

A mathematical model to evaluate hemodynamic effects of the graft anastomosis in coronary surgery



Giovanni Ruvolo¹, Calogera Pisano¹, Fabio Bertoldo¹, Marco Russo¹, Roberto Verzicco², Paolo Nardi¹

¹Department of Cardiac Surgery, Tor Vergata University Hospital, Rome, Italy

²Department of Industrial Engineering, Tor Vergata University, Rome, Italy

Kardiochirurgia i Torakochirurgia Polska 2019; 16 (2): 106-108

Abstract

The durability and patency of a coronary graft can be negatively affected by technical factors that induce thrombosis of the graft and poor prognosis of patients undergoing coronary artery bypass grafting. Technical factors include the inclination angle of the coronary anastomosis and the alignment between the main vessel and the inserted vessel as graft. We have studied a mathematical model aimed to assess the best angulation of the anastomosis and the influence of a correct alignment in order to prevent the risk of early graft occlusion. From data obtained from the mathematical model, in our opinion an inclination of the anastomotic angle of at least 30° seems to be a right choice when performing a coronary artery bypass graft. In addition, the incision of the coronary vessel should be done perfectly on the same axis as that performed on the graft, since even a deviation of the axis of the anastomosis of only 10° can create turbulence of the flow in the anastomosis site, which is accentuated when the deviation reaches 20°.

Key words: coronary graft, mathematical model.

Background and rationale of the mathematical model

Maintenance of the he patency of a coronary graft is crucial to improve the long-term prognosis of patients undergoing coronary artery bypass grafting (CABG). Early closure due to the thrombosis of the graft is affected by the perioperative pro-thrombotic effect, which can be amplified by technical factors that reduce graft flow, including anastomotic stricture or hemodynamic factors related to composition of the anastomosis causing slowing of the flow [1–6].

We have studied a mathematical model that has allowed us to evaluate the hemodynamic effects of the flow at the anastomosis point of the coronary artery in relation to the inclination angle of the anastomosis and to the alignment between the main vessel and the inserted vessel, i.e., the saphenous vein graft.

Streszczenie

Na trwałość i drożność przeszczepu wieńcowego mogą negatywnie wpływać czynniki techniczne, które powodują zakrzepicę przeszczepu i pogarszają rokowanie pacjentów poddawanych pomostowaniu tętnic wieńcowych. Czynniki techniczne obejmują kąt nachylenia zespolenia wieńcowego i wyrównanie między naczyniem głównym a naczyniem stanowiącym przeszczep. Przeanalizowaliśmy model matematyczny, którego celem jest ustalenie najlepszego kąta zespolenia i wpływu prawidłowego wyrównania, aby zapobiec ryzyku wczesnego zamknięcia przeszczepu. Na podstawie danych uzyskanych z modelu matematycznego autorzy uważają, że kąt zespolenia podczas wykonywania pomostowania aortalno-wieńcowego powinien wynosić co najmniej 30°. Ponadto nacięcie naczynia wieńcowego powinno być wykonane idealnie w tej samej osi co na przeszczepie, ponieważ odchylenie nawet o zaledwie 10° może spowodować turbulencje przepływu w miejscu zespolenia, które są wyraźne, gdy odchylenie osiągnie 20°.

Słowa kluczowe: przeszczep wieńcowy, model matematyczny.

In this research we took two cylindrical tubes of diameter $d = 1.5$ mm and $D = 2.1$ mm with a connection as shown in Figure 1 A. A constant flow $Q = 0.01$ l/min was produced from the diameter tube d , generating a mean velocity of $U = 10$ cm/s, and the same flow coming from the distal end of the diameter D tube. The two ducts met with an angle θ to which values of 15°, 30°, and 45° were assigned. The results showed the distributions of the velocities (Fig. 1 B), of the pressures (Fig. 1 C), and of the stresses on the wall (Fig. 1 D).

When the angle θ decreased, the input stream tended to align with the direction of the main duct and thus reduced the flow disturbances. If, therefore, no other factors are involved, the duct insertion, i.e. the anastomosis, should be made at the smallest possible angle.

The geometrical setup is that sketched above in which a circular vessel of diameter D has to be joined to another vessel of diameter $d < D$. Since the circumferential length

Address for correspondence: Calogera Pisano MD, PhD, Department of Cardiac Surgery, Tor Vergata University Hospital, Viale Oxford 81, 00133 Rome, Italy, phone: +39-3283297692, fax: +39 (06)20903538, e-mail: lindapisano82@gmail.com

Received: 30.01.2019, **accepted:** 30.05.2019.

of the first has to be preserved, the contact line is deformed into an ellipse. In order to maximize the section of the anastomosis, it will result for the ellipse axes $2b = d$ and $2a \sin\theta = d$, θ being the insertion angle of the anastomosis (Fig. 2).

The length of the contact line therefore decreases to the perimeter of an ellipse of semi-axes a and b which would require the integration of a complete elliptic integral of the second kind. Nevertheless, if $\varepsilon = \sqrt{1 - (b/a)^2} = \cos\theta$ is the eccentricity of the ellipse, the integral can be expanded into an infinite series of terms according to:

$$p = 2\pi a \left(1 - \left(\frac{1}{2}\right)\left(\frac{\varepsilon^2}{1}\right) - \left(\frac{1\cdot3}{2\cdot4}\right)\left(\frac{\varepsilon^4}{3}\right) - \left(\frac{1\cdot3\cdot5}{2\cdot4\cdot6}\right)\left(\frac{\varepsilon^6}{5}\right) - \left(\frac{1\cdot3\cdot5\cdot7}{2\cdot4\cdot6\cdot8}\right)\left(\frac{\varepsilon^8}{7}\right) - \dots \right)$$

Upon noticing that $a = d/(2 \sin\theta)$ and $\varepsilon = \cos\theta$ the above series become the following mathematical model:

$$p = \frac{\pi d}{\sin \theta} (1 - 0.25 \cos^2 \theta - 0.0476 \cos^4 \theta - 0.0195 \cos^6 \theta - 0.0107 \cos^8 \theta - \dots)$$

It is worth mentioning that the terms drop rapidly to zero since the coefficients keep decreasing and the increasing powers of $\cos\theta$ make this decrease even faster; as a consequence, retaining terms beyond the fifth does not alter the relevant figures of p .

The above formula is plotted on the side figure as a function of the angle θ and it can be noted that as θ decreases the length of the perimeter of the ellipse increases (and for $\theta \rightarrow 0$, $p \rightarrow \infty$).

The determination of the “optimum” angle, therefore, comes from the two opposite needs of minimizing the flow disturbances produced by the anastomosis (which would require $\theta \rightarrow 0^\circ$) while maintaining the length of p as short as possible (which implies $\theta \rightarrow 90^\circ$). From the plot of the figure it has been found that the angle $\theta = 30^\circ$ allows p to be maintained within a reasonable value ($\cong 1.5\pi d$), while limiting the flow disturbances (Fig. 3).

Discussion

The CABG surgery is still widely practiced today. In our center about 250 CABG procedures are performed annually from a total of 500–600 cardiac surgery procedures done, both as isolated and combined, and the care of the technical aspects for the success of an excellent coronary anastomosis is important for the patient’s prognosis.

In the proposed mathematic model, taking as reference the perimeter $p^* = \pi d$ of the diameter of the tube d , the value of the perimeter “ p ” of the graft anastomosis calculated in centimeters, is $p = 1.216 p^*$ for $\theta = 45^\circ$, $p = 1.548 p^*$ for $\theta = 30^\circ$, $p = 2.709 p^*$ for $\theta = 15^\circ$, respectively. Consequently, taking as a reference the largest diameter of an elliptical circumference, the diameter d of the graft incision obtained with Potts scissors required to make the anastomosis should be about the half of the perimeter value.

As can be seen, the length of p grows very rapidly at the decrease of θ when the latter drops below 30° , which suggests taking this value as a good angle to make the coronary artery anastomosis. The 30-degree value of θ may be

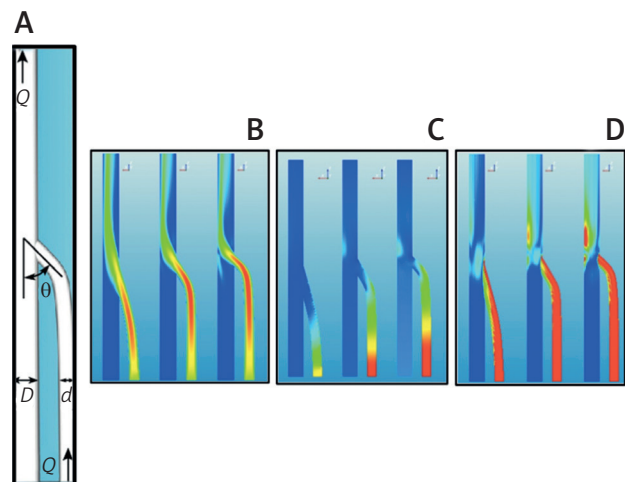


Fig. 1. A – Sketch of the set-up with the main geometrical and flow parameters. B – Color contours of the velocity magnitude in the symmetry plane of the flow for three different angles: $\theta = 15^\circ$ (left), $\theta = 30^\circ$ (centre) and $\theta = 45^\circ$ (right). Contour levels range from $U = 1$ cm/s (blue) (reference value) to $U = 16$ cm/s (red). C – The same as Figure 1 B, but for pressure values. Contour levels range from 1 mm Hg (blue) (reference value) to 3 mm Hg (red). D – Shear stress values on the wall. Contour levels range from $\tau = 1$ N/m² (blue) (reference value) to $\tau = 6$ N/m² (red)

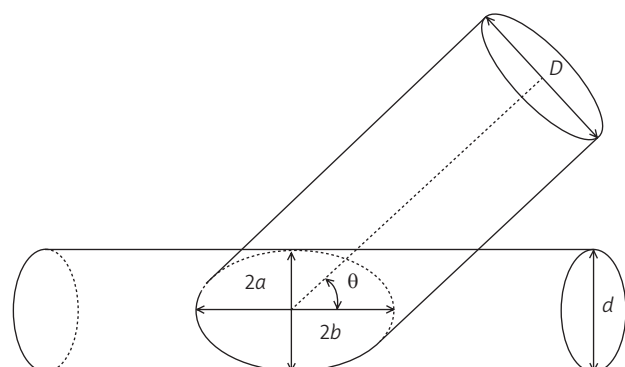


Fig. 2. Mathematical model representation of an anastomosis between the coronary artery (Tube d) and the graft (Tube D), i.e., of autologous saphenous vein

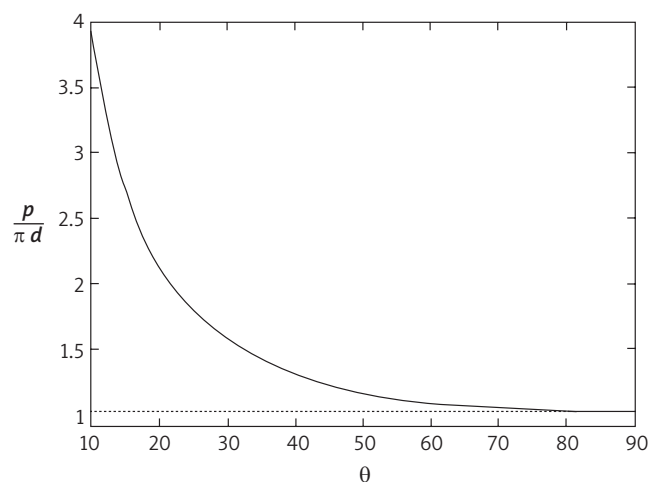


Fig. 3. Graphical representation of the relationship between the values of p and of angle θ

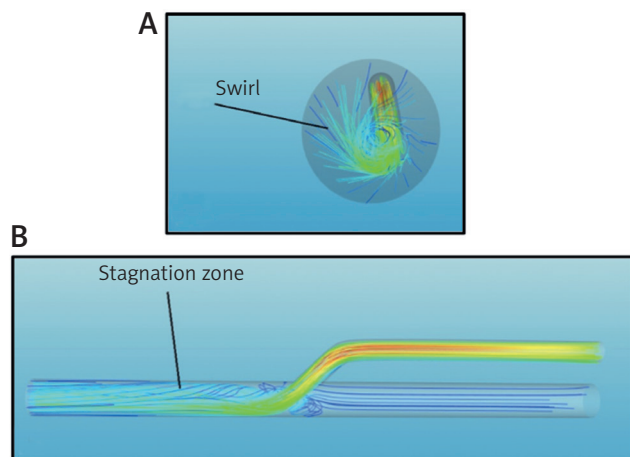


Fig. 4. **A** – Axial view of the stream traces colored by velocity magnitude for an anastomosis performed at an angle $\theta = 20^\circ$. **B** – The same as Figure 4 A, but for a side view

optimal for coronary anastomosis, as below this value the perimeter required for anastomosis increases considerably. For example, for a θ angle of 15° , the perimeter of the anastomosis almost doubles, from $1.548p^*$ to $2.709p^*$. However, based on the results obtained in the mathematical model, at angle θ ranging from 25° to 35° , presumably the graft anastomosis would perform equally well.

In addition to the inclination of the angle between the two vessels, a further parameter that can cause disturbance in the flow is the misalignment between the main vessel and the inserted vessel. In other words, if the axes of the two ducts are not coplanar, the flow in the anastomosis zone is not in an axial direction but with an angle α that determines a swirl. In this study the simulations were performed for angles $\alpha = 10^\circ$ and $\alpha = 20^\circ$, respectively. As it is easy to guess, the greater the dissipation between the two ducts is, more intense will be the swirl motion, which generates higher shear stress on the wall of the coronary vessel and a greater loss of pressure in the anastomosis area (Fig. 4 A). Therefore, the incision performed on the coronary vessel should be done perfectly on the axis with the graft, whether the coronary artery bypass is carried out in extracorporeal circulation and cardiac arrest, or on beating heart [7]. In addition to these aforementioned negative

effects, the presence of swirl motion is also an indicator of the presence of recirculation areas that are particularly damaging as they potentially cause stagnation of the blood (Fig. 4 B) and, consequently, early thrombosis of the graft [8–12].

In conclusion, in the case of coronary surgical revascularization, to reduce the hemodynamic stress on the coronary artery, from the data examined in the mathematical model studied, it appears that an inclination of the anastomotic angle of at least 30° seems to be a right choice when performing a coronary bypass. Moreover, it is necessary to make sure that coronary artery incision is done perfectly correctly in the axis on the graft anastomosis.

Disclosure

The authors report no conflict of interest.

References

1. Motwani JG, Topol EJ. Aortocoronary saphenous vein graft disease. Pathogenesis, predisposition, and prevention. *Circulation* 1998; 97: 916-931.
2. Verrier ED, Boyle EM. Endothelial cell injury in cardiovascular surgery. *Ann Thorac Surg* 1996; 62: 915-922.
3. Angelini GD, Christie MI, Bryan AJ, Lewis MJ. Surgical preparation impairs release of endothelium-derived relaxing factor from human saphenous vein. *Ann Thorac Surg* 1989; 48: 417-420.
4. Halabi AR, Alexander JH, Shaw LK, Lorenz TJ, Liao L, Kong DF, Milano CA, Harrington RA, Smith PK. Relation of early saphenous vein graft failure to outcomes following coronary artery bypass surgery. *Am J Cardiol* 2005; 96: 1254-1259.
5. Harskamp RE, Lopes RD, Baisden CE, de Winter RJ, Alexander JH. Saphenous vein graft failure after coronary artery bypass surgery: pathophysiology, management, and future directions. *Ann Surg* 2013; 257: 824-833.
6. Head SJ, Börgermann J, Osnabrügge RL, Kieser TM, Falk V, Taggart DP, Puskas JD, Gummert JF, Kappetein AP. Coronary artery bypass grafting: part 2-optimizing outcomes and future prospects. *Eur Heart J* 2013; 34: 2873-2886.
7. Moshkovitz Y, Raanani E. The art of saphenous vein grafting and patency maintenance. *J Thorac Cardiovasc Surg* 2016; 151: 300-302.
8. Sabik III JF. Understanding saphenous vein graft patency. *Circulation* 2011; 124: 273-275.
9. Milo S, Massini C, Goor DA. Coronary vein graft marking: a method to prevent graft twisting and length misjudgment. *Ann Thorac Surg* 1982; 33: 200-202.
10. de Vries MR, Simons KH, Jukema JW, Braun J, Quax PH. Vein graft failure: from pathophysiology to clinical outcomes. *Nat Rev Cardiol* 2016; 13: 451-470.
11. Ghista DN, Kabinejadian F. Coronary artery bypass grafting hemodynamics and anastomosis design: a biomedical engineering review. *Biomed Eng Online* 2013; 12: 129.
12. Tinica G, Chistol RO, Iliescu DB, Furnica C. Long-term graft patency after coronary artery bypass grafting: effects of surgical technique. *Exp Ther Med* 2019; 17: 359-367.