurs within the experiments time; thus, no recovery and purity were calculated. It is worth noting that the dissolution of  $\text{Na}_2\text{SO}_4$  salts also causes a salting-in effect that, in turn, leads to a  $\text{Li}_2\text{CO}_3$  solubility increase, affecting the overall precipitation process.

Figure 11 shows the  $\text{Li}^+$  concentration trend in the presence of  $\text{Br}^-$ . It can be observed that  $\text{Br}^-$  ions do not significantly affect the Li precipitation since similar concentration trends as those for pure LiCl solutions, see Figure 5a, are obtained. Furthermore, in the presence of KCl salt ( $I = 2.80$  M), a final



**Figure 10.**  $\text{Li}^+$  concentration over time in a 0.70 M LiCl solution containing (i) 1.4 M  $\text{Na}_2\text{SO}_4$  (dashed lines with rhombus symbols,  $I = 4.90$  M), (ii) 1.4 M  $\text{Na}_2\text{SO}_4$  and 1.0 M KCl ( $I = 5.90$  M, dot-dashed lines with triangle symbols), and (iii) without  $\text{Na}_2\text{SO}_4$  ( $I = 4.20$  M, dashed lines with square symbols, see Figure 5d).  $T = 50$  °C. Stirring speed = 300 rpm,  $\text{CO}_3^{2-}/\text{Li}^+$  ratio = 1, and  $\text{Na}_2\text{CO}_3$  solution flow rate = 10 mL/min.

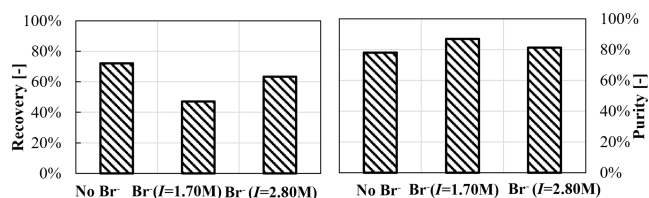


**Figure 11.**  $\text{Li}^+$  concentration over time in a 0.70 M LiCl solution containing (i) 1.0 M NaBr ( $I = 1.70$  M, dotted lines with rhombus symbols), (ii) 1.1 M KCl and 1.0 M NaBr ( $I = 2.80$  M, dot-dashed lines with triangle symbols), and (iii) without NaBr ( $I = 4.20$  M, dashed lines with square symbols, see Figure 5d).  $T = 50$  °C, stirring speed = 300 rpm,  $\text{CO}_3^{2-}/\text{Li}^+$  ratio = 1, and  $\text{Na}_2\text{CO}_3$  solution flow rate = 10 mL/min.

$\text{Li}^+$  concentration close to that in high-ionic strength solution without dissolved  $\text{Br}^-$  ions ( $I = 4.20$  M) is observed.

Figure 12 shows purity and recovery values for  $\text{Li}_2\text{CO}_3$  solids precipitated from solutions containing  $\text{Br}^-$  ions.

A Li recovery of  $\sim 47\%$  is found in the presence of  $\text{Br}^-$  ions, which increases up to 63% in higher-ionic strength solutions, almost as that in the case with no  $\text{Br}^-$  ions (72%, see Figure



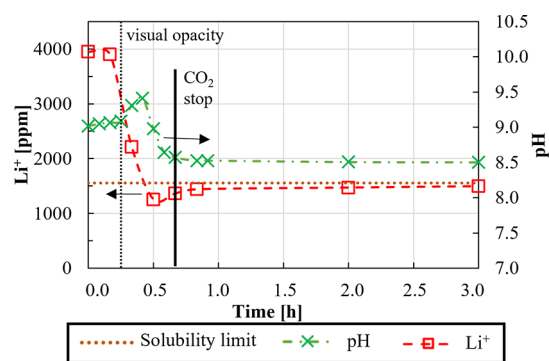
**Figure 12.** Lithium recovery and purity for  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation experiments in the presence of Br ions.

5d). Similar purity values are observed in high-ionic strength solutions with and without  $\text{Br}^-$  ions ( $\sim 80\%$ ).

**3.2. Lithium Precipitation with  $\text{NaOH}/\text{CO}_2(\text{g})$ .** The recovery of  $\text{Li}^+$  using a NaOH solution and  $\text{CO}_2$  gas insufflation represents a promising and environmentally friendly strategy for  $\text{Li}_2\text{CO}_3(\text{s})$  production and  $\text{CO}_2$  capture. The influence of several operating parameters was investigated on lithium recovery adopting such a precipitation strategy, namely, (i) the influence of the  $\text{OH}^-/\text{Li}^+$  ratio, (ii) the influence of temperature and solution ionic strength, and (iii) the influence of dissolved magnesium ions.

**3.2.1. Influence of the  $\text{OH}^-/\text{Li}^+$  Ratio.** The influence of the  $\text{OH}^-/\text{Li}^+$  ratio on  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation in a gas–liquid system was investigated within a  $\text{OH}^-/\text{Li}^+$  mole ratio between 1 and 4. Experiments were conducted at 80 °C employing different 8.0 M NaOH volume solutions. The solution was steadily stirred at 300 rpm, and  $\text{CO}_2$  gas was fed at a flow rate of  $\sim 4.5$  L/h. Details of the reacting solutions are reported in Table S5 in the Supporting Information.

In addition to the  $\text{Li}^+$  concentration variation along time, Figure 13 reports also the solution pH and indications on the



**Figure 13.** Lithium concentration (dashed lines with square symbols) and pH (dot-dashed lines with cross-symbols) versus time for a  $\text{OH}^-/\text{Li}^+ = 2$ .  $\text{Li}^+$  initial concentration after NaOH solution addition of  $\sim 3900$  ppm,  $T = 80$  °C, and stirring speed = 300 rpm.  $\text{CO}_2$  flow rate  $\approx 4.5$  L/h.

visual opacity threshold observed during the experiment, thus allowing a more phenomenological interpretation of the experiment.

For the sake of brevity, such trends are reported only for the  $\text{OH}^-/\text{Li}^+$  ratio of 2, although similar considerations hold for the other cases.

Starting from time = 0, after the addition of the alkaline reactant and starting insufflating  $\text{CO}_2$ , the solution pH increases slightly from 9.0 to 9.1 until the solution becomes turbid, indicating that  $\text{Li}_2\text{CO}_3$  precipitation has started. Then, pH increases up to  $\sim 9.4$  to further sharply decrease to 8.5. At such a pH value,  $\text{CO}_2(\text{g})$  is stopped (40 min) to prevent a pH decrease, causing  $\text{Li}_2\text{CO}_3$  “re-carbonation” (see the Supporting Information for further details). As for the pH, the  $\text{Li}^+$  concentration remains almost constant until the solution becomes turbid to suddenly drop to a value of  $\sim 1300$  ppm after 30 min, and then, it slightly increases again to a final concentration of  $\sim 1450$  ppm caused by very slight re-carbonation of  $\text{Li}_2\text{CO}_3$ . No further concentration variation is observed after  $\text{CO}_2$  interruption.

The recovery and purity as a function of the  $\text{OH}^-/\text{Li}^+$  ratio are reported in Figure 14.



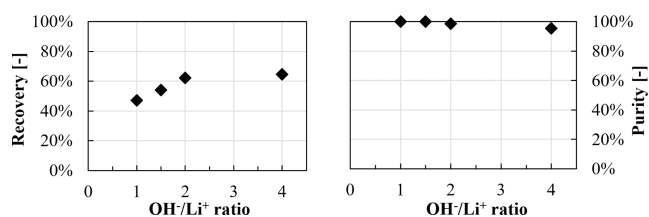


Figure 14.  $\text{Li}_2\text{CO}_3$  recovery and purity at different  $\text{OH}^-/\text{Li}^+$  ratios.

The  $\text{Li}^+$  recovery increases from ~45 to ~65%, increasing the  $\text{OH}^-/\text{Li}^+$  ratio from 1 to 4, while purity nearly reaches 100% in all cases.

**3.2.2. Influence of Solution Ionic Strength and Temperature.** To study the influence of temperature and ionic strength on the  $\text{Li}_2\text{CO}_3$  precipitation using NaOH solution and  $\text{CO}_2$  insufflation, four tests were carried out. Specifically, starting from the reference conditions presented above, an additional precipitation test was performed at 50 °C using pure 0.70 M  $\text{Li}^+$  solutions, and tests at 50 and 80 °C were performed adding 2.2 M NaCl and 3.3 M KCl to increase the solution ionic strength up to 6.20 M. Salt concentrations refer to solutions before NaOH solution addition. Solutions were steadily stirred at 300 rpm. In all the experiments a  $\text{OH}^-/\text{Li}^+$  ratio of 2 was used. The  $\text{CO}_2$  flow rate was 1.8 and 4.5 L/h at 50 and 80 °C, respectively. Figure 15 reports solution pH and Li concentrations during the experiment.

As can be seen in Figure 15, solution pH values remain almost constant until the solution becomes turbid. After turbidity detection, pH increases for ~30 min to further decrease until  $\text{CO}_2$  is stopped. Only in the case of low-ionic strength solutions at 50 °C, pH remains constant after turbidity detection and decreases after ~20 min. After  $\text{CO}_2$  insufflation interruption, solution pH settles to final values of

8.5 and 9.0 at 80 and 50 °C, respectively. Sun et al.<sup>23</sup> reported pH values of 9.0–9.5 when performing  $\text{Li}_2\text{CO}_3$  precipitation from 14,000 ppm LiCl solution at 20 °C. Conversely, Han et al.<sup>19</sup> measured a lower pH value of 8.0 at 25 and 50 °C using, however, a starting 20,000 ppm  $\text{Li}_2\text{SO}_4$  solution.

In all the experiments,  $\text{Li}^+$  concentration remains almost constant until the solution turbidity detection to further decrease sharply. In the case of low-ionic strength solutions, final  $\text{Li}^+$  concentration values of ~1500 ppm are reached, while, in high-ionic strength solution environment, the final  $\text{Li}^+$  concentration decreases up to 50%.

From Figure 15, it is also noted that  $\text{Li}_2\text{CO}_3$  precipitation is faster at 80 °C, but it is even faster in high-ionic strength solutions, where almost no induction time is recorded.

$\text{Li}^+$  recovery and purity are reported in Figure 16, along with purity after ethanol washing.

$\text{Li}^+$  recovery increases from ~50 to ~60% with increasing temperature from 50 to 80 °C. Higher recovery values are measured in high-ionic strength solutions, that is, from 60 to 80% at 80 °C. Purity values are almost 100% in low-ionic strength solutions, but significantly decrease to ~85% in high-ionic strength ones. Purity can be enhanced up to 100% by ethanol washing, causing, however, recovery losses, for example, from ~80 to ~60% in high-ionic strength solutions at 80 °C. Results are in accordance with the discussed influence of monovalent ions on the  $\text{Li}_2\text{CO}_3$  solubility, presented in Section 3.1.1.

**3.2.3. Influence of Magnesium Concentration on  $\text{Li}_2\text{CO}_3$ (s) Precipitation.** As discussed in Section 3.1.3, it is expected that LiCl solution from real biterms may contain traces of  $\text{Mg}^{2+}$ , even after  $\text{Mg}^{2+}$  removal and selective Li extraction in the abovementioned SEArctularMINE process. Thus, the detrimental influence of  $\text{Mg}^{2+}$  traces in  $\text{Li}^+$  feed solutions was also studied in the case of NaOH +  $\text{CO}_2$

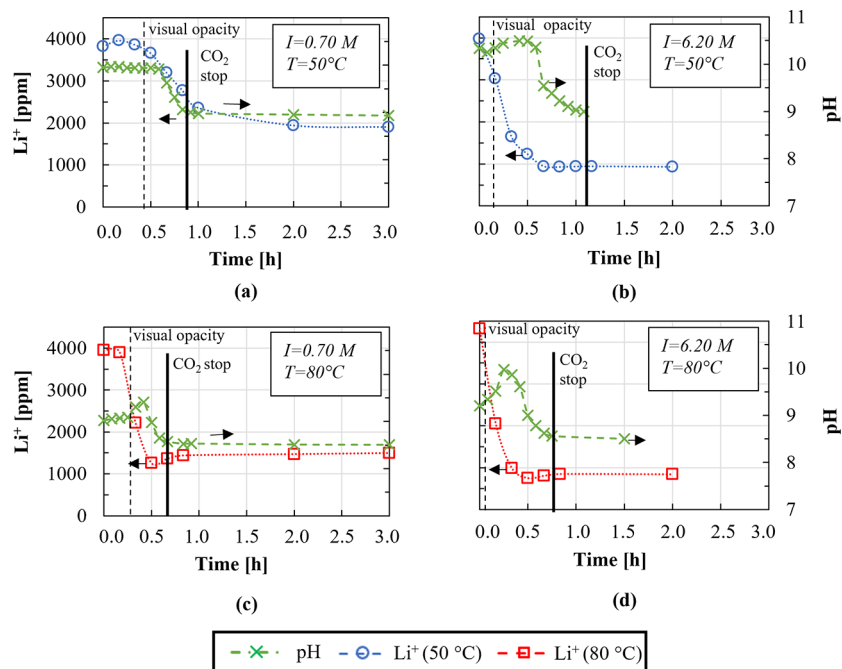
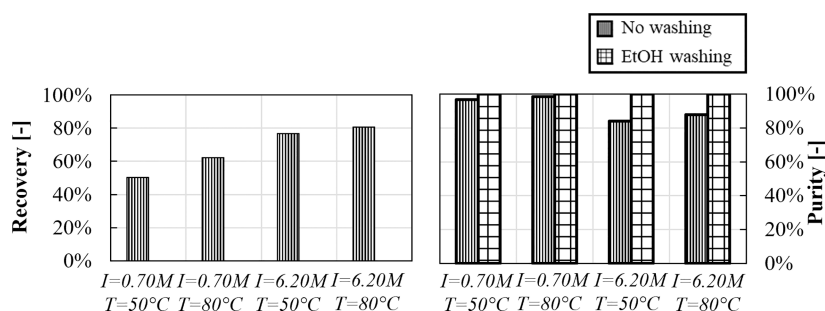


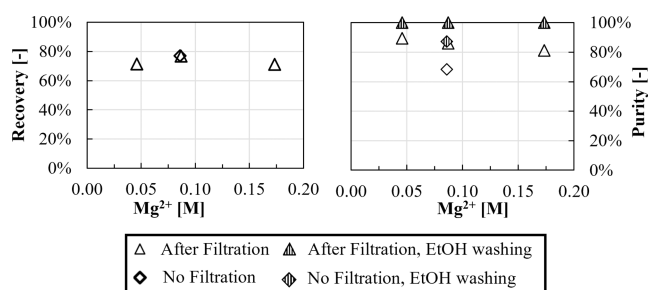
Figure 15. Lithium concentration (dotted lines with circles and square symbols) and pH (dashed lines with cross-symbols) as a function of experimental time. Experiments were performed at 50 (a,b) and 80 °C (c, d) employing 0.70 M LiCl solutions without the addition of further ions (a,c) and adding 2.2 M NaCl, 3.3 M KCl (b,d). Stirring speed of 300 rpm and the  $\text{OH}^-/\text{Li}^+$  ratio of 2. The  $\text{CO}_2$  flow rate of (a,c) 1.8 and (b,d) 4.5 L/h.



**Figure 16.** Recovery and purity for  $\text{Li}_2\text{CO}_3$  precipitation experiments from a gas–liquid system in  $\text{LiCl}$  solutions with high and low ionic strength at 50 and 80 °C.

precipitation, considering a possible  $\text{Mg}^{2+}$  concentration range from 0 to 0.2 M. Since  $\text{Li}_2\text{CO}_3(\text{s})$  forms after the addition of  $\text{NaOH}$  solutions and the insufflation of  $\text{CO}_2$ , the possibility of performing the precipitation into a two-step process was investigated, with (i) first basification of the solution ( $\text{OH}^-$  addition stage), in which  $\text{Mg}(\text{OH})_2$  solids precipitated and were then filtered out and (ii) carbonization ( $\text{CO}_2$  insufflation stage) of the filtered solution for lithium carbonate precipitation. For comparison purposes, for the case of a  $\text{LiCl}$  solution containing a  $\text{Mg}^{2+}$  concentration of 0.08 M only,  $\text{Li}_2\text{CO}_3(\text{s})$  precipitation was performed with and without filtration. All experiments were performed adding 1.8 M  $\text{NaCl}$  and 3.0 M  $\text{KCl}$  to increase ionic strength of the solution. Salt concentrations refer to solutions before  $\text{NaOH}$  addition. Temperature was kept at 50 °C, and solutions were stirred at 300 rpm. The  $\text{CO}_2$  flow rate was  $\approx 4.0$  L/h.

$\text{Li}^+$  recovery and purity values as a function of  $\text{Mg}^{2+}$  concentration are reported in Figure 17.



**Figure 17.** Recovery and purity over magnesium concentration in 0.70 M  $\text{LiCl}$ , a  $\text{OH}^-/\text{Li}^+$  ratio of 2, 3.0 M  $\text{KCl}$  and 1.8 M  $\text{NaCl}$ .  $T = 50$  °C, a stirring speed of 300 rpm, and a  $\text{CO}_2$  flow rate of  $\approx 4.0$  L/h.

Similar final  $\text{Li}(\text{l})$  concentrations of  $\sim 800$  ppm were measured in all tests leading to recovery values of about  $\sim 70$ – $75\%$ . Purity decreases with increasing  $\text{Mg}^{2+}$  concentration from 90% (0.04 M  $\text{Mg}^{2+}$ ) to 80% (0.18 M  $\text{Mg}^{2+}$ ) caused by the co-precipitation of  $\text{Mg}(\text{OH})_2(\text{s})$  and  $\text{MgCO}_3$ . Purities can be enhanced up to 100% by applying ethanol washing. It is worth noting that, when the basification step (in which  $\text{Mg}(\text{OH})_2$  precipitates) is not followed by filtration (case at  $\text{Mg}^{2+}$  0.08 M), a similar recovery of  $\sim 75\%$  is observed, while purity considerably drops from  $\sim 87$  to  $\sim 68\%$ . In this case, the ethanol washing step is not able to increase the purity above 90%, as it was also reported in Section 3.1.3. Such a result demonstrates that  $\text{Mg}(\text{OH})_2$  precipitation and filtration before  $\text{CO}_2$  insufflation and  $\text{Li}_2\text{CO}_3$  precipitation can be employed as a promising approach to first eliminate  $\text{Mg}^{2+}$  content in  $\text{LiCl}$  solutions and then obtain  $\text{Li}_2\text{CO}_3$  solids with high purity ( $\sim 90\%$ ) and recovery ( $\sim 70\%$ ).

**3.3. Comparison between  $\text{Li}^+$  Precipitation Using  $\text{Na}_2\text{CO}_3$  and  $\text{NaOH}/\text{CO}_2$  Insufflation.** The precipitation of  $\text{Li}_2\text{CO}_3$  in  $\text{LiCl}$  solutions using either  $\text{Na}_2\text{CO}_3$  or  $\text{NaOH}$  solutions and  $\text{CO}_2(\text{g})$  insufflation alternatives was extensively addressed in Sections 3.1 and 3.2. Table 1 reports a comparison between recovery and purity results obtained from the two precipitation approaches: (i) in the case of a double excess of the precipitants at 80 °C (reference case, see Sections 3.1.1 and 3.2.1), (ii) at a low temperature of 50 °C (see Figures 5a and 15a), (iii) in the presence of high-ionic strength solutions at 80 °C (Figures 5d and 15d), and (iv) in  $\text{LiCl}$  solution in the presence of 0.04 M  $\text{Mg}^{2+}$  concentration at 80 °C (Figures 9 and 17).

From Table 1, it can be observed that temperature is a crucial parameter for  $\text{Li}$  recovery. The lowest recovery values of  $\sim 50\%$  are, in fact, achieved at 50 °C.  $\text{Li}$  recovery can be

**Table 1.** Comparison between  $\text{Li}^+$  Recovery and Purity Obtained Using Either  $\text{Na}_2\text{CO}_3$  or  $\text{NaOH}$  Solution and  $\text{CO}_2(\text{g})$  Insufflation Precipitation Routes

	precipitation method	$T$ [°C]	recovery [%]	purity [%]	equivalent recovery after EtOH washing [%]	purity after EtOH washing [%]
reference case	$\text{Na}_2\text{CO}_3$ , ( $\text{CO}_3^{2-}/\text{Li}^+ = 1$ )	80	$\sim 62$	$\sim 95$		
	$\text{NaOH}$ & $\text{CO}_2(\text{g})$ , ( $\text{OH}^-/\text{Li}^+ = 2$ )	80	$\sim 60$	$\sim 99$		
low temperature	$\text{Na}_2\text{CO}_3$	50	$\sim 55$	$\sim 94$		
	$\text{NaOH}$ & $\text{CO}_2(\text{g})$	50	$\sim 50$	$\sim 97$	$\sim 45$	$\sim 100$
high ionic strength	$\text{Na}_2\text{CO}_3$	80	$\sim 77$	$\sim 80$	$\sim 53$	$\sim 100$
	$\text{NaOH}$ & $\text{CO}_2(\text{g})$	80	$\sim 80$	$\sim 90$	$\sim 60$	$\sim 100$
0.04 M $\text{Mg}$ concentration	$\text{Na}_2\text{CO}_3$	80	$\sim 65$	$\sim 65$	$\sim 50$	$\sim 75$
	$\text{NaOH}$ & $\text{CO}_2(\text{g})$ after filtration	80	$\sim 70$	$\sim 90$	$\sim 60$	$\sim 100$

increased by using high-ionic strength solutions, reaching the highest measured recovery value of 80% when using NaOH and CO<sub>2</sub> insufflation at 80 °C. On the other hand, purity values range from 65 to 90% in high-ionic strength solution or in the presence of Mg ions. Conversely, solids produced from pure LiCl solutions exhibit purities higher than 94%. The ethanol washing step allows the production of 100% pure solids, causing, however, a Li<sup>+</sup> reduction of equivalent recovery that ranges from 45 to 63%. Results also highlight that the Li<sub>2</sub>CO<sub>3</sub>(s) precipitation using NaOH solutions and CO<sub>2</sub> insufflation can be pursued as a promising alternative for the simultaneously recovery of Li<sup>+</sup> and CO<sub>2</sub> capture since results are similar to those obtained using the classical Na<sub>2</sub>CO<sub>3</sub> precipitant, especially due to the option of enhancing the purity by a simple filtration step without losing the product in the presence of divalent ions.

Li<sub>2</sub>CO<sub>3</sub> reaction times can also be compared between results of the two precipitation approaches, see Figures 5 and 15. Specifically, precipitation times were selected when Li<sup>+</sup> concentrations did not vary more than 10% in two consecutive measurements. Table 2 reports a comparison between the precipitation times at 50 and 80 °C in LiCl solutions with and without salt addition.

**Table 2. Comparison of the Reaction Times during Li<sub>2</sub>CO<sub>3</sub> Precipitation Tests**

temperature [°C]	solution	Na <sub>2</sub> CO <sub>3</sub> [min]	NaOH and CO <sub>2</sub> (g) [min]
50	pure LiCl	300	120
	high ionic strength	60	60
80	pure LiCl	60	60
	high ionic strength	60	50

Li<sub>2</sub>CO<sub>3</sub> precipitation is faster at 80 °C, showing similar reaction times of about 50–60 min for both precipitation approaches. Similar reaction times are also observed in high-ionic strength solutions. At 50 °C, the precipitation is faster in gas–liquid systems (120 min against 300 min for Na<sub>2</sub>CO<sub>3</sub>), while it is more than two times faster in high-ionic strength solutions.

**3.4. Process Performance Comparison with the State of Art.** For the sake of comparison with the state of art, an overview of recent literature studies is reported below for the Li<sub>2</sub>CO<sub>3</sub> precipitation from Li brines, followed by a comparative table with the present work's best identified scenario.

An et al.<sup>33</sup> presented a two-stage Li extraction process from Uyuni Salar brine (Bolivia) containing 700–900 mg/L Li<sup>+</sup> and 15,000–18,000 mg/L Mg<sup>2+</sup>, among the other ions. First Mg<sup>2+</sup>, Ca<sup>2+</sup>, and sulfates were removed by precipitation using lime and sodium oxalate. Then, the purified brine was concentrated 30 folds by evaporation, reaching a final Li<sup>+</sup> concentration of 20,000 mg/L. The concentrated brine also contained 56,000, 52,000, <0.05, 350, and 20,000 mg/L concentrations of Na<sup>+</sup>, K<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>, and SO<sub>4</sub><sup>2-</sup>, respectively. Li<sub>2</sub>CO<sub>3</sub> precipitation was performed at 80–90 °C by the addition of Na<sub>2</sub>CO<sub>3</sub>. Li<sub>2</sub>CO<sub>3</sub> solid purity was higher than 99.55%, after employing hot-water washing, while the recovery was estimated to be higher than 90%. Jiang et al.<sup>34</sup> investigated the production of Li<sub>2</sub>CO<sub>3</sub> from lithium brines adopting a laboratory-scale electro-dialysis system. A synthetic brine was prepared to mimic the ion concentration in Zabuye lake brines (China)

that contain a Li<sup>+</sup> concentration of 879 mg/L. The brine was first treated with Na<sub>2</sub>CO<sub>3</sub> to reduce Ca<sup>2+</sup> and Mg<sup>2+</sup>. Afterward, a conventional electro-dialysis process was employed to increase the Li<sup>+</sup> concentration up to 3485 mg/L. The concentrated solution had also 7319, 5.3, and 37 mg/L concentrations of Na<sup>+</sup>, Ca<sup>2+</sup> and Mg<sup>2+</sup>. After Li<sub>2</sub>CO<sub>3</sub> precipitation, a secondary crystallization step was adopted to increase powder purity from 90.33 to 95.30%. Unfortunately, the authors did not provide information regarding Li<sup>+</sup> recovery. Um and Hirato<sup>35</sup> studied the recovery of lithium from seawater adopting an adsorption Li<sup>+</sup> selective step with the manganese oxide adsorbent and a further precipitation step. The obtained brine was treated using NaOH to reduce Ca<sup>2+</sup> and Mg<sup>2+</sup>. Na<sub>2</sub>CO<sub>3</sub> solution was added into the Li solution that was concentrated by evaporation at 100 °C, decreasing the solution volume to 67, 53, and 40%. The Li<sub>2</sub>CO<sub>3</sub> yield varied from 51 to 77%; however, the purity decreased from 99.4 to 98.7%. Xu et al.<sup>36</sup> developed a two-step process to produce battery-grade lithium carbonate from the Damxungcuo saline lake brine (Tibet). The brine contained 360 mg/L Li<sup>+</sup>, 54,000 mg/L, 7,300 mg/L, and 810 mg/L Na<sup>+</sup>, K<sup>+</sup>, and Mg<sup>2+</sup>, respectively. Li<sub>2</sub>CO<sub>3</sub> solids were first produced by evaporation of saline lake solutions and then added to the Li brine. Lime milk and H<sub>2</sub>O<sub>2</sub> were employed to remove insoluble compounds, NaOH was added to deplete Fe species concentration, and oxalic acid was added to remove Mg(OH)<sub>2</sub> and Na<sub>2</sub>CO<sub>3</sub> to treat Ca. After purification, industrial-grade Li<sub>2</sub>CO<sub>3</sub> was obtained that was further treated using CO<sub>2</sub> and EDTA-Li (lithium 2-carboxyhydrazine-1,1,2-tricarboxylate) at 85 °C to increase its purity up to 99.6% with a recovery of about 84%. Zhao et al.<sup>27</sup> studied the recovery of lithium carbonate from synthetic lithium chloride solutions using ultrasounds. Lithium sulfate solutions with a Li concentration between 5000 and 25,000 mg/L were obtained from the leachate of the cathode scrap of lithium-ion batteries. The precipitation process was conducted at 70 °C. Na<sub>2</sub>CO<sub>3</sub> was added at one time, immediately applying ultrasounds. Recovery and purity were compared with those of classical stirred precipitation systems without the use of ultrasounds. Recovery increased adopting ultrasound varying from 45 to 60 and from 70 to 80% for an initial Li<sup>+</sup> concentration of 5000 and 10,000 mg/L, respectively. Purity also increased using ultrasounds, showing values higher than 98% at such concentrations. Quintero et al.<sup>37</sup> developed a process for the direct production of magnesium-doped Li<sub>2</sub>CO<sub>3</sub> solids by direct co-precipitation of Mg(OH)<sub>2</sub> treating industrial Li-enriched brines. An industrial refined brine from the Albemarle industrial plant (North of Chile) was used with a concentration of 0.030, 1.14, 0.04, 0.02, and 3.22 % wt for Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>, and Li<sup>+</sup>, respectively. Ca<sup>2+</sup> was removed by using oxalate and NaOH solutions. Furthermore, NaOH was added to precipitate the remaining magnesium. Na<sub>2</sub>CO<sub>3</sub> solution was used at a 1:2 Li<sup>+</sup> ratio to co-precipitate Li<sub>2</sub>CO<sub>3</sub>. The Li<sub>2</sub>CO<sub>3</sub> precipitation process occurred with a Li<sup>+</sup> initial concentration of 30,000 ppm performed at 80 °C. The Li<sub>2</sub>CO<sub>3</sub>/Mg(OH)<sub>2</sub> solid recovery was 88%.

Table 3 reports a comparison between Li<sub>2</sub>CO<sub>3</sub> precipitation approaches presented in the literature and the best scenarios addressed in the present work.

Results indicate how the NaOH and CO<sub>2</sub> (g) precipitation route conducted at 80 °C in a high-ionic strength Li solution leads to final Li recovery and purity values not too far from those of the other presented approaches in the literature. Specifically, a recovery of 80% is slightly lower than the other

Table 3. Comparison Between  $\text{Li}_2\text{CO}_3$  Precipitation Approaches Presented in the Literature and the Best Scenarios Addressed in the Present Work

	An et al. <sup>33</sup>	Jiang et al. <sup>34</sup>	Um and Hirato <sup>35</sup>	Xu et al. <sup>36</sup>	Zhao et al. <sup>37</sup>	Quintero et al. <sup>37</sup>	present work
Li solution	Uyuni solar brine (Bolivia)	synthetic	seawater	Damxungcuo saline lake brine (Tibet)	synthetic	Albemarle industrial plant (North of Chile)	synthetic
Li concentration precipitation conditions	evaporation (from 700–900 to 20,000 mg/L) 80–90 °C $\text{Na}_2\text{CO}_3$	electrodialysis (from 879 to 3485 mg/L) $\text{Na}_2\text{CO}_3$	adsorption and evaporation (from 0.17 mg/L) 100 °C, $\text{Na}_2\text{CO}_3$	lithium seeds in a Li brine of 360 mg/L 20–85 °C, $\text{Na}_2\text{CO}_3$	5000–25,000 mg/L ultrasounds. 70 °C, $\text{Na}_2\text{CO}_3$	3000 mg/L 80 °C, $\text{Na}_2\text{CO}_3$ double excess	~4000 mg/L with high ionic strength 80 °C, NaOH & $\text{CO}_2$ (g), high ionic strength
Li recovery	expected >90%	95.3% after secondary crystallization	51–77%	84%	60–80%	88%	80% (60% after EtOH washing)
Li purity	99.55% after hot water washing		99.4–98.7%	99.6% after $\text{CO}_2$ and EDTA–Li	>98%	90% (100% after EtOH washing)	

reported values, while the purity passes from 90% of the raw precipitated product up to 100% via an ethanol washing step, thus also confirming the need for a purifying step mentioned in most of the literature studies.

#### 4. CONCLUSIONS

An extensive experimental investigation on lithium carbonate precipitation from moderately concentrated Li-rich brine was presented, with a focus on recovery and solid purity.  $\text{Li}^+$  was precipitated via homogenous and heterogeneous crystallization routes using  $\text{Na}_2\text{CO}_3$  and a gas ( $\text{CO}_2$ )–liquid (NaOH–LiCl) system. Numerous parameters affecting the crystallization process were investigated, also mimicking expected scenarios for implementation within the SEArctularMINE valorization chain with real saltworks bitterns, for example, by dissolving monovalent and divalent ions in  $\text{Li}^+$ -containing solutions. For the first time, to the best of authors' knowledge, experimental results were conducted in the case of heterogeneous  $\text{Li}_2\text{CO}_3$ (s) precipitations in the presence of added monovalent and divalent ions in the LiCl–NaOH– $\text{CO}_2$  system.

First, the influence of reaction temperature and solution ionic strength, by addition of other monovalent ions, that is,  $\text{K}^+$  and  $\text{Na}^+$ , in the feed LiCl solutions was investigated.  $\text{Li}^+$  recovery varied from 50%, in the case of low-ionic strength solutions using NaOH and  $\text{CO}_2$ (g) at 50 °C, to 80%, in high-ionic strength solutions at 80 °C employing both precipitation routes. This was not only due to the higher employed temperature at which  $\text{Li}_2\text{CO}_3$  had a lower solubility but also due to the interaction between  $\text{Li}^+$ ,  $\text{Na}^+$ , and  $\text{Ca}^{2+}$  ions that caused a further  $\text{Li}_2\text{CO}_3$  solubility decrease (salting-out effect). On the other hand,  $\text{Li}_2\text{CO}_3$ (s) purity decreased from ~95–99 to ~80–90% due to the higher concentration of other cations, namely,  $\text{Na}^+$  and  $\text{K}^+$ . It is interesting to note that higher purities were obtained using NaOH solutions and the  $\text{CO}_2$ (g) insufflation precipitation approach.

$\text{Li}_2\text{CO}_3$ (s) precipitation was found to be faster in high-ionic strength solutions, probably induced by the interaction between added cations, where reaction at 50 °C mostly occurred within 60 min, while up to 120 min were needed in low-ionic strength ones. Such a difference was not observed at 80 °C, where the high temperature led to very similar precipitation rates, thus marking a clear influence of the  $\text{Li}_2\text{CO}_3$  solubility on the precipitation process.

Afterward, the influence of divalent cations and anions, namely,  $\text{Ca}^{2+}$ ,  $\text{Sr}^{2+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Br}^-$ , and  $\text{SO}_4^{2-}$ , added in high-ionic strength LiCl feed solutions was analyzed when employing  $\text{Na}_2\text{CO}_3$  precipitant solutions. Only the influence of dissolved  $\text{Mg}^{2+}$  ions was studied in the case of NaOH and  $\text{CO}_2$ (g) insufflation. The addition of  $\text{Ca}^{2+}$ ,  $\text{Sr}^{2+}$ , and  $\text{Br}^-$  ions caused a slight decrease in  $\text{Li}^+$  recovery from ~80 to ~60% with respect to the case with no divalents. Purity considerably dropped to values of ~20% in the presence of  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  ions, while a negligible variation was observed in the presence of  $\text{Br}^-$  due to the low solubility of carbonate compounds that mostly precipitated together with  $\text{Li}_2\text{CO}_3$  in the presence of  $\text{Ca}^{2+}$  and  $\text{Sr}^{2+}$  ions in solution.

$\text{SO}_4^{2-}$  ions dramatically affected the precipitation process, which was totally inhibited for the 2 h of experimental run caused by the increase in  $\text{Li}_2\text{CO}_3$  solubility and the delay effect of  $\text{SO}_4^{2-}$  ions on the precipitation process (salting-in effect).

Considering the presence of  $\text{Mg}^{2+}$  ions, 40%  $\text{Li}^+$  recovery and 20%  $\text{Li}_2\text{CO}_3$ (s) purity were obtained with 0.25 M  $\text{Mg}^{2+}$  using the  $\text{Na}_2\text{CO}_3$  precipitation route. Further experiments

with lower  $Mg^{2+}$  concentrations, that is, from 0 to 0.05 M, confirmed the high impact of  $Mg^{2+}$  on  $Li_2CO_3(s)$  purity that was  $\sim 60\%$  even at a  $Mg^{2+}$  concentration of 0.05 M, caused by the low solubility of Mg carbonate species.

In the case of the NaOH and  $CO_2$  insufflation precipitation route, a two-step precipitation process was implemented. First, NaOH solution was added, raising the pH and leading to the precipitation of Mg insoluble salts, and then,  $CO_2$  was insufflated in the filtered solution. The method was found to be very effective: high  $Li^+$  recovery ( $\sim 70\%$ ) and high  $Li_2CO_3(s)$  purity ( $\sim 80\%$ ) were obtained even starting with a 0.20 M  $MgCl_2$  solution.

$Li_2CO_3(s)$  purity was successfully enhanced in several cases by employing an ethanol washing step that allowed to reach solid purity values of  $\sim 99\%$  accompanied, however, by a Li loss of about 10–20%.

Overall, the results provide important guidelines for the best choice of operational conditions and process control for industrial scale-up of  $Li^+$  recovery from relatively low-concentration brines. Specifically, it was demonstrated that precipitation should be performed at a high temperature (80 °C) to decrease  $Li_2CO_3$  solubility, thus achieving higher recovery values. NaCl and KCl salts can be employed to increase Li recovery, thanks to the induced salting-out effect. On the other hand, a purity decrease is expected, requiring a further purification step. Divalent ions should be removed before precipitation due to the low solubility of their carbonate and hydroxide compounds that precipitate using both  $Na_2CO_3$  and NaOH solutions. Sulfate ions should be reduced as much as possible before precipitation since they cause a  $Li_2CO_3$  solubility increase (salting-in) and a kinetic delay effect. In regard to process control, care must be taken for the accurate control of the pH, especially in the case of the NaOH and  $CO_2$  precipitation route. In this case,  $CO_2$  insufflation must be blocked before re-carbonation of  $Li_2CO_3$ . It is worth noting that the NaOH and  $CO_2$  insufflation precipitation route represents an appealing potential industrial application, as also discussed in Section 3.4, whose performance is going to be demonstrated on a pilot scale, in the second phase of the SEArctularMINE project, treating real Li-rich brines.

## ■ ASSOCIATED CONTENT

### SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.iecr.2c01397>.

Fundamentals of  $Li_2CO_3(s)$  precipitation routes by  $Na_2CO_3$  or NaOH/ $CO_2$  addition along with tables reporting details of the experimental tests discussed in the main text (PDF)

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## Notes

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